

Stability Properties of the Transverse Envelope Equations Describing Intense Ion Beam Transport*

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The transverse evolution of the envelope of an intense, unbunched ion beam in a periodic, linear transport channel can be modeled by the Kapchinskij-Vladimirskij (KV) envelope equations. Here we employ the KV envelope equations to analyze the linear stability properties of so-called mismatch perturbations about the matched (i.e., periodic) beam envelope in continuous focusing, periodic solenoidal, and periodic quadrupole transport lattices for a coasting beam. The formulation is analyzed and new self-consistent KV distributions are derived for an elliptical beam envelope in a periodic solenoidal transport channel. This derivation identifies appropriate emittance measures and Larmor frame transformations to allow application of standard form envelope equations to solenoidal focusing channels. Perturbed envelope equations are derived that include driving sources of mismatch excitation resulting from focusing errors, particle loss, and beam emittance growth. These equations are solved analytically for continuous focusing and demonstrate a factor of two increase in maximum mismatch excursions resulting from sudden driving perturbations relative to adiabatic driving perturbations. Numerical and analytical studies are carried out to explore properties of normal mode envelope oscillations without driving excitations in periodic solenoidal and quadrupole focusing lattices. Previous work on this topic by Struckmeier and Reiser [Part. Accel. **14**, 227 (1984)] is extended and clarified. Regions of parametric instability are mapped, new classes of envelope instabilities are found, parametric sensitivities are explored, general limits and mode invariants are derived, and analytically accessible limits are checked. Important, and previously unexplored, launching conditions are described for pure envelope modes in periodic quadrupole focusing channels.

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I. INTRODUCTION

Intense ion beams are usually transported in a periodic lattice of linear focusing elements that radially confine the beam against defocusing space-charge and thermal forces arising from the distribution of beam particles. Envelope equations are frequently used to model the low-order, statistical evolution of the beam edge. The KV envelope equations are coupled ordinary differential equations that describe the transverse evolution of the edge of an unbunched elliptical beam in a linear focusing lattice consistent with linear space-charge defocusing forces and constant emittances (i.e, invariant phase space projections)[1–3]. Even though the KV equations are self-consistent only for the singular and unphysical KV distribution function which has higher-order collective instabilities internal to the beam[4], the KV equations are valid for general distributions with evolving emittances in a rms equivalent beam sense[2, 5, 6]. Moreover, because space-charge profiles on intense beams tend to be fairly uniform in the core of the beam, the linear self-fields in the KV model should be accurate at high space-charge intensities except in a thin layer near the beam edge where the charge-density drops rapidly to zero. Consequently, for intense beams propagating in linear transport channels without significant particle loss or emittance growth, the KV envelope equations can provide a good estimate of the actual (rms statistical measure) envelope of the beam. Because of this and the fact that the ordinary differential equations describing the KV envelope evolution are straightforward to solve numerically, the KV envelope equations are extensively employed in the design of practical linear transport lattices.

The matched beam envelope is the solution to the KV envelope equations with the periodicity of the focusing lattice. The matched solution is expected to have smallest maximum radial excursions relative to other possible envelope evolutions in the lattice and it requires particular initial conditions in the envelope of beam particles. There will always be some finite mismatch error or deviation of the beam envelope from this matched evolution.

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These mismatch errors can be analyzed in terms of the small-amplitude modes about the matched solution that are supported by the KV envelope equations[2, 7]. Parametric instabilities of the mismatch modes must be avoided for practical machine operating points to maintain beam control. Even in cases where the envelope is stable, the structure of the mismatch modes is important. The frequencies of the envelope modes can resonate with lattice structures, particle orbits, and collective space-charge waves causing deleterious beam effects. For example, the high frequency breathing envelope mode is well-known to drive large-amplitude resonant beam halo causing loss of beam particles[8]. Therefore the control of this mode, even when stable, can be of critical importance.

In this paper we carry out a systematic parametric analysis of mismatch modes supported by the KV envelope equations for continuous focusing, periodic solenoid, and periodic quadrupole doublet linear transport lattices. Regions of strong parametric (band) instability for the periodic lattices are numerically mapped in a scaled manner rendering results immediately applicable to a large range of beam parameters and lattices. New classes of envelope instability are found and results are checked against analytical calculations of the envelope modes in the zero space-charge limit and in the thin-lens limit with a beam of maximal space-charge intensity. Important and often overlooked mode launching conditions and sources of envelope mismatch (driving terms) due to focusing errors, particle loss, and emittance evolution are analyzed. These launching conditions are of practical importance in understanding how to launch pure mode oscillations in experiments and simulations which can aid in understanding of complex effects.

This paper is organized as follows. In Sec. II, the envelope model employed is developed. The basic equations are reviewed, classes of transport lattices are defined, characteristic envelope responses are calculated, convenient parameterizations are identified, equations describing small amplitude driven perturbations about the matched beam envelope are derived, and general properties of envelope mode solutions are analyzed. Self-consistent KV distributions for solenoidal focusing channels are developed in Appendix B. These results are important to establish the validity of models employed. In Sec. III, the linear mode structure is completely solved in the continuous focusing limit employing a Green's function approach and the structure of the formal solutions are illustrated with specific examples to understand the differences between adiabatic, sudden, and harmonic driven perturbations. Next, normal envelope modes of periodic solenoidal and quadrupole doublet lattices are analyzed in Secs. IV and V. In both sections numerical results are presented that illustrate properties of: the matched envelope solutions, mode properties and symmetries, regions of parametric (band) instability, and pure mode launching conditions.

II. MODEL EQUATIONS

We consider an unbunched beam of ions of charge q and mass m coasting with axial relativistic factors $\beta_b = \text{const}$ and $\gamma_b = 1/\sqrt{1-\beta_b^2}$. The ions are confined transversely by linear applied focusing fields that may result from a variety of focusing systems. Linear space-charge forces internal to the beam envelope are assumed, corresponding to a spatially uniform distribution of charge within an elliptical beam envelope with beam image charges induced on any aperture structures neglected.

A. KV envelope equations

As illustrated in Fig. 1, the transverse beam cross section at axial coordinate s is taken to have an s -varying elliptical cross-section with envelope (i.e., edge) radii $r_x(s)$ and $r_y(s)$ along the principal x - and y -coordinate axes. The charge distribution is centered at $x = y = 0$ with uniform uniform space-charge within the ellipse $(x/r_x)^2 + (y/r_y)^2 = 1$, and zero outside. The x - and y -equations of motion for the orbit of a single-particle within this uniform density elliptical beam are given by [1, 2]

$$\begin{aligned} x''(s) + \kappa_x(s)x(s) - \frac{2Qx(s)}{[r_x(s) + r_y(s)]r_x(s)} &= 0, \\ y''(s) + \kappa_y(s)y(s) - \frac{2Qy(s)}{[r_x(s) + r_y(s)]r_y(s)} &= 0, \end{aligned} \tag{1}$$

where $\kappa_x(s)$ and $\kappa_y(s)$ represent linear applied forces of focusing optics in the transport lattice, and

$$Q = \frac{q\lambda}{2\pi\epsilon_0 mc^2 \gamma_b^3 \beta_b^2} = \text{const} \tag{2}$$

is the dimensionless beam perveance representing self-field defocusing forces internal to the beam. Here, $\lambda = \text{const}$ is the beam line-charge density, c is the speed of light in vacuo, and ϵ_0 is the permittivity of free-space. In the limit

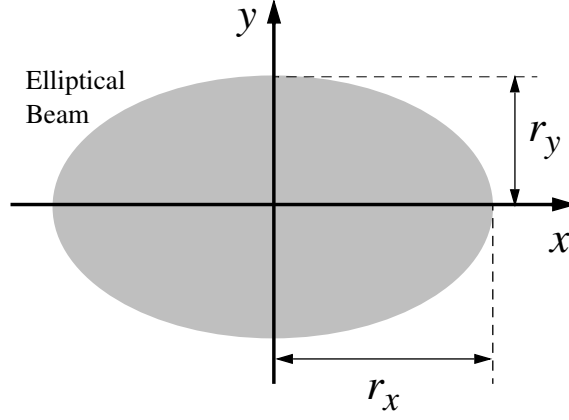


FIG. 1: Transverse cross section of an elliptical beam centered at $x = y = 0$ with envelope radii r_x and r_y along the x - and y -axes and uniform charge density within the ellipse.

of negligible beam space-charge, $Q \rightarrow 0$ in Eq. (1), and the particle moves solely in response to the applied focusing forces of the lattice.

For a uniform density elliptical beam, the envelope radii r_x and r_y are connected to statistical moments of the distribution by

$$\begin{aligned} r_x &= 2\sqrt{\langle x^2 \rangle_{\perp}}, \\ r_y &= 2\sqrt{\langle y^2 \rangle_{\perp}}, \end{aligned} \quad (3)$$

where $\langle \dots \rangle_{\perp}$ denotes a transverse statistical average over the beam phase-space. Differentiating Eq. (3) with respect to s and employing the equations of motion (1) yields coupled ordinary differential equations describing the evolution of the envelope radii $r_x(s)$ and $r_y(s)$ [1, 2, 7]

$$r_j''(s) + \kappa_j(s)r_j(s) - \frac{2Q}{r_x(s) + r_y(s)} - \frac{\varepsilon_j^2}{r_j^3(s)} = 0. \quad (4)$$

Here and henceforth j ranges over both transverse coordinates x and y , and

$$\begin{aligned} \varepsilon_x &= 4[\langle x^2 \rangle_{\perp} \langle x'^2 \rangle_{\perp} - \langle xx' \rangle_{\perp}^2]^{1/2}, \\ \varepsilon_y &= 4[\langle y^2 \rangle_{\perp} \langle y'^2 \rangle_{\perp} - \langle yy' \rangle_{\perp}^2]^{1/2} \end{aligned} \quad (5)$$

are the rms emittances which provide statistical measures of the beam phase-space area projections in the x - x' and y - y' phase-spaces. For charge distributions that are constant on nested elliptical surfaces, the envelope equations (4) are valid with evolving emittances and can be solved for the evolution of $r_j(s)$ provided consistent emittance evolutions are employed [6]. In this situation the envelope equations are often referred to as the rms envelope equations and can be applied to a wide variety of nonuniform laboratory beams through an “equivalence” to a uniform density beam with equal second-order statistical moments [2, 5, 6]. For the case of a KV distribution with uniform space-charge, the ε_j are constants and the envelope equations are referred to as the KV envelope equations [1–3]. The corresponding self-consistent KV distribution under a Vlasov model is singular and unphysical and has numerous higher-order collective instabilities internal to the beam [4, 9]. However, in cases of reasonably smooth initial beam distributions and a transport channel tuned for applied focusing linearity and a lack of instabilities, the emittance evolutions will be small, the linear space-charge model will be accurate, and the KV envelope model with constant emittances can be reliably applied.

For a particular focusing lattice [i.e., specified focusing functions $\kappa_j(s)$] and beam parameters (Q and ε_j), the KV envelope equations (4) are typically integrated from an initial condition (i.e., specified r_j and r_j' at $s = s_i$) to solve for the envelope evolution. In many cases we will take $\varepsilon_x = \varepsilon_y \equiv \varepsilon = \text{const}$ corresponding to a beam with isotropic transverse temperature (on average) and negligible emittance evolution propagating in a linear transport channel without bends, dispersion, and edge-focusing.

B. Periodic transport channels and beam matching

In a periodic transport lattice, applied focusing elements are arranged in a periodic sequence with lattice period L_p and lattice focusing functions $\kappa_j(s)$ satisfying

$$\kappa_j(s + L_p) = \kappa_j(s). \quad (6)$$

The matched beam envelope is the solution to the KV envelope equations (4) in a periodic transport where the envelope radii $r_j(s)$ are also periodic functions with period of the lattice, i.e., $r_j(s) = r_{jm}(s)$ with

$$r_{jm}(s + L_p) = r_{jm}(s). \quad (7)$$

For specified focusing functions $\kappa_j(s)$, beam perveance Q , and emittances ε_j , this is equivalent to requiring that r_j and r'_j satisfy specific initial conditions at $s = s_i$ when the envelope equations (4) are integrated as an initial value problem. Required initial conditions will change with the phase of s_i within the lattice period. The matched envelope solution is important because it is believed to have minimum radial excursions in the transport channel relative to all other possible envelope evolutions[10], thereby allowing use of more radially compact transport channels.

Although formulations in the following parts of this section apply for arbitrary periodic focusing functions $\kappa_j(s)$, in Secs. III–V we analyze special classes of (a) continuous, (b) periodic solenoidal, and (c) periodic quadrupole doublet focusing lattices described below with $\kappa_j(s)$ that are piecewise constant, corresponding to so-called hard-edge or square-edge models. These three choices are representative of broad classes of lattices used in practical applications and can guide analysis of more complicated lattices. Examples of matched envelope solutions will be presented for each class of lattice in Secs. III–V. These hard-edge models can be applied to a wide range of periodic solenoid and quadrupole lattices with fringe fields where the $\kappa_j(s)$ vary smoothly in s by using equivalent hard-edge replacement prescriptions (see Appendix A).

(a) *Continuous focusing*, with equal and constant focusing in each plane [see Fig. 2(a)][2]. In this case,

$$\kappa_x(s) = \kappa_y(s) = k_{\beta 0}^2 = \text{const} > 0. \quad (8)$$

Continuous focusing is equivalent to a partially neutralizing, non-interacting background of charges and is commonly used to simply estimate the average focusing properties of periodic lattices in rapid design estimates. Here, $k_{\beta 0}$ is the wavenumber of particle oscillations in the absence of space-charge (see Sec. II D). The choice of “lattice period” L_p for continuous focusing is arbitrary.

(b) *Solenoidal focusing*, produced by a magnetic field $\mathbf{B}(s) = -[B'_z(s)/2](x\hat{\mathbf{x}} + y\hat{\mathbf{y}}) + B_z(s)\hat{\mathbf{z}}$ with period L_p [see Fig. 2(b)][2]. In this case,

$$\kappa_x(s) = \kappa_y(s) \equiv \kappa(s) = \left[\frac{qB_z(s)}{2m\gamma_b\beta_b c} \right]^2. \quad (9)$$

Here, the envelope equations (4) must be interpreted in a local rotating “Larmor” frame in the sense shown in Appendix B. In analyses of solenoidal focused systems, we will assume that all calculations carried out in the Larmor frame unless otherwise noted. We define a hard-edge lattice where the solenoids have axial length ηL_p with $\kappa = \hat{\kappa} = \text{const} > 0$ within the solenoid and zero outside and the solenoids are separated by axial drifts of length $d = (1 - \eta)L_p$. Here, $\eta \in (0, 1]$ is the occupancy factor of the solenoid in the lattice period. In the Larmor frame, solenoidal focusing is equivalent to continuous focusing in the limit $\eta \rightarrow 1$.

(c) *Quadrupole doublet focusing* in an alternating gradient lattice with period L_p [see Fig. 2(c)][2]. In this case,

$$\kappa_x(s) = -\kappa_y(s) \equiv \kappa_q(s). \quad (10)$$

The quadrupole focusing fields are commonly derived either from electrostatic or magnetostatic lenses. In terms of a simple 2D field model, the focusing strength for electric lenses can be expressed as

$$\kappa_q = \frac{1}{[B\rho]} \frac{dE_x}{dx}, \quad (11)$$

where $[B\rho] \equiv \gamma_b\beta_b mc/q$ is the particle rigidity and dE_x/dx is the (generally s -varying) linear quadrupole field gradient of the electric field. Similarly, the focusing strength for magnet lenses can be expressed as

$$\kappa_q = \frac{1}{[B\rho]\beta_b c} \frac{dB_x}{dy}, \quad (12)$$

where dB_x/dy is the (generally s -varying) linear quadrupole field gradient of the magnetic field. We define a hard-edge doublet lattice where the focusing ($\kappa_q > 0$ for focusing in x) and defocusing ($\kappa_q < 0$) quadrupoles have axial length $\eta L_p/2$ with $\kappa_q = \pm \hat{\kappa}_q$ with $\hat{\kappa}_q = \text{const}$ within the quadrupoles and zero outside, and are separated by (generally unequal) axial drifts of length $d_1 = \alpha(1-\eta)L_p$ and $d_2 = (1-\alpha)(1-\eta)L_p$. Here, $\eta \in (0, 1]$ is the quadrupole occupancy factor in the lattice period, and $\alpha \in [0, 1]$ is a syncopation factor that measures how close the focusing and defocusing quadrupoles are to each other in the lattice period. For the special case of $\alpha = 1/2$ corresponding to a symmetric FODO lattice, the drifts are equal [$d_1 = d_2 = (1-\eta)L_p/2$] and the lenses are equally spaced. For $\alpha \neq 1/2$, the lattice is called syncopated. Without loss of generality, we restrict analysis to $0 \leq \alpha \leq 1/2$ because values of α with $1/2 \leq \alpha \leq 1$ can be mapped to the range $0 \leq \alpha \leq 1/2$ by relabeling lattice quantities.

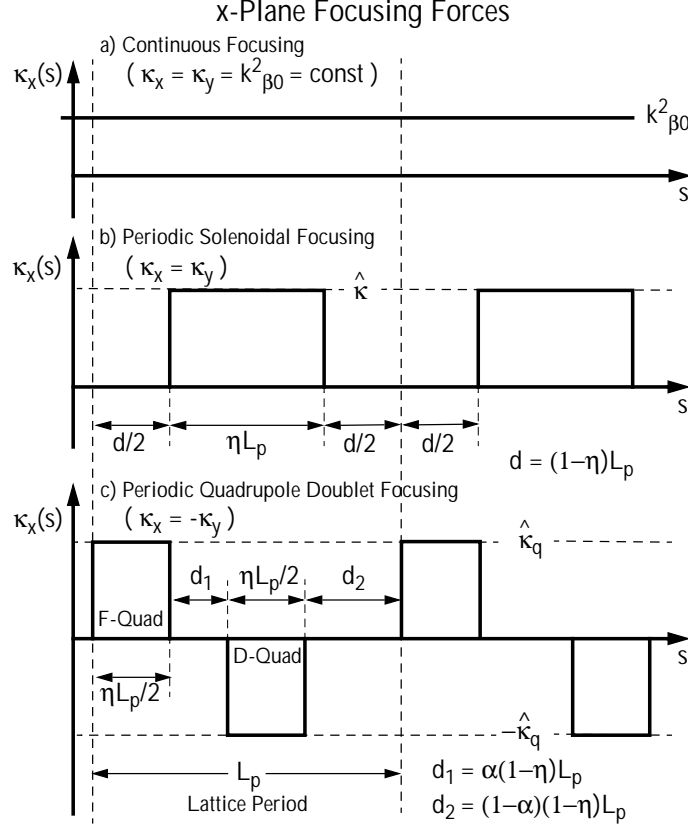


FIG. 2: Linear focusing functions for (a) continuous focusing, (b) periodic solenoidal focusing, and (c) periodic quadrupole doublet focusing.

C. Characteristic Envelope Responses

The envelope evolution in the periodic, hard-edge focusing lattices described in Sec. II B can be interpreted in terms of the sequential response of the envelope to the focusing action of optical elements followed by free-drift expansions without focusing ($\kappa_j = 0$).

No general analytical solutions to the envelope evolution within hard-edge solenoidal or quadrupole optics are known for arbitrary values of Q and ε_j . Some simplifications can be made using the envelope Hamiltonian as a constant of the motion within a particular optical element, but full integrations of the envelope trajectories $r_j(s)$ are not known. However, the essential effect of the optics can be simply understood in the thin-lens limit where $\eta \rightarrow 0$ while adjusting the focusing strength such that the desired net particle focusing (measured by σ_{0j} , see Sec. II D) is produced. This is effected by taking

$$\kappa_j(s) = \frac{1}{f} \delta(s - s_o), \quad (13)$$

where $\delta(s)$ is the Dirac delta-function, $f = \text{const}$ is the thin-lens focal length, and $s = s_o$ is the axial location of the equivalent model optical impulse. In this thin-lens limit, it follows from Eqs. (4) and (13) that the action of the optic is to transform the envelope as

$$\begin{pmatrix} r_j \\ r'_j \end{pmatrix} \Big|_{s_o^\pm} = \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} \begin{pmatrix} r_j \\ r'_j \end{pmatrix} \Big|_{s_o^\mp}, \quad (14)$$

where $|_{s_o^\pm}$ denotes the limit $\lim_{s \rightarrow s_o}$ from above and below $s = s_o$. For solenoidal and quadrupoles that are focusing in the j -plane, $f > 0$, whereas for defocusing quadrupoles in the j -plane, $f < 0$.

General analytical solutions for the envelope evolution in drift regions are also unknown, though some simplifications can be made using envelope Hamiltonian invariants in particular drift regions. However, the range of drift envelope evolution can be analytically understood in the extremes of an emittance-dominated beam with $Q = 0$ and a space-charge dominated beam with $\varepsilon_j = 0$. First, in the limit of a emittance-dominated beam, $Q = 0$, and the j -plane envelope equation (4) reduces to

$$r_j'' - \frac{\varepsilon_j^2}{r_j^3} = 0. \quad (15)$$

This equation is straightforward to integrate using the constancy of the envelope Hamiltonian, $r_j'^2/2 + \varepsilon_j^2/(2r_j^2) = \text{const}$. After some manipulations we obtain

$$r_j(s) = r_j(s_i) \sqrt{1 + \frac{2r'_j(s_i)}{r_j(s_i)}(s - s_i) + \left[1 + \frac{r_j^2(s_i)r_j'^2(s_i)}{\varepsilon_j^2}\right] \frac{\varepsilon_j^2}{r_j^4(s_i)}(s - s_i)^2}. \quad (16)$$

Here, $s = s_i$ is the initial condition where $r_j = r_j(s_i)$ and $r'_j = r'_j(s_i)$. In the opposite limit of a space-charge dominated beam, $\varepsilon_j = 0$, the envelope equations can be cast in decoupled form using sum and difference coordinates defined as $r_\pm = (r_x \pm r_y)/2$ to give

$$\begin{aligned} r_+'' - \frac{Q}{r_+} &= 0, \\ r_-'' &= 0. \end{aligned} \quad (17)$$

The constancy of the envelope Hamiltonian, $r_+^2/2 - Q \ln r_+ = \text{const}$ can be employed to simplify integration of the equation for r_+ and the equation for r_- is trivially integrable. We obtain (see Appendix C)

$$\begin{aligned} r_+(s) &= r_+(s_i) \exp \left(-\frac{r_+^2(s_i)}{2Q} + \left[\text{erfi}^{-1} \left\{ \text{erfi} \left[\frac{r'_+(s_i)}{\sqrt{2Q}} \right] + \sqrt{\frac{2Q}{\pi}} e^{\frac{r_+^2(s_i)}{2Q}} \frac{(s - s_i)}{r_+(s_i)} \right\} \right]^2 \right), \\ r_-(s) &= r_-(s_i) + r'_-(s_i)(s - s_i). \end{aligned} \quad (18)$$

Here, $\text{erfi}(z) = \text{erf}(iz)/i = (2/\sqrt{\pi}) \int_0^z dt \exp(t^2)$ is the imaginary error function, $i \equiv \sqrt{-1}$, and notation on initial conditions is analogous to that employed in Eq. (16). An alternative form of the solution for r_+ has been presented by Humphries[11].

To contrast these two limiting free-drift solutions, the envelope expansions $r_x(s)/r_x(s_i)$ and $r_+(s)/r_\pm(s_i)$ given by Eqs. (16) and (18) are plotted in Fig. 3 for equal initial forces $Q/r_+(s_i) = \varepsilon_x/r_x^3(s_i)$ and zero initial angles. The space-charge dominated expansion is more rapid due to the $\sim 1/r_+$ expansion force being larger than the $\sim 1/r_x^3$ expansion force at large radii.

D. Single-particle phase advances

Because it is useful to employ single-particle phase advances to parameterize matched solutions to the KV envelope equations (4), we review these phase advances here in order to define notations employed and summarize results needed later.

The solution to the linear x -equation of motion (1) can be expressed in terms of a transfer map as[12, 13]

$$\begin{pmatrix} x(s) \\ x'(s) \end{pmatrix} = \mathbf{M}_x(s|s_i) \cdot \begin{pmatrix} x(s_i) \\ x'(s_i) \end{pmatrix}, \quad (19)$$

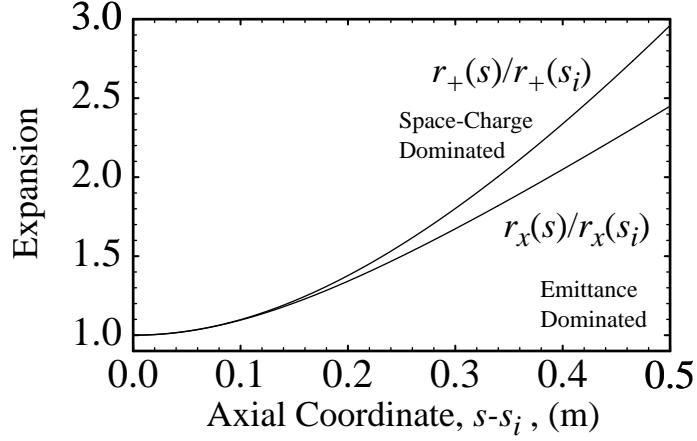


FIG. 3: Scaled envelope free-expansions $r_x(s)/r_x(s_i)$ and $r_+(s)/r_+(s_i)$ plotted versus axial coordinate $s - s_i$. Curves correspond to the emittance-dominated ($Q = 0$) and space-charge dominated ($\varepsilon_x = 0$) limits given by Eqs. (16) and (18). Initial coordinates at $s = s_i$ correspond to $Q/r_+(s_i) = \varepsilon_x/r_x^3(s_i)$, $Q = 10^{-3}$, $r_x(s_i) = r_+(s_i) = 0.01$ m, and $r'_x(s_i) = r'_+(s_i) = 0$.

where $\mathbf{M}_x(s|s_i)$ denotes the 2×2 transfer matrix from the initial x -plane particle phase-space coordinates at axial coordinate $s = s_i$ to the phase-space coordinates at s . An analogous equation holds for the y -plane orbit. An eigenvalue analysis of $\mathbf{M}_j(s|s_i)$ shows that orbit stability corresponds to

$$\frac{1}{2} |\text{Tr } \mathbf{M}_j(s_i + L_p|s_i)| < 1, \quad (20)$$

and that $\text{Tr } \mathbf{M}_j(s_i + L_p|s_i)$ is independent of the initial axial coordinate s_i .

A stable orbit of the particle satisfying Eq. (1) can be expressed in terms of the phase-amplitude formulation as [12, 13]

$$\begin{aligned} x(s) &= A_x w_x(s) \cos[\psi_x(s)], \\ y(s) &= A_y w_y(s) \cos[\psi_y(s)], \end{aligned} \quad (21)$$

where $A_j = \text{const}$ and the amplitude and phase functions w_j and ψ_j satisfy

$$\begin{aligned} w_j'' + \kappa_j w_j - \frac{2Qw_j}{(r_x + r_y)r_j} - \frac{1}{w_j^3} &= 0, \\ \psi_j' &= \frac{1}{w_j^2}. \end{aligned} \quad (22)$$

For a periodic lattice with $\kappa_j(s + L_p) = \kappa_j(s)$, without loss of generality, w_j can be taken to be the positive, real solution to the amplitude equation satisfying $w_j(s + L_p) = w_j(s)$. Comparing the amplitude equation (22) with the envelope equation (4) for a matched beam, we observe that r_{jm} and w_j are related as

$$r_{jm} = \sqrt{\varepsilon_j} w_j. \quad (23)$$

The phase advance σ_j of the orbit through one lattice period can then unambiguously be defined by integrating $\psi_j' = 1/w_j^2$ to yield

$$\sigma_j = \psi_j(s_i + L_p) - \psi_j(s_i) = \varepsilon_j \int_{s_i}^{s_i + L_p} \frac{ds}{r_{jm}^2(s)}, \quad (24)$$

independent of s_i . Analysis of the transfer matrix elements then shows that

$$\cos \sigma_j = \frac{1}{2} \text{Tr } \mathbf{M}_j(s_i + L_p|s_i). \quad (25)$$

Direct application of this formula to calculate σ_j requires proper branch identification.

For the case of an isotropic beam with $\varepsilon_x = \varepsilon_y \equiv \varepsilon$ and the three classes of lattices outlined in Sec. II B, the phase advances of the x - and y -orbits will be equal, i.e., $\sigma_x = \sigma_y$. In this symmetric situation, we will not distinguish between σ_x and σ_y , and we denote $\sigma_x = \sigma_y \equiv \sigma$.

In the limit of zero space-charge ($Q \rightarrow 0$), we denote the phase advance σ_j calculated from Eq. (24) as

$$\sigma_{0j} \equiv \lim_{Q \rightarrow 0} \sigma_j. \quad (26)$$

The so-called undepressed phase-advance σ_{0j} measures the phase advance of particles in response to the linear applied focusing fields and provides a measure of the focusing strength of the lattice. For periodic focusing lattices with $\kappa_x = \kappa_y$ or $\kappa_x = -\kappa_y$, $\sigma_{0x} = \sigma_{0y}$, and we denote $\sigma_{0x} = \sigma_{0y} \equiv \sigma_0$. Equations (1) and (25) can be employed to relate $\sigma_0 = \lim_{Q \rightarrow 0} \sigma$ to the lattice focusing functions κ_j .

For the three classes of lattices described in Sec. II B, we summarize expressions for σ_0 . First, for the continuous focusing lattice, $\kappa_x = \kappa_y = k_{\beta 0}^2 = \text{const}$ and there is no strict periodicity. However, for purposes of comparisons to periodic systems (see Fig. 2), we can define the undepressed particle phase advance σ_0 over an arbitrary “period” L_p by

$$k_{\beta 0}^2 = \left(\frac{\sigma_0}{L_p} \right)^2. \quad (27)$$

For the hard-edge solenoidal and quadrupole doublet focusing channels illustrated in Fig. 2, it can be shown that

$$\cos \sigma_0 = \cos(2\Theta) - \frac{1-\eta}{\eta} \Theta \sin(2\Theta) \quad (28)$$

for the solenoidal channel with $\Theta \equiv \sqrt{\hat{\kappa}} L_p / 2$, and

$$\begin{aligned} \cos \sigma_0 = & \cos \Theta \cosh \Theta + \frac{1-\eta}{\eta} \Theta (\cos \Theta \sinh \Theta - \sin \Theta \cosh \Theta) \\ & - 2\alpha(1-\alpha) \frac{(1-\eta)^2}{\eta^2} \Theta^2 \sin \Theta \sinh \Theta \end{aligned} \quad (29)$$

for the quadrupole channel with $\Theta \equiv \sqrt{|\hat{\kappa}_q|} L_p / 2$. For any periodic channel with specified focusing functions $\kappa_j(s)$ (possibly including fringe variations), particular values of σ_0 can be produced by scaling the amplitude of the focusing functions, i.e., $\kappa_x \rightarrow k\kappa_x$ and $\kappa_y \rightarrow k\kappa_y$ with $k = \text{const}$ constrained by σ_0 . For example, consider the hard-edge quadrupole lattice. At specified lattice period L_p , occupancy η , and syncopation factor α , Eq. (29) constrains the value of the focusing strength $|\hat{\kappa}_q|$ in terms of σ_0 .

The thin-lens limit of Eqs. (28) and (29) can be explored by setting $\hat{\kappa} = \eta/(fL_p)$ for solenoids and $\hat{\kappa}_q = \eta/(fL_p)$ for quadrupoles and then taking the limit $\eta \rightarrow 0$. This gives

$$\cos \sigma_0 = \begin{cases} 1 - \frac{1}{2} \frac{L_p}{f}, & \text{thin-lens solenoids,} \\ 1 - 2\alpha(1-\alpha) \left(\frac{L_p}{f} \right)^2, & \text{thin-lens quadrupoles.} \end{cases} \quad (30)$$

These results can also be derived directly from a transfer matrix approach of the undepressed orbits using Eq. (25) in the limit $Q \rightarrow 0$ to show that

$$\begin{aligned} \cos \sigma_0 &= \frac{1}{2} \text{Tr} \begin{bmatrix} 1 & L_p \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} = 1 - \frac{1}{2} \frac{L_p}{f}, \\ \cos \sigma_0 &= \frac{1}{2} \text{Tr} \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} \begin{bmatrix} 1 & \alpha L_p \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{bmatrix} \begin{bmatrix} 1 & (1-\alpha)L_p \\ 0 & 1 \end{bmatrix} = 1 - 2\alpha(1-\alpha) \left(\frac{L_p}{f} \right)^2, \end{aligned}$$

for solenoidal and quadrupole channels, respectively.

When $\sigma_{0x} = \sigma_{0y}$ and $\sigma_x = \sigma_y$, the ratio of space-charge depressed to undepressed phase advances σ/σ_0 provides a convenient, normalized measure of space-charge intensity which we call the space-charge depression. For a fixed value of σ_0 , the limit $\sigma/\sigma_0 \rightarrow 0$ corresponds to a cold-beam at the space-charge limit with zero emittance (i.e., $Q \neq 0$ and $\varepsilon = 0$, or $Q \rightarrow \infty$ for finite ε), and the limit $\sigma/\sigma_0 \rightarrow 1$ corresponds to an emittance-dominated beam with zero space-charge effects (i.e., $\varepsilon \neq 0$ with $Q = 0$, or $\varepsilon \rightarrow \infty$ for finite Q). Stability properties of the envelope equations (4) will be characterized in terms of σ_0 and σ/σ_0 for stable undepressed orbits with $\sigma_0 \in (0, \pi)$ and the full range of space-charge intensity $\sigma/\sigma_0 \in [0, 1]$.

Matched envelopes can also exist in periodic transport channels for ranges (bands) of σ_{0j} with $\sigma_{0j} > \pi$. These bands will correspond to higher focusing strength (e.g., larger $\hat{\kappa}$ for the hard-edge solenoidal lattice) and will be

separated from the stable range $\sigma_{0j} \in (0, \pi)$ by so-called stop bands where $(1/2)|\text{Tr } \mathbf{M}_j(s_i + L_p|s_i)| > 1$ and the single-particle orbits are unstable. Successive stable bands will have narrower ranges of σ_{0j} and the first stop band begins at $\sigma_{0j} = \pi$. Higher stable bands tend to be more sparse and narrower for quadrupole focusing as opposed to solenoidal focusing, as can be seen from analyzing regions where $|\cos \sigma_0| < 1$ from Eqs. (28) and (29). This occurs because stronger quadrupole focusing in alternating gradient lattices tends to produce large excursions within the defocusing quadrupoles, leading to narrow parameter bands for stable orbit bundles. Higher stable bands in solenoidal channels are wider than for quadrupole channels because such systems are focusing in all planes. However, contrary to assertions by some authors[14–16], we find that machine operation in higher bands of stability for solenoidal focusing will not, in general, prove advantageous. This follows because the higher bands require significantly larger focusing strengths, while for fixed beam perveance Q , these stronger optics also result in matched beams with larger envelope excursions than for $\sigma_{0j} < \pi$, leading to larger apertures needed for beam confinement[17]. Moreover, matching the beam envelope to transport at high phase advances from lower phase advances can prove problematic. Because of these problems we only consider $\sigma_{0j} \in (0, \pi)$ in this paper. Contrary to $\sigma_{0j} > \pi$, we find that for fixed Q in periodic focusing lattices with high degrees of symmetry, that the matched beam envelope generally is radially more compact for higher values of σ_{0j} in the range $\sigma_{0j} \in (0, \pi)$ [18, 19].

E. Scaled envelope equations and system parameters

Solutions for the envelope equations (4) can be parameterized in terms of the lattice focusing functions κ_j , the perveance Q , and the emittances $\varepsilon_x = \varepsilon_y = \varepsilon$. For example, in the hard-edge solenoid and quadrupole doublet lattices defined in Sec. II B, the functions κ_j are described in terms of the lattice period L_p , the occupancy η , the focusing strength $\hat{\kappa}$ (solenoids) or $\hat{\kappa}_q$ (quadrupoles), and the syncopation parameter α (quadrupoles only). Thus for hard-edge solenoids, five “direct” parameters (L_p , η , $\hat{\kappa}$, Q , and ε) can be employed to specify the matched beam solution, while for the hard-edge quadrupole doublet six direct parameters (L_p , η , α , $\hat{\kappa}_q$, Q , and ε) can be employed. Other choices of hard-edge solenoidal and quadrupole lattices yield similar direct parameters. Focusing lattices including axial fringe field models of the elements introduce additional direct parameters that replace the hard-edge occupancy η and focusing strengths $\hat{\kappa}$ and $\hat{\kappa}_q$.

Rather than employing the direct parameters, matched beam solutions of the envelope equations can be described with a reduced number of dimensionless parameters[20, 21]. The particle phase advance parameters σ_0 and σ (or σ_0 and σ/σ_0). This procedure can be carried out by introducing scaled coordinates for continuous focusing, or general solenoidal and quadrupole transport lattices as follows. For equal emittances and finite perveance (i.e., $\varepsilon_x = \varepsilon_y \equiv \varepsilon$ and $Q > 0$), the envelope equations (4) can be expressed for the three classes of lattices as

$$\frac{d^2}{dS^2} R_j + \xi_j F(S; \sigma_0, \{\mathcal{S}\}) R_j - \frac{1}{R_x + R_y} - \frac{\Gamma^2}{R_j^3} = 0. \quad (31)$$

Here, $S = s/L_p$ is a dimensionless axial coordinate that increases by unity as the beam advances over a lattice period L_p ,

$$R_j = \frac{r_j}{\sqrt{2Q}L_p}, \quad (32)$$

are dimensionless scaled envelope radii, for continuous or solenoidal focusing $\xi_j = 1$, for quadrupole focusing $\xi_x = +1$ and $\xi_y = -1$, $F(S; \sigma_0, \{\mathcal{S}\})$ is a scaled focusing function that depends on S , σ_0 , and a set of “shape” parameters $\{\mathcal{S}\}$ of the focusing function, and

$$\Gamma = \frac{\varepsilon}{2QL_p} \quad (33)$$

is a dimensionless parameter measuring relative space-charge intensity. For a matched beam envelope (i.e., $r_j = r_{jm}$), the parameter Γ can be related to the depressed particle phase advance σ through Eq. (24) as

$$\sigma = \Gamma \int_0^1 \frac{dS}{R_j^2(S)}. \quad (34)$$

The parameters of the scaled envelope equations (31) are σ_0 , the shape parameters $\{\mathcal{S}\}$ which describe the action of the applied focusing forces on a single-particle, and the dimensionless parameter Γ defined in Eq. (34), or alternatively to Γ , σ or σ/σ_0 .

Specific examples of the scaled focusing function $F(S; \sigma_0, \{\mathcal{S}\})$ for the hard-edge solenoidal and quadrupole lattices described in Sec. II B clarify the forms given in Eqs. (31)–(34). For the solenoidal lattice, we take $F(S; \sigma_0, \{\mathcal{S}\}) = F(S; \sigma_0, \eta) = [L_p^2 \hat{\kappa}] [\kappa_x(s)/\hat{\kappa}]$ where $[\kappa_x(s)/\hat{\kappa}]$ is a function of S and η , and $[L_p^2 \hat{\kappa}]$ is a function of σ_0 and η through an application of the phase advance equation of constraint (28). Similarly, for the quadrupole lattice, we take $F(S; \sigma_0, \{\mathcal{S}\}) = F(S; \sigma_0, \eta, \alpha) = [L_p^2 |\hat{\kappa}_q|] [\kappa_x(s)/|\hat{\kappa}_q|]$, where $[\kappa_x(s)/|\hat{\kappa}_q|]$ is a function of S , η , and α , and $[L_p^2 |\hat{\kappa}_q|]$ is a function of σ_0 , η , and α through an application of the phase advance equation of constraint (29). For the special case of continuous focusing, there are no shape parameters (i.e., $\{\mathcal{S}\} = \emptyset$), and the choice of lattice period L_p entering in σ_0 and σ is arbitrary. Hence, matched solutions in continuous focusing can be regarded as a function solely of σ/σ_0 (see also Sec. III A).

From the results above, it follows that the matched beam envelope in the hard-edge solenoidal transport lattice considered can be described in terms of three parameters: the magnet occupancy η , the undepressed particle phase advance σ_0 , and the space-charge depression σ/σ_0 rather than five direct parameters[20]; whereas matched solutions to the quadrupole doublet lattice can be described in terms of four parameters: η , σ_0 , σ/σ_0 , plus the syncopation factor α ($\alpha \equiv 1/2$ for the special case of a symmetric FODO lattice) rather than the five direct parameters[21]. In subsequent analyses we will exploit this reduction by specifying matched beam solutions in terms of these reduced parameter sets. However, to maintain direct connection the usual form of the envelope equations we will carry out most analyses in terms of conventional dimensioned envelope coordinates and direct parameters.

F. Small amplitude perturbations about the matched beam envelope

To analyze the evolution of perturbations about the matched beam envelope, we resolve the envelope coordinates r_j evolving according to Eq. (4) from general initial conditions as

$$r_j(s) = r_{jm}(s) + \delta r_j(s). \quad (35)$$

Here, r_{jm} is a matched solution to the envelope equation and δr_j are perturbations about the matched beam envelope. In the small-amplitude limit we require that $|\delta r_j| \ll r_{jm}$ over the range of s analyzed. The envelope perturbations δr_j are typically referred to as mismatch oscillations about the matched beam envelope.

In addition to the perturbations in the envelope coordinates δr_j , we consider additional driving perturbations that can excite the envelope perturbations from the matched beam condition. Specifically, we allow the lattice focusing functions κ_j , the beam perveance Q , and the rms emittances ε_j to vary by making the following substitutions in the envelope equations (4)

$$\begin{aligned} \kappa_j(s) &\rightarrow \kappa_j(s) + \delta \kappa_j(s), \\ Q &\rightarrow Q + \delta Q(s), \\ \varepsilon_j &\rightarrow \varepsilon_j + \delta \varepsilon_j(s). \end{aligned} \quad (36)$$

Here, $\delta \kappa_j(s)$ represent perturbations to the focusing functions $\kappa_j(s)$ used in generating the matched beam envelope, $\delta Q(s)$ with $-Q \leq \delta Q \leq 0$ represents the effect of particles lost outside the beam envelope, and $\delta \varepsilon_j(s)$ with $\varepsilon_j + \delta \varepsilon_j > 0$ model evolutions in the rms emittances. The focusing perturbations $\delta \kappa_j(s)$ need not be periodic and can represent construction and excitation errors in the focusing optics. The long-path trend of the perturbed perveance $\delta Q(s) \leq 0$ will be negative due to halo particles being scraped, but it can locally increase if any halo particles re-enter the core distribution. Similarly, over a long path the emittance perturbations $\delta \varepsilon_j(s)$ will tend to be positive and increasing due to the relaxation of the beam in response to nonlinear applied focusing fields, space-charge nonlinearities, etc., but can locally decrease because rms emittances are statistical measures of phase-space area (e.g., momentary unwrapping of strong “S”-shaped distortions in the particle phase-space, etc.). In the small amplitude regime we require that $\delta Q \ll Q$ and that $\delta \kappa_j$ and $\delta \varepsilon_j$ be small in the sense that they induce small corrections on the particle orbits relative to κ_j and ε_j , respectively. Higher-order theories outside the scope of the envelope model are generally necessary to calculate $\delta Q(s)$ and $\delta \varepsilon_j(s)$ for use in this formulation.

Inserting Eqs. (35) and (36) into the envelope equation (4) and neglecting all terms of order δ^2 and higher yields the linearized perturbation equations

$$\begin{aligned} \delta r_j'' + \kappa_j \delta r_j + \frac{2Q}{(r_{xm} + r_{ym})^2} (\delta r_x + \delta r_y) + \frac{3\varepsilon_j^2}{r_{jm}^4} \delta r_j \\ = -r_{jm} \delta \kappa_j + \frac{2}{r_{xm} + r_{ym}} \delta Q + \frac{2\varepsilon_j^2}{r_{jm}^3} \delta \varepsilon_j. \end{aligned} \quad (37)$$

These equations can be equivalently expressed in first-order matrix form as

$$\frac{d}{ds}\delta\mathbf{R} + \mathbf{K} \cdot \delta\mathbf{R} = \delta\mathbf{P}, \quad (38)$$

where

$$\delta\mathbf{R} = \begin{pmatrix} \delta r_x \\ \delta r'_x \\ \delta r_y \\ \delta r'_y \end{pmatrix} \quad (39)$$

is a vector of perturbed envelope phase-space coordinates,

$$\mathbf{K} = \begin{pmatrix} 0 & -1 & 0 & 0 \\ k_{xm} & 0 & k_{0m} & 0 \\ 0 & 0 & 0 & -1 \\ k_{0m} & 0 & k_{ym} & 0 \end{pmatrix} \quad (40)$$

with

$$k_{0m} = \frac{2Q}{(r_{xm} + r_{ym})^2}, \quad (41)$$

$$k_{jm} = \kappa_j + 3\frac{\varepsilon_j^2}{r_{jm}^4} + k_{0m},$$

is a 4×4 matrix with periodic s -dependence of period L_p , and

$$\delta\mathbf{P} = \begin{pmatrix} 0 \\ -\delta\kappa_x + 2\frac{\delta Q}{r_{xm} + r_{ym}} + 2\frac{\varepsilon_x \delta\varepsilon_x}{r_{xm}^3} \\ 0 \\ -\delta\kappa_y + 2\frac{\delta Q}{r_{xm} + r_{ym}} + 2\frac{\varepsilon_y \delta\varepsilon_y}{r_{ym}^3} \end{pmatrix} \quad (42)$$

is a vector of driving perturbations. The solution to Eq. (38) can be expressed as

$$\delta\mathbf{R} = \delta\mathbf{R}_h + \delta\mathbf{R}_p, \quad (43)$$

where $\delta\mathbf{R}_h$ is the general solution to the homogeneous equation (38) with $\delta\mathbf{P} = 0$, and $\delta\mathbf{R}_p$ is any particular solution for the full equation with general $\delta\mathbf{P}$. Henceforth, the homogeneous and particular components of the solution will be analyzed in turn without explicitly distinguishing them to avoid cumbersome notation.

For the special cases of continuous ($\kappa_x = \kappa_y = \kappa_{\beta 0}^2 = \text{const}$) and periodic solenoidal focusing ($\kappa_x = \kappa_y = \kappa$) channels with a round beam equilibrium ($\varepsilon_x = \varepsilon_y = \varepsilon$ and $r_{xm} = r_{ym} = r_m$), considerable simplification results by resolving the envelope perturbations into sum and difference variables as

$$\delta r_{\pm} \equiv \frac{\delta r_x \pm \delta r_y}{2}. \quad (44)$$

In these cases, the perturbed envelope equations (37) can be expressed as

$$\begin{aligned} \delta r_+'' + \kappa \delta r_+ + \frac{2Q}{r_m^2} \delta r_+ + \frac{3\varepsilon^2}{r_m^4} \delta r_+ &= -r_m \left(\frac{\delta\kappa_x + \delta\kappa_y}{2} \right) + \frac{1}{r_m} \delta Q + \frac{2\varepsilon^2}{r_m^3} \left(\frac{\delta\varepsilon_x + \delta\varepsilon_y}{2} \right), \\ \delta r_-'' + \kappa \delta r_- + \frac{3\varepsilon^2}{r_m^4} \delta r_- &= -r_m \left(\frac{\delta\kappa_x - \delta\kappa_y}{2} \right) + \frac{2\varepsilon^2}{r_m^3} \left(\frac{\delta\varepsilon_x - \delta\varepsilon_y}{2} \right), \end{aligned} \quad (45)$$

and are decoupled. Here, $\kappa = \kappa_{\beta 0}^2$ for continuous focusing. Each of the decoupled equations for δr_{\pm} in Eq. (45) can be cast into matrix form analogous to Eqs. (38)–(43). However, in this case the vectors and matrices will be of dimension 2 rather than dimension 4. From the structure of Eq. (45), note that changes in beam perveance (i.e., $\delta Q \neq 0$) drive only δr_+ and not δr_- , whereas changes in focusing strength ($\delta\kappa_j \neq 0$) and emittance ($\delta\varepsilon_j \neq 0$) can project on δr_+ for in-phase error components in x and y , and δr_- for out of phase errors. Also, due to the additional factor of

$(2Q/r_m^2)\delta r_+$, the restoring force coefficient $\propto \delta r_{\pm}$ is larger in the equation for δr_+ than in the equation for δr_- , and oscillations in δr_+ will be more rapid than oscillations in δr_- for $Q \neq 0$.

The homogeneous solution to the linear equations (38) describes the evolution of normal mode perturbations launched by mismatch in the initial conditions at $s = s_i$ (i.e., $\delta \mathbf{R} \neq 0$ at $s = s_i$), whereas the particular solution describes how mismatch oscillations can be driven by changes in beam and focusing parameters. The normal modes supported by the homogeneous equations have been previously analyzed for both continuous and periodic focusing channels by Struckmeier and Reiser[7]. In this paper, this previous work is extended to carefully identify classes of modes supported over a wide range of system parameters.

The homogeneous solution to Eq. (38) can be expressed in terms of a transfer map as

$$\delta \mathbf{R}(s) = \mathbf{M}_e(s|s_i) \cdot \delta \mathbf{R}(s_i), \quad (46)$$

where $\mathbf{M}_e(s|s_i)$ is a 4×4 matrix that maps the perturbed envelope coordinates $\delta \mathbf{R}$ from an initial axial coordinate $s = s_i$ to position s . Stability and launching conditions of normal modes can be analyzed in terms of eigenvalues and eigenvectors of the transfer map \mathbf{M}_e [12, 13, 22]. The four complex eigenvectors \mathbf{E}_n and eigenvalues λ_n (not to be confused with the line-charge λ) of the envelope transfer matrix through one lattice period $\mathbf{M}_e(s_i + L_p|s_i)$ from an initial condition s_i are defined according to

$$\mathbf{M}_e(s_i + L_p|s_i) \cdot \mathbf{E}_n(s_i) = \lambda_n \mathbf{E}_n(s_i), \quad (47)$$

where $n = 1, 2, 3$, and 4. The overall scale of the eigenvectors \mathbf{E}_n is arbitrary. Without loss of generality, we take all eigenvectors to be normalized according to $\mathbf{E}_n \cdot \mathbf{E}_n^* = 1$, where $*$ denotes complex conjugation. The eigenvalues λ_n are independent of the location of the initial axial coordinate s_i , whereas the eigenvectors $\mathbf{E}_n(s_i)$ vary with the relative location of s_i in the lattice period[22]. Stability in the sense of bounded excursions of perturbations in phase-space correspond to λ_n on the complex unit circle with $|\lambda_n| = 1$ for all n , whereas instability results from any λ_n lying off the complex unit circle (i.e., at least one unstable mode).

Because the envelope perturbation equations are real and Hamiltonian, \mathbf{M}_e is a real symplectic matrix. Consequently, the four eigenvalues λ_n of \mathbf{M}_e occur both as complex conjugate pairs (λ_n, λ_n^*) and reciprocal pairs ($\lambda_n, 1/\lambda_n$) and can be categorized according to four symmetry classes (not counting possible degeneracies) described by Dragt[12, 22]. These classes with associated eigenvalue and eigenvector symmetries are illustrated in Fig. 4. Eigenvalues are expressed in polar form as $\lambda_n = \gamma_n \exp(i\sigma_n)$ with real γ_n and σ_n and the specific labellings in n indicated. Standard analyses[12, 13, 22] show that γ_n is the growth factor of the mode per lattice period with $|\gamma_n| = 1$ corresponding to stable oscillations, and $|\gamma_n| > 1$ and $|\gamma_n| < 1$ corresponding to oscillations with exponential growth and damping, respectively. The number of e -folds that the amplitude of mode oscillations grows per lattice period is $\ln|\gamma_n|$. It is shown later that σ_n is related to the phase advance of the mode oscillations per lattice period. For each of the four classes of eigenvalue symmetries in Fig. 4, two real numbers are needed to describe the four eigenvalues [e.g., σ_1 and σ_2 in case (a)]. In case (a), $|\lambda_n| = 1$ and the eigenvectors corresponding to eigenvalues λ_n and $1/\lambda_n$ are simply related as complex conjugates with $\mathbf{E}_3 = \mathbf{E}_1^*$ and $\mathbf{E}_4 = \mathbf{E}_2^*$. For $|\lambda_n| \neq 1$, some relation between eigenvectors associated with the eigenvalues λ_n and $1/\lambda_n$ (i.e., through operations with $\mathbf{M}_e, \mathbf{M}_e^{-1}$, symplectic group generators, conjugation, etc.) would be useful rather than calculating them both directly from the characteristic equation defining the eigenvalues from Eq. (47). Unfortunately, it was shown that no such relationship exists in cases (c) and (d) [e.g., \mathbf{E}_1 and \mathbf{E}_3 are not simply related in case (c)]. Although such a relationship may in principle exist in case (b), efforts to derive it failed.

In Fig. 4, eigenvalues in case (a) correspond to stability ($\gamma_n = 1$), whereas cases (b)–(d) are unstable. Case (b) is called a “confluent resonance” instability because it represents a parametric resonance between both envelope mode oscillation frequencies and the lattice as evident by the eigenvalue symmetry. Cases (c) and (d) are called “lattice resonance” and “double lattice resonance” instabilities because they represent a half-integer parametric resonance between the focusing structure and one or both mode oscillation frequencies. Transitions between cases lead to degenerate eigenvalues which can result in either linear growth in oscillation amplitude with periods traversed or no instability[22]. Which case the degeneracy falls into requires further analysis and is not addressed in this paper (other than a special case in the thin-lens limit) because the degenerate cases correspond to lower-dimensional surfaces in accessible parameter-space that are launched with probability zero. For the types of lattices in Sec. II B, we find in Secs. III–V that the eigenvalues λ_n fall into cases (a)–(c) and case (d) does not occur.

Any initial envelope perturbation at $s = s_i$ can be expanded in terms of the eigenvectors as

$$\delta \mathbf{R}(s_i) = \sum_{n=1}^4 \alpha_n \mathbf{E}_n(s_i), \quad (48)$$

where the α_n are complex constants subject to $\delta \mathbf{R}(s_i)$ being real. To launch pure envelope modes with specific phase advances and growth factors for each of the eigenvalue classes listed in Fig. 4, it is convenient to resolve the initial

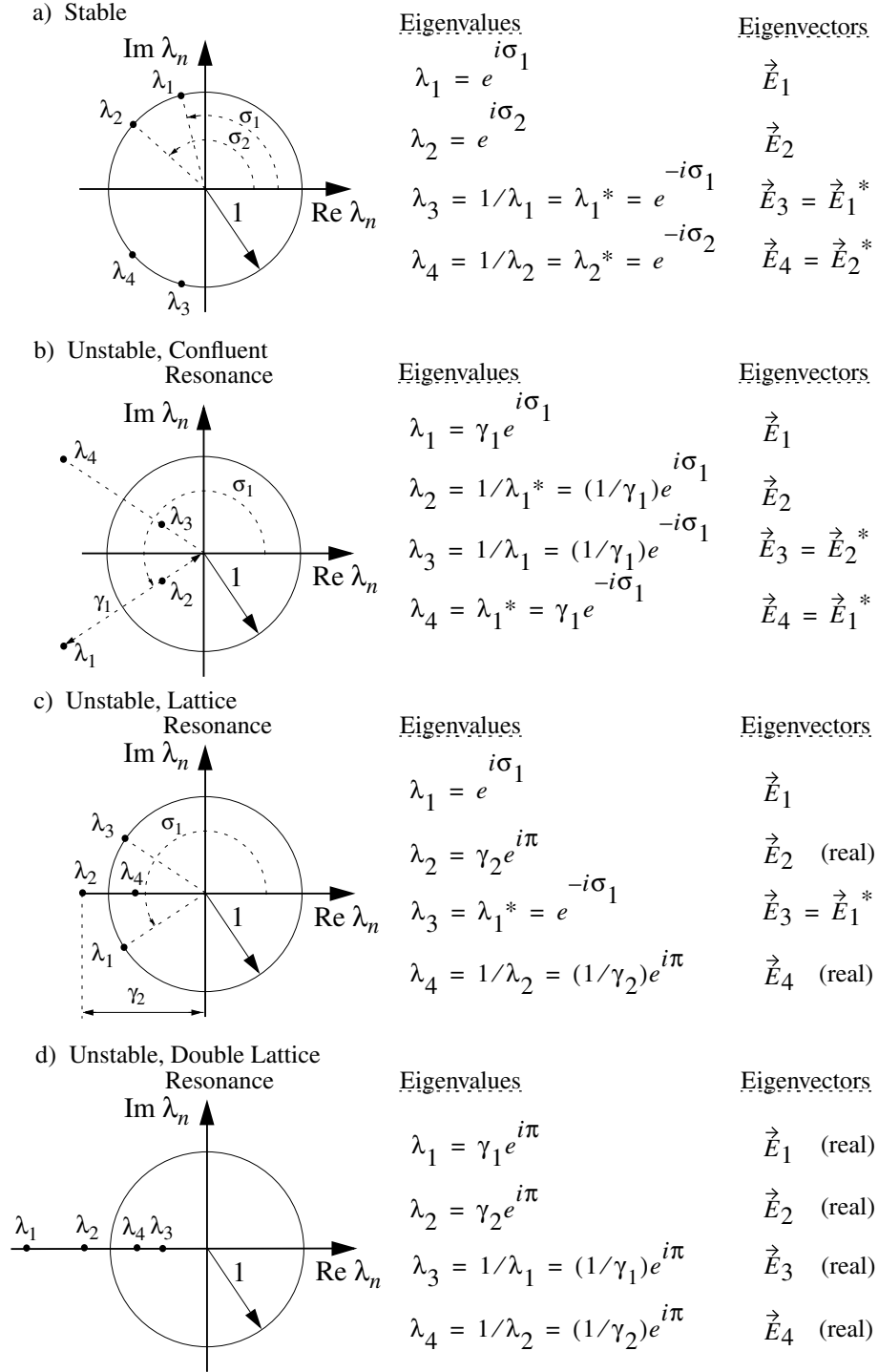


FIG. 4: Four possible classes of symmetries for the four eigenvalues defined by Eq. (47) corresponding to stability in (a), and instability in (b), (c), and (d).

condition $\delta R(s_i) = \delta R_\ell(s_i)$ into pure normal modes as summarized in Table I. Mode structures are illustrated in the table by mappings of the pure mode initial condition through one lattice. The eigenvectors \mathbf{E}_n , and consequently the pure mode launching conditions $\delta \mathbf{R}_\ell(s_i)$, vary with the relative location of the initial condition s_i in the lattice period. Note that cases (a) and (b) in Fig. 4 have two distinct modes, while cases (c) and (d) have three and four distinct modes.

The evolution of the beam mismatch $\delta \mathbf{R}(s)$ can also be interpreted as evolving linear projections of envelope

TABLE I: Launching conditions for distinct normal modes corresponding to the eigenvalue classes illustrated in Fig. 4. Here, A_ℓ and ψ_ℓ are real-valued amplitudes (unnormalized) and phases of mode ℓ ($\ell = 1, 2$, and possibly 3 and 4 under conventions taken), and σ_ℓ and $\gamma_\ell > 1$ are the phase advances and growth factors of the mode over one lattice period. Symbols are abbreviated with $\delta\mathbf{R}_\ell \equiv \delta\mathbf{R}_\ell(s_i)$, $\mathbf{E}_\ell \equiv \mathbf{E}_\ell(s_i)$, and $\mathbf{M}_e \equiv \mathbf{M}_e(s_i + L_p|s_i)$.

Case	Mode	Launching Condition	Lattice Period Advance
(a) Stable	1 - Stable Oscillation	$\delta\mathbf{R}_1 = A_1(e^{i\psi_1}\mathbf{E}_1 + e^{-i\psi_1}\mathbf{E}_1^*)$	$\mathbf{M}_e\delta\mathbf{R}_1(\psi_1) = \delta\mathbf{R}_1(\psi_1 + \sigma_1)$
	2 - Stable Oscillation	$\delta\mathbf{R}_2 = A_2(e^{i\psi_2}\mathbf{E}_2 + e^{-i\psi_2}\mathbf{E}_2^*)$	$\mathbf{M}_e\delta\mathbf{R}_2(\psi_2) = \delta\mathbf{R}_2(\psi_2 + \sigma_2)$
(b) Unstable Confluent Resonance	1 - Exponential Growth	$\delta\mathbf{R}_1 = A_1(e^{i\psi_1}\mathbf{E}_1 + e^{-i\psi_1}\mathbf{E}_1^*)$	$\mathbf{M}_e\delta\mathbf{R}_1(\psi_1) = \gamma_1\delta\mathbf{R}_1(\psi_1 + \sigma_1)$
	2 - Exponential Damping	$\delta\mathbf{R}_2 = A_2(e^{i\psi_2}\mathbf{E}_2 + e^{-i\psi_2}\mathbf{E}_2^*)$	$\mathbf{M}_e\delta\mathbf{R}_2(\psi_2) = (1/\gamma_1)\delta\mathbf{R}_2(\psi_2 + \sigma_1)$
(c) Unstable Lattice Resonance	1 - Stable Oscillation	$\delta\mathbf{R}_1 = A_1(e^{i\psi_1}\mathbf{E}_1 + e^{-i\psi_1}\mathbf{E}_1^*)$	$\mathbf{M}_e\delta\mathbf{R}_1(\psi_1) = \delta\mathbf{R}_1(\psi_1 + \sigma_1)$
	2 - Exponential Growth	$\delta\mathbf{R}_2 = A_2\mathbf{E}_2$	$\mathbf{M}_e\delta\mathbf{R}_2 = -\gamma_2\delta\mathbf{R}_2$
	3 - Exponential Damping	$\delta\mathbf{R}_3 = A_3\mathbf{E}_4$	$\mathbf{M}_e\delta\mathbf{R}_3 = -(1/\gamma_2)\delta\mathbf{R}_3$
(d) Unstable Double Lattice Resonance	1 - Exponential Growth	$\delta\mathbf{R}_1 = A_1\mathbf{E}_1$	$\mathbf{M}_e\delta\mathbf{R}_1 = -\gamma_1\delta\mathbf{R}_1$
	2 - Exponential Growth	$\delta\mathbf{R}_2 = A_2\mathbf{E}_2$	$\mathbf{M}_e\delta\mathbf{R}_2 = -\gamma_2\delta\mathbf{R}_2$
	3 - Exponential Damping	$\delta\mathbf{R}_3 = A_3\mathbf{E}_3$	$\mathbf{M}_e\delta\mathbf{R}_3 = -(1/\gamma_1)\delta\mathbf{R}_3$
	4 - Exponential Damping	$\delta\mathbf{R}_4 = A_4\mathbf{E}_4$	$\mathbf{M}_e\delta\mathbf{R}_4 = -(1/\gamma_2)\delta\mathbf{R}_4$

mismatch onto pure normal modes according to:

$$\delta\mathbf{R}(s) = \begin{cases} A_1[\mathbf{E}_1(s)e^{i\psi_1(s)} + \mathbf{E}_1^*(s)e^{-i\psi_1(s)}] + A_2[\mathbf{E}_2(s)e^{i\psi_2(s)} + \mathbf{E}_2^*(s)e^{-i\psi_2(s)}], & \text{cases (a) and (b),} \\ A_1[\mathbf{E}_1(s)e^{i\psi_1(s)} + \mathbf{E}_1^*(s)e^{-i\psi_1(s)}] + A_2\mathbf{E}_2(s) + A_3\mathbf{E}_4(s), & \text{case (c),} \\ A_1\mathbf{E}_1(s) + A_2\mathbf{E}_2(s) + A_3\mathbf{E}_3(s) + A_4\mathbf{E}_4(s), & \text{case (d),} \end{cases} \quad (49)$$

where A_ℓ and ψ_ℓ are real-valued. This interpretation allows us to unambiguously define that pure mode phase advance σ_ℓ as the change in ψ_ℓ as s advances over one lattice period L_p , thereby providing a concrete branch selection criteria to relate the complex eigenvalues λ_n to the mode phase advances σ_ℓ . Alternatively, the correct branch for the mode phase advance σ_ℓ can be selected by numerically integrating Eq. (38) with $\delta\mathbf{P} = 0$ from the pure mode initial conditions in Table I to calculate the orbit $\delta\mathbf{R}_\ell(s)$, and then Fourier transforming $\delta r_x(s)$ or $\delta r_y(s)$ to identify frequency components. A sufficient propagation distance should be taken to allow clear branch identification from discretized transforms.

A specific initial envelope mismatch $\delta\mathbf{R}(s_i)$ can be resolved into normal mode projections according to Eq. (49) by solving for the four (in total) real-valued amplitude A_ℓ and phase $\psi_\ell(s_i)$ parameters needed. Values of $A_\ell \cos \psi_\ell(s_i)$ and $A_\ell \sin \psi_\ell(s_i)$ needed [$\psi_\ell = \pi$ for $\ell = 2, 3$ in case (c) and for all ℓ in case (d)] can be found by matrix inversion of Eq. (49). A pure mode of a given amplitude can be launched by setting one A_ℓ in Eq. (49) to the desired amplitude and setting all other $A_\ell = 0$. The pure mode phase ψ_ℓ can be varied over 2π [except modes that do not have phases: 2 and 3 in case (c) and all in case (d)] to sweep through all possible phase launches. Individual mode launching conditions are not, in general, orthogonal [e.g., $A_1(\mathbf{E}_1e^{i\psi_1} + \mathbf{E}_1^*e^{-i\psi_1}) \cdot A_2(\mathbf{E}_2e^{i\psi_2} + \mathbf{E}_2^*e^{-i\psi_2}) \neq 0$ in case (a)]. However, in the stable case (a) the two modes are almost orthogonal in a sense that $\lim_{s \rightarrow \infty} (1/s) \int_0^s A_1[\mathbf{E}_1e^{i\psi_1} + \mathbf{E}_1^*e^{-i\psi_1}] \cdot A_2[\mathbf{E}_2e^{i\psi_2} + \mathbf{E}_2^*e^{-i\psi_2}] ds = 0$.

For the special cases of continuous and periodic solenoidal focusing channels with a round beam equilibrium ($\varepsilon_x = \varepsilon_y = \varepsilon$ and $r_{xm} = r_{ym} = r_m$), the mode structure is simpler to analyze in terms of the decoupled equations (45) for $\delta r_\pm = (\delta r_x \pm \delta r_y)/2$ rather than the coupled equations (37) for δr_x and δr_y . The transfer matrix \mathbf{M}_e that advances $\delta\mathbf{R} = (\delta r_+, \delta r'_+, \delta r_-, \delta r'_-)$ through one lattice period is of block diagonal form with

$$\mathbf{M}_e(s_i + L_p|s_i) = \begin{bmatrix} \mathbf{M}_+(s_i + L_p|s_i) & 0 \\ 0 & \mathbf{M}_-(s_i + L_p|s_i) \end{bmatrix}, \quad (50)$$

where $\mathbf{M}_\pm(s_i + L_p|s_i)$ are 2×2 symplectic matrices that can be independently analyzed for the stability of $\delta\mathbf{R}_\pm = (\delta r_\pm, \delta r'_\pm)$. The analysis for the normal modes and launching conditions supported by the uncoupled homogeneous equations is analogous to the coupled case above. For each uncoupled equation for δr_\pm we need only analyze a 2×2 eigenvalue equation

$$\mathbf{M}_\pm(s_i + L_p|s_i) \cdot \mathbf{E}_n(s_i) = \lambda_\pm \mathbf{E}_n(s_i). \quad (51)$$

Each of these reduced equations defines a pair of eigenvalues: λ_+ and $1/\lambda_+$ for the δr_+ equation, and λ_- and $1/\lambda_-$ for the δr_- equation. Stable modes with λ_\pm on the unit circle correspond to [13]

$$\frac{1}{2} |\text{Tr } \mathbf{M}_\pm(s_i + L_p|s_i)| < 1. \quad (52)$$

Possible reduced symmetry classes of the eigenvalues are illustrated in Fig. 5[22]. It follows that for a continuous or periodic solenoidal focusing channel with a round beam equilibrium there can only be a single stable mode (phase advance σ_\pm) or two modes: one with pure exponential growth, and one with pure damping (both of the lattice

resonance class with phase advance $\sigma_{\pm} = \pi$). The situation in Fig. 4(b) corresponding to a confluent resonance is excluded when the 4×4 coupled envelope equations reduce to two 2×2 decoupled equations. Initial envelope perturbations in x and y can be projected onto the sum and difference perturbations at axial coordinate $s = s_i$ as

$$\begin{aligned}\delta r_x(s_i) &= \delta r_+(s_i) + \delta r_-(s_i), \\ \delta r'_x(s_i) &= \delta r'_+(s_i) + \delta r'_-(s_i), \\ \delta r_y(s_i) &= \delta r_+(s_i) - \delta r_-(s_i), \\ \delta r'_y(s_i) &= \delta r'_+(s_i) - \delta r'_-(s_i).\end{aligned}\tag{53}$$

For pure mode launches, one takes

$$\begin{aligned}\delta r_-(s_i) = 0 = \delta r'_-(s_i), \quad \delta r_+(s_i) \neq 0 \quad \text{and/or} \quad \delta r'_+(s_i) \neq 0 : & \text{breathing mode,} \\ \delta r_+(s_i) = 0 = \delta r'_+(s_i), \quad \delta r_-(s_i) \neq 0 \quad \text{and/or} \quad \delta r'_-(s_i) \neq 0 : & \text{quadrupole mode.}\end{aligned}\tag{54}$$

This launching condition is schematically plotted in Fig. 6. Note that the pure mode in δr_+ with $\delta r_- = 0$ has in-phase perturbations with $\delta r_x = \delta r_y$ (breathing distortion), whereas a pure mode in δr_- with $\delta r_+ = 0$ has π out of phase perturbations with $\delta r_x = -\delta r_y$ (quadrupole distortion). For this reason, pure decoupled modes in δr_+ and δr_- are called “breathing” and “quadrupole” modes, respectively.

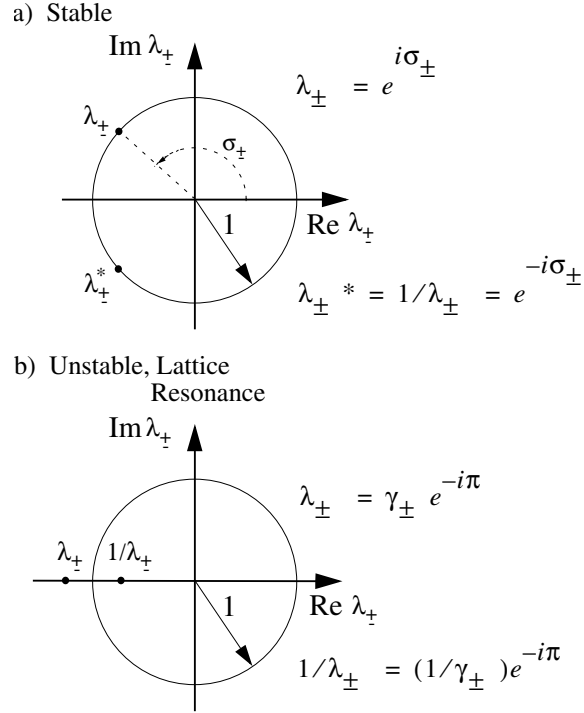


FIG. 5: Two possible classes of eigenvalue symmetries for continuous focusing or periodic solenoidal focusing channels with round beam equilibrium corresponding to stability in (a), and instability in (b).

In the limit of zero space-charge ($Q \rightarrow 0$), the perturbed envelope equations (37) decouple and the envelope modes can be analyzed independently in the x - and y -planes. Therefore, eigenvalue cases for undriven modes reduce to decoupled 2×2 problems in the δr_j and $\delta r'_j$ variables that are directly analogous to the cases discussed above for the δr_{\pm} and $\delta r'_{\pm}$ variables. A phase-amplitude analysis is employed in Appendix D to show that in this zero space-charge limit the phase advance σ_{ej} of oscillations in δr_j over one lattice period is

$$\sigma_{ej} = 2\sigma_{0j}.\tag{55}$$

This limit holds for *any* periodic focusing functions $\kappa_j(s)$. An immediate consequence of Eq. (55) is that all coordinates connected by linear transformation to the δr_j and $\delta r'_j$ coordinates must have oscillations with the same phase advance. Normal mode coordinates $\delta \mathbf{R}_{\ell}$ of an envelope mode are related to the δr_j and $\delta r'_j$ coordinates through linear transformations specified by the eigenvectors as given in Table I. Therefore, the phase advance σ_{ℓ} of any normal

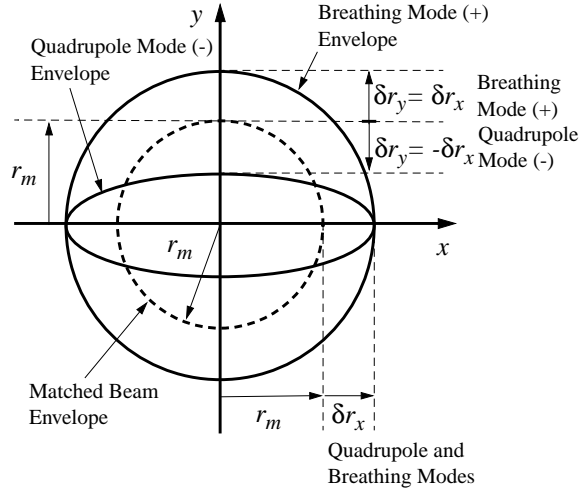


FIG. 6: Round, matched beam envelope with $r_x = r_y = r_m$ in a continuous or solenoidal focusing channel with pure breathing ($\delta r_x = \delta r_y$) and quadrupole ($\delta r_x = -\delta r_y$) mode perturbations superimposed.

envelope mode for any transport channel with $\sigma_{0j} = \sigma_0$ and a symmetric beam with $\varepsilon_x = \varepsilon_y$ must satisfy the zero space-charge limit

$$\lim_{Q \rightarrow 0} \sigma_\ell = 2\sigma_0, \quad (56)$$

regardless of the details of the focusing lattice. This limit provides a consistency check useful in practical calculations. The result can be understood qualitatively as follows. All j -plane particle oscillations in the zero space-charge limit beam have phase advance σ_{0j} . Particles contributing to the perturbed beam edge in phase-space must have contributions from positive and negative coordinates, leading to a envelope locus of particle orbits that oscillates at double the particle oscillation frequency. A consequence of the limit (56) and the decoupling of the x - and y -coordinates for zero space-charge is that envelope instabilities for zero space-charge can *only* occur for $\sigma_0 = \pi/2$ or $\sigma_0 = \pi$. This can be understood as follows. Because the coordinates are decoupled, only lattice resonance instabilities [see Fig. 5(b)] are possible in the x - and y -variables or in any other set of variables connected to these by linear transformations. Therefore, for instability, the eigenvalues must lie on the real axis and $\lim_{Q \rightarrow 0} \sigma_\ell$ must be an integer multiple of π . Equation (56) then establishes a necessary (but not sufficient) condition for instability is that σ_0 be an integer multiple of $\pi/2$, of which only $\pi/2$ and π are relevant to the analysis in this paper because we consider only stable undepressed particle orbits with $\sigma_0 < \pi$.

Another feature of the envelope normal modes is that they evolve with quadratic Courant-Snyder invariants in the normal coordinate phase-space variables of the modes. These invariants are valid regardless of the details of the lattice focusing functions $\kappa_j(s)$ and can be interpreted as phase-space area measures in the normal coordinates of the envelope modes. In Appendix E, a complete derivation of the envelope Courant-Snyder invariants is presented for the case of envelope perturbations in continuous and solenoidal focusing channels with $\kappa_x = \kappa_y \equiv \kappa$ and a symmetric matched beam with $\varepsilon_x = \varepsilon_y$. In this case the normal coordinates of the envelope mode perturbations are the simple sum and difference coordinates $\delta r_\pm = (r_x \pm r_y)/2$ which evolve according to Eq. (45) with zero driving terms. This situation renders the derivation of the invariants directly analogous to standard treatments for decoupled single-particle orbits and shows that

$$\left(\frac{\delta r_\pm}{w_\pm}\right)^2 + (w'_\pm \delta r_\pm - w_\pm \delta r'_\pm)^2 = \text{const}, \quad (57)$$

where the w_\pm are positive mode amplitude functions satisfying

$$\begin{aligned} w''_+ + \kappa w_+ + \frac{2Q}{r_m^2} w_+ + \frac{3\varepsilon^2}{r_m^4} w_+ - \frac{1}{w_+^3} &= 0, \\ w''_- + \kappa w_- + \frac{3\varepsilon^2}{r_m^4} w_- - \frac{1}{w_-^3} &= 0. \end{aligned} \quad (58)$$

For stable envelope oscillations, the amplitudes w_\pm can be interpreted as scaled maximum excursions of pure envelope modes. Analogous Courant-Snyder invariants exist also for the more complicated case of lattices with $\kappa_x \neq \kappa_y$,

where the coupled envelope perturbations δr_j evolve according to Eq. (37) with zero driving terms. In this case, calculation of normal mode coordinates is much more complicated, and is treated in Appendix E by connecting the formulation to a reference where the general coupling problem is analyzed. Although envelope mode Courant-Snyder invariants increase our formal understanding of the mode structure, in practical applications the utility of these invariants is limited because they require calculation of periodic amplitude functions in the lattice that are not, in general, analytically tractable. However, for a given lattice and beam parameters, these amplitude functions can be numerically calculated and the mode invariants can then be employed to improve understanding of mode evolution and launching conditions in an analogous manner to standard treatments of single-particle dynamics.

Finally, the particular solution to Eq. (38) for driving perturbations with $\delta \mathbf{P} \neq 0$ is complicated for periodic focusing lattices. In Sec. III we construct the particular solution for the special case of continuous focusing where it can be carried out directly. This special case may provide a partial guide to the much more complicated situation for periodic focusing lattices which is not addressed in this paper. However, future studies of the particular solution will be aided from the analyses of the homogeneous solutions for periodic solenoidal and quadrupole focusing lattices presented in Secs. IV and V, because such solutions can aid in formulation of Green's function type methods to construct the particular solution.

III. ENVELOPE MODES IN CONTINUOUS FOCUSING CHANNELS

The continuous focusing model described in Sec. IIB is straightforward to analyze and can serve as a good approximation to more realistic periodic focusing lattices when effects do not depend strongly on the periodic nature of the applied focusing forces. In this regard, we find in Secs. IV and V that the continuous focusing model can provide good estimates of normal mode oscillation frequencies in periodic lattices when system parameters are far from bands of parametric instability. Moreover, the continuous focusing model can be solved *exactly* for driven envelope perturbations ($\delta \mathbf{P} \neq 0$), thereby providing new insight into this previously unexplored situation.

A. Matched envelope solution

In a continuous focusing channel, $\kappa_x = \kappa_y = k_{\beta 0}^2 = (\sigma_0/L_p)^2$ [see Eq. (27)]. In this situation, if $\varepsilon_x = \varepsilon_y = \varepsilon$, then the matched beam envelope is round with $r_{xm} = r_{ym} \equiv r_m = \text{const}$, where r_m satisfies the reduced envelope equation of constraint

$$k_{\beta 0}^2 r_m - \frac{Q}{r_m} - \frac{\varepsilon^2}{r_m^3} = 0, \quad (59)$$

or equivalently,

$$\left(\frac{r_m}{L_p}\right)^2 = \frac{Q}{2\sigma_0^2} \left[1 + \sqrt{1 + 4\frac{\sigma_0^2 \varepsilon^2}{Q^2 L_p^2}}\right]. \quad (60)$$

From Eqs. (24) and (60), the depressed phase advance of a particle over an axial distance L_p is given by

$$\sigma = \sqrt{\sigma_0^2 - \frac{Q}{(r_m/L_p)^2}} = \frac{\varepsilon L_p}{r_m^2}. \quad (61)$$

Equations (60) and (61) can be used to relate the space-charge depression σ/σ_0 for the continuous focused beam, which is independent of the specific choice of L_p , to the beam parameters as

$$\frac{k_{\beta 0}^2 \varepsilon^2}{Q^2} = \frac{\sigma_0^2 \varepsilon^2}{Q^2 L_p^2} = \frac{(\sigma/\sigma_0)^2}{[1 - (\sigma/\sigma_0)^2]^2}. \quad (62)$$

B. Envelope modes

Using the equilibrium condition in Eq. (61), the linearized equations (45) describing small amplitude elliptical beam perturbations $\delta r_{\pm} = (\delta r_x \pm \delta r_y)/2$ in the continuous focusing model can be expressed in scaled form as

$$\begin{aligned} L_p^2 \frac{d^2}{ds^2} \left(\frac{\delta r_+}{r_m} \right) + \sigma_+^2 \left(\frac{\delta r_+}{r_m} \right) &= -\frac{\sigma_0^2}{2} \left(\frac{\delta \kappa_x}{k_{\beta 0}^2} + \frac{\delta \kappa_y}{k_{\beta 0}^2} \right) + (\sigma_0^2 - \sigma^2) \frac{\delta Q}{Q} + \sigma^2 \left(\frac{\delta \varepsilon_x}{\varepsilon} + \frac{\delta \varepsilon_y}{\varepsilon} \right), \\ L_p^2 \frac{d^2}{ds^2} \left(\frac{\delta r_-}{r_m} \right) + \sigma_-^2 \left(\frac{\delta r_-}{r_m} \right) &= -\frac{\sigma_0^2}{2} \left(\frac{\delta \kappa_x}{k_{\beta 0}^2} - \frac{\delta \kappa_y}{k_{\beta 0}^2} \right) + \sigma^2 \left(\frac{\delta \varepsilon_x}{\varepsilon} - \frac{\delta \varepsilon_y}{\varepsilon} \right), \end{aligned} \quad (63)$$

where

$$\begin{aligned} \sigma_+ &\equiv \sqrt{2\sigma_0^2 + 2\sigma^2}, \\ \sigma_- &\equiv \sqrt{\sigma_0^2 + 3\sigma^2}. \end{aligned} \quad (64)$$

The homogeneous solutions to Eq. (63) are trivially expressible as

$$\delta r_{\pm}(s) = \delta r_{\pm}(s_i) \cos \left(\sigma_{\pm} \frac{s - s_i}{L_p} \right) + \frac{\delta r'_{\pm}(s_i)}{\sigma_{\pm}/L_p} \sin \left(\sigma_{\pm} \frac{s - s_i}{L_p} \right), \quad (65)$$

where $r_{\pm}(s_i)$ and $r'_{\pm}(s_i)$ denote initial ($s = s_i$) values of the perturbed envelope coordinates. The \pm normal mode solutions to the homogeneous equation correspond to the well-known breathing (+) and quadrupole (−) modes with phase advances σ_+ and σ_- [7]. Projections of the modes onto general initial envelope perturbations in x and y are given by Eq. (53) and the pure mode launching conditions are presented in Sec. II F and are illustrated in Fig. 6. The stability of these undriven oscillations is expected because the applied forces of the continuous focusing lattice cannot change the energy of the oscillations. Variations of the normalized phase advances σ_{\pm}/σ_0 of the breathing and quadrupole modes calculated from Eq. (64) are plotted in Fig. 7 as a function of σ/σ_0 over the full range of space-charge intensity $0 \leq \sigma/\sigma_0 \leq 1$. As expected for finite space-charge intensity with $\sigma/\sigma_0 < 1$, the phase advance of the breathing mode is always greater than the phase advance of the quadrupole mode. Also, consistent with Eq. (56), the zero space-charge limit phase advances satisfy $\lim_{\sigma \rightarrow \sigma_0} \sigma_{\pm} = 2\sigma_0$. The homogeneous solutions for the normal envelope modes given in Eq. (65) is also straightforward to derive using the matrix formulation in Sec. II F. This derivation is carried out in Appendix F [23]. Results presented in Appendix F provide insight on the matrix formulation and may prove useful as a conceptual guide for calculations with periodic lattices where explicit transformations to decoupled variables are not possible.

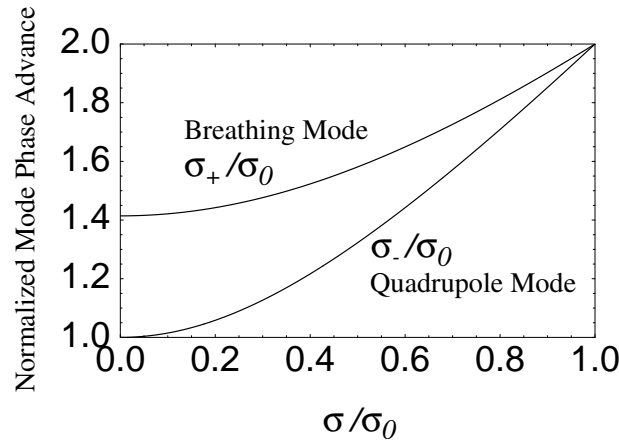


FIG. 7: Normalized phase advances σ_+/σ_0 and σ_-/σ_0 of the breathing and quadrupole modes plotted versus σ/σ_0 for a continuous focusing channel.

A Green's Function method [13] based on the the homogeneous solutions (65) can be employed to calculate particular

solutions of Eq. (63) in terms of an integral as

$$\begin{aligned}\frac{\delta r_{\pm}(s)}{r_m} &= \frac{1}{L_p^2} \int_{s_i}^s d\tilde{s} G_{\pm}(s, \tilde{s}) \delta p_{\pm}(\tilde{s}), \\ \delta p_+(s) &= -\frac{\sigma_0^2}{2} \left[\frac{\delta \kappa_x(s)}{k_{\beta 0}^2} + \frac{\delta \kappa_y(s)}{k_{\beta 0}^2} \right] + (\sigma_0^2 - \sigma^2) \frac{\delta Q(s)}{Q} + \sigma^2 \left[\frac{\delta \varepsilon_x(s)}{\varepsilon} + \frac{\delta \varepsilon_y(s)}{\varepsilon} \right], \\ \delta p_-(s) &= -\frac{\sigma_0^2}{2} \left[\frac{\delta \kappa_x(s)}{k_{\beta 0}^2} - \frac{\delta \kappa_y(s)}{k_{\beta 0}^2} \right] + \sigma^2 \left[\frac{\delta \varepsilon_x(s)}{\varepsilon} - \frac{\delta \varepsilon_y(s)}{\varepsilon} \right],\end{aligned}\tag{66}$$

where

$$G_{\pm}(s, \tilde{s}) = \frac{1}{\sigma_{\pm}/L_p} \sin \left(\sigma_{\pm} \frac{s - \tilde{s}}{L_p} \right)\tag{67}$$

are Green's functions for the breathing (+) and quadrupole (−) terms. The particular solutions in Eq. (66) satisfies the initial conditions $\delta r_{\pm}(s = s_i) = 0$ and $\delta r'_{\pm}(s = s_i) = 0$, and the solution can be readily interpreted as a scaled convolution of the driving perturbations onto the natural harmonic response of the normal modes. This is expected because continuous focusing is spatially homogeneous.

Given specific initial mismatches (i.e., δr_j and $\delta r'_j$ at $s = s_i$ for $j = x, y$) and driving terms (i.e., $\delta \kappa_j$, δQ , and $\delta \varepsilon_j$), Eqs. (65) and (66) for the homogeneous (denoted $|_h$ here) and particular (denoted $|_p$ here) solution components can be applied to calculate the general evolution of the envelope perturbations $\delta r_x = \delta r_x|_h + \delta r_x|_p = (r_+ + r_-)|_h + (r_+ + r_-)|_p$ and $\delta r_y = \delta r_y|_h + \delta r_y|_p = (r_+ - r_-)|_h + (r_+ - r_-)|_p$. To better understand the range of possible envelope evolutions the driving terms induce, it is instructive to calculate the response to specific classes of driving perturbations that are adiabatic, sudden, ramped, and harmonic.

First, in the adiabatic limit, variations of the driving terms $\delta p_{\pm}(s)$ are taken to be slow on the scale of the quadrupole mode wavelength $2\pi L_p/\sigma_-$, which is longer than the breathing mode wavelength $2\pi L_p/\sigma_+$ for $\sigma/\sigma_0 < 1$. In this situation, Eqs. (63) and (64) can be employed to express the particular solutions as

$$\begin{aligned}\frac{\delta r_+}{r_m} &= \frac{\delta p_+}{\sigma_+^2} \\ &= -\left[\frac{1}{2} \frac{1}{1 + (\sigma/\sigma_0)^2} \right] \frac{1}{2} \left(\frac{\delta \kappa_x}{k_{\beta 0}^2} + \frac{\delta \kappa_y}{k_{\beta 0}^2} \right) + \left[\frac{1}{2} \frac{1 - (\sigma/\sigma_0)^2}{1 + (\sigma/\sigma_0)^2} \right] \frac{\delta Q}{Q} + \left[\frac{(\sigma/\sigma_0)^2}{1 + (\sigma/\sigma_0)^2} \right] \frac{1}{2} \left(\frac{\delta \varepsilon_x}{\varepsilon} + \frac{\delta \varepsilon_y}{\varepsilon} \right), \\ \frac{\delta r_-}{r_m} &= \frac{\delta p_-}{\sigma_-^2} \\ &= -\left[\frac{1}{1 + 3(\sigma/\sigma_0)^2} \right] \frac{1}{2} \left(\frac{\delta \kappa_x}{k_{\beta 0}^2} - \frac{\delta \kappa_y}{k_{\beta 0}^2} \right) + \left[\frac{2(\sigma/\sigma_0)^2}{1 + 3(\sigma/\sigma_0)^2} \right] \frac{1}{2} \left(\frac{\delta \varepsilon_x}{\varepsilon} - \frac{\delta \varepsilon_y}{\varepsilon} \right).\end{aligned}\tag{68}$$

The particular solutions (68) can also be derived by partial integration of Eq. (66) and neglecting the terms containing $\delta p'_{\pm}$. Coefficients of the driving terms $(\delta \kappa_x/k_{\beta 0}^2 \pm \delta \kappa_y/k_{\beta 0}^2)/2$, $\delta Q/Q$, and $(\delta \varepsilon_x/\varepsilon \pm \delta \varepsilon_y/\varepsilon)/2$ in the adiabatic solution (68) (i.e., the terms in the square brackets) are plotted as a function of space-charge depression σ/σ_0 in Fig. 8. These curves describe the relative strength of the response in δr_{\pm} to different classes of adiabatic driving perturbations as a function of space-charge intensity.

Next, to analyze the opposite limit of driven perturbations $\delta p_{\pm}(s)$ with sudden changes, we take

$$\delta p_{\pm}(s) = \widehat{\delta p_{\pm}} \Theta(s - s_p).\tag{69}$$

Here, $\Theta(x)$ is the Heaviside step function defined by $\Theta(x) = 0$ for $x < 0$ and $\Theta(x) = 1$ for $x > 0$, $s = s_p$ is the axial coordinate where the perturbations jump, and

$$\begin{aligned}\widehat{\delta p_+} &= -\frac{\sigma_0^2}{2} \left[\frac{\widehat{\delta \kappa_x}}{k_{\beta 0}^2} + \frac{\widehat{\delta \kappa_y}}{k_{\beta 0}^2} \right] + (\sigma_0^2 - \sigma^2) \frac{\widehat{\delta Q}}{Q} + \sigma^2 \left[\frac{\widehat{\delta \varepsilon_x}}{\varepsilon} + \frac{\widehat{\delta \varepsilon_y}}{\varepsilon} \right], \\ \widehat{\delta p_-} &= -\frac{\sigma_0^2}{2} \left[\frac{\widehat{\delta \kappa_x}}{k_{\beta 0}^2} - \frac{\widehat{\delta \kappa_y}}{k_{\beta 0}^2} \right] + \sigma^2 \left[\frac{\widehat{\delta \varepsilon_x}}{\varepsilon} - \frac{\widehat{\delta \varepsilon_y}}{\varepsilon} \right]\end{aligned}\tag{70}$$

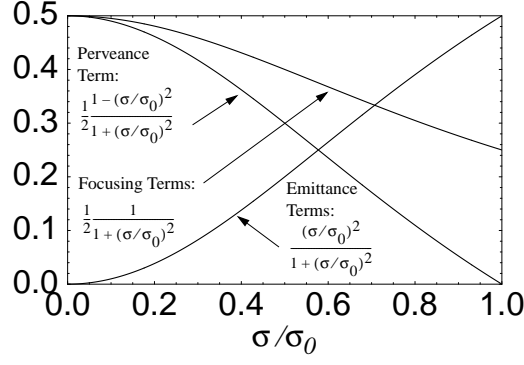
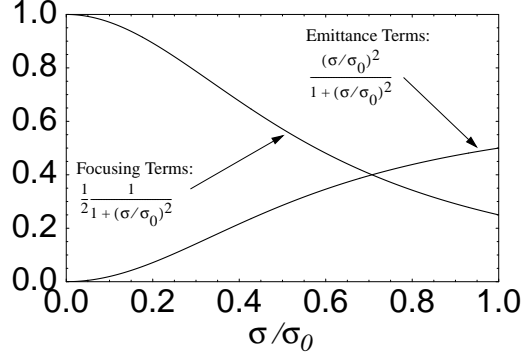
a) Adiabatic Solution Coefficients for $\delta r_+ = (\delta r_x + \delta r_y)/2$ b) Adiabatic Solution Coefficients for $\delta r_- = (\delta r_x - \delta r_y)/2$ 

FIG. 8: Coefficients in Eq. (68) describing the strength of adiabatic limit envelope response terms to classes of driving perturbations are plotted as a function of σ/σ_0 . Coefficients occurring in the sum (r_+) and difference (r_-) particular solutions are plotted separately in (a) and (b).

are constant amplitudes of the sudden, step-perturbations defined according to Eq. (66) with $\delta Q \rightarrow \widehat{\delta Q} = \text{const}$ for the perveance perturbation, etc. For these step-function perturbations, Eq. (66) can be integrated, and the response in the particular solutions for δr_{\pm} can be expressed in the same form as the adiabatic solutions with the following substitutions in Eq. (68):

$$\delta p_{\pm} \rightarrow \widehat{\delta p}_{\pm} \left[1 - \cos \left(\sigma_{\pm} \frac{s - s_p}{L_p} \right) \right] \Theta(s - s_p). \quad (71)$$

The response to other sudden perturbations $\delta p_{\pm}(s)$ can be calculated by superimposing perturbations of the form in Eqs. (69) and (70).

Comparing the adiabatic solutions in Eq. (68) with the sudden solutions given by Eqs. (68) and (71), note that the sudden response is oscillatory with periods $2\pi L_p/\sigma_{\pm}$ in the solutions for δr_{\pm} rather than steady as in the adiabatic case. For the same driving perturbation amplitude [e.g., $\delta Q(s) = \widehat{\delta Q}$ for $s \gtrsim s_p$ for the adiabatic perturbation], the excursions of the envelope oscillations for sudden perturbations oscillate between zero and *twice* the adiabatic excursion. This characteristic response to a step-function perturbation is illustrated in Fig. 9 for the evolution of $\delta r_+/r_m$ resulting from a pure emittance perturbation with $(\widehat{\delta \varepsilon_x}/\varepsilon + \widehat{\delta \varepsilon_y}/\varepsilon)/2 > 0$. The dashed line shows the adiabatic response for a slowly varied perturbation that achieves the same emittance change as the sudden perturbation applied at $s = s_p$ {i.e., an adiabatic perturbation with $[\delta \varepsilon_x(s)/\varepsilon + \delta \varepsilon_y(s)/\varepsilon]/2 = (\widehat{\delta \varepsilon_x}/\varepsilon + \widehat{\delta \varepsilon_y}/\varepsilon)/2$ for $s \gtrsim s_p$ }.

Another instructive example is the envelope response to linear ramp driving perturbations. In this case we take

$$\delta p_{\pm}(s) = \widehat{\delta p}'_{\pm}(s - s_p)\Theta(s - s_p). \quad (72)$$

Here, $\widehat{\delta p}'_{\pm}$ is a constant that describes the ramp perturbations applied at axial coordinate $s = s_p$ and is defined by replacing $\widehat{\delta Q} \rightarrow \widehat{\delta Q}'$ with $\widehat{\delta Q}' = \text{const}$ in Eq. (70) for the perveance perturbation, etc. For these ramp perturbations, the particular solutions given by Eq. (66) can be expressed in the same form as the adiabatic solutions with the

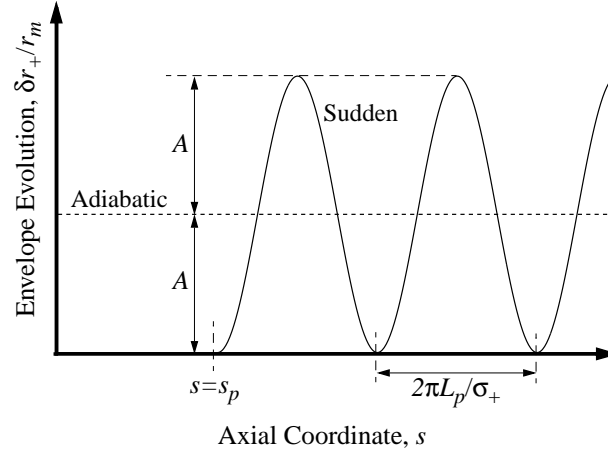


FIG. 9: Contrast of the envelope response $\delta r_+(s)$ to sudden and adiabatic driving emittance perturbations with $(\widehat{\delta\varepsilon'_x}/\varepsilon + \widehat{\delta\varepsilon'_y}/\varepsilon)/2 > 0$ that achieve the same value of emittance change.

following substitutions in Eq. (68):

$$\delta p_{\pm} \rightarrow \frac{L_p}{\sigma_{\pm}} \widehat{\delta p'_{\pm}} \left[\sigma_{\pm} \frac{s - s_p}{L_p} + \sin \left(\sigma_{\pm} \frac{s - s_p}{L_p} \right) \right] \Theta(s - s_p). \quad (73)$$

Comparing the solutions for adiabatic, sudden, and linear ramped driving perturbations given by Eqs. (68)–(73), the response to the ramped perturbations can be interpreted as having both adiabatic and “sudden” oscillatory components given by the first and second terms in Eq. (73), respectively. The particular solution for the ramped perturbation is illustrated schematically in Fig. 10 for the evolution of $\delta r_+/r_m$ in response to a pure emittance perturbation with $(\widehat{\delta\varepsilon'_x}/\varepsilon + \widehat{\delta\varepsilon'_y}/\varepsilon)/2 > 0$. For $s \gg s_p$, the response is dominated by the adiabatic component, whereas for $s \gtrsim s_p$, the sudden oscillatory component with period $2\pi L_p/\sigma_+$ can be significant.

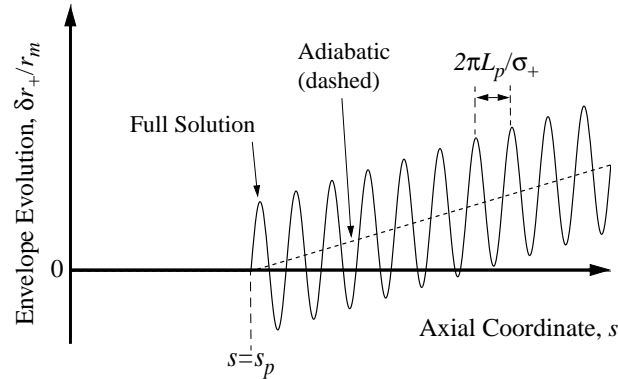


FIG. 10: Envelope response $\delta r_+(s)$ for a linear ramp driving emittance perturbation with $(\widehat{\delta\varepsilon'_x}/\varepsilon + \widehat{\delta\varepsilon'_y}/\varepsilon)/2 > 0$.

Finally, we analyze harmonic driving perturbations in $\delta p_{\pm}(s)$ by taking

$$\delta p_{\pm}(s) = \widehat{\delta p_{\pm}} \exp(iks). \quad (74)$$

Here, $\widehat{\delta p_{\pm}}$ are complex constants defined from $\delta p_{\pm}(s)$ that are of the same form as given in Eq. (70) and represent the amplitude of the harmonic perturbations, and $k = \text{const}$ is the complex wavenumber of the perturbations. The physical perturbations are represented by the real part of the expressions in Eq. (74). Driving perturbations with pure harmonic oscillations can be modeled by taking k real, pure exponential growing or damping by taking k imaginary, and damped or growing oscillations by taking k complex. Superpositions of harmonic perturbations of the form in Eq. (74) can be employed to recover previous examples analyzed. For these harmonic perturbations, the particular solutions (66) can be expressed in the same form as the adiabatic solution by taking the real part of the following

substitutions in (68):

$$\delta p_{\pm} \rightarrow \widehat{\delta p_{\pm}} \left[\frac{\cos(\sigma_{\pm}s/L_p) + i(kL_p/\sigma_{\pm}) \sin(\sigma_{\pm}s/L_p) - \exp(iks)}{(kL_p/\sigma_{\pm})^2 - 1} \right]. \quad (75)$$

For k pure imaginary the particular solutions given by Eqs. (68) and (75) lead to oscillatory solutions with damping ($\text{Im } k > 0$) or growth terms ($\text{Im } k < 0$). For $|\text{Re } k|$ sufficiently removed from σ_{\pm}/L_p , the response is pure oscillatory ($\text{Im } k = 0$), or oscillatory with growth or damping terms ($\text{Im } k \neq 0$). When $|\text{Re } k| \simeq \sigma_{\pm}/L_p$, the response has classic linear resonance growth with

$$\lim_{k \rightarrow \sigma_{\pm}/L_p} \frac{\cos(\sigma_{\pm}s/L_p) + i(kL_p/\sigma_{\pm}) \sin(\sigma_{\pm}s/L_p) - \exp(iks)}{(kL_p/\sigma_{\pm})^2 - 1} = \frac{i}{2} [\sin(\sigma_{\pm}s/L_p) - (\sigma_{\pm}s/L_p) \exp(\sigma_{\pm}s/L_p)]. \quad (76)$$

Linear superposition of the specific examples above provides insight into the range of envelope responses to small-amplitude driving perturbations formally given by Eq. (66). Several conclusions can be drawn from these results. First, driving perturbations that are fast on the scale of the breathing and quadrupole envelope mode phase advances σ_{\pm} are more dangerous than slow changes because they can result in twice the beam envelope excursion for equal amplitude changes in the driving terms. Second, oscillatory driving perturbations of small amplitude are not problematic unless the driving terms have frequency components with phase advances close to the breathing or quadrupole mode phase advances σ_{\pm} . This simple continuous focusing analysis of driven perturbations should help guide the more complicated situation in periodic focusing lattices. However, caution must be employed in application of these results, particularly when making higher-order extrapolations. For example, if a periodic focusing perturbation with $\delta\kappa_x = -\delta\kappa_y$ is taken, one might expect to recover net focusing because this perturbation corresponds to a superimposed alternating gradient quadrupole lattice. However, from Eq. (66), such a choice has no projection on the breathing mode to linear order. A recent analytical study of matched beam envelopes in periodic quadrupole focusing channels suggest how such higher-order effects might be more accurately modeled but are beyond the scope of the present analysis[18].

IV. ENVELOPE MODES IN SOLENOIDAL FOCUSING CHANNELS

A beam with an elliptical cross-section envelope and zero total canonical angular momentum {i.e., $P_{\theta} = \langle xy' - yx' \rangle_{\perp} + [qB_z/(2m\gamma_b\beta_b c)]\langle x^2 + y^2 \rangle_{\perp} = 0$ } that is focused in a solenoidal transport channel by a periodic solenoidal magnetic field $\mathbf{B}(s) = -[B'_z(s)/2](x\hat{\mathbf{x}} + y\hat{\mathbf{y}}) + B_z(s)\hat{\mathbf{z}}$ can be analyzed with the envelope equations (4), provided that we take the focusing strength to be $\kappa_x = \kappa_y \equiv \kappa = [qB_z/(2m\gamma_b\beta_b c)]^2$ and interpret the analysis as applying in a local (s -varying) rotating Larmor frame. This correspondence is developed in Appendix B by deriving a self-consistent KV distribution describing elliptical beams with $P_{\theta} = 0$ in a solenoidal focusing channel. The derivation identifies correspondences needed to apply Eq. (4) to this situation including replacements for the laboratory-frame rms emittances ε_x and ε_y in terms of Larmor-frame invariant emittance measures. In the context of interpreting the envelope equations (4) with appropriate Larmor-frame replacements, the formalism in Sec. IIF can be applied to analyze elliptical perturbations in the beam envelope for solenoidal transport channels. For simplicity of presentation, we carry out analysis in this section without making explicit reference to the Larmor frame. However, the Larmor frame transformations presented in Appendix B must be applied to project nonaxisymmetric normal modes ($\delta r_x \neq \delta r_y$) into the stationary laboratory frame to view the evolution there — a distinction not made in previous work on envelope modes in solenoidal transport channels[2, 7].

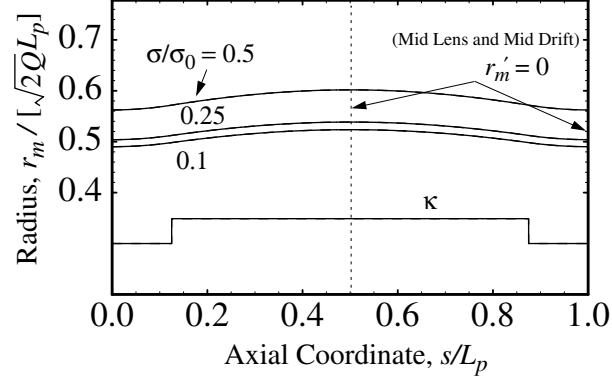
In this section we explore normal mode envelope perturbations ($\delta\mathbf{P} = 0$) in a periodic solenoidal transport channel with piecewise constant $\kappa(s)$. Physical solenoidal focusing lattices with fringe fields associated with continuously varying $\kappa(s)$ can be approximated by the model with piecewise constant $\kappa(s)$ using the equivalency procedures developed in Appendix A. Mode structures and launching conditions are classified and instabilities are parametrically mapped using the decoupled mode formulation in Sec. IIF. In addition to elliptical beam perturbations with zero beam canonical angular momentum ($P_{\theta} = 0$), results for axisymmetric perturbations ($\delta r_x = \delta r_y$) can also be applied to beams with nonzero canonical angular momentum using the correspondences derived in Appendix B. Results in this section can also be applied without transformation to idealized beam models where a stationary, partially neutralizing charge distribution produces the specified focusing function $\kappa(s)$. Driving perturbations with $\delta\mathbf{P} \neq 0$ are not analyzed.

A. Matched envelope solution

We consider the case of a periodic, matched solution ($r_x = r_{xm}$ and $r_y = r_{ym}$) to the the envelope equations (4) with equal emittances $\varepsilon = \varepsilon_x = \varepsilon_y$ and a round beam envelope $r_{xm} = r_{ym} = r_m$. A hard-edge focusing lattice

is taken with $\kappa_x(s) = \kappa_y(s) \equiv \kappa(s)$ piecewise constant as illustrated in Fig. 2(b) with lattice period L_p , solenoid strength $\hat{\kappa} = \text{const}$, and occupancy η . The matched envelope solutions are parameterized by L_p , σ_0 , σ/σ_0 , and η . Numerical solutions are plotted for one lattice period in Fig. 11 in terms of the scaled envelope radius $[r_m/(\sqrt{2Q}L_p)]$ versus normalized axial coordinate (s/L_p) for fixed undepressed single-particle phase advance σ_0 , and values of σ/σ_0 . Solutions for large and small occupancies are contrasted in (a) and (b) and symmetry points are indicated on the plot. Comparing (a) and (b), observe that the radial extent of the periodic flutter of the beam envelope varies strongly with the solenoid occupancy η . This strong flutter variation is expected because the limit $\eta \rightarrow 1$ corresponds to continuous focusing in the Larmor frame with $r_m = \text{const}$, whereas the limit $\eta \rightarrow 0$ corresponds to focusing with thin-lens kicks (see Appendix G) and maximal flutter motion. The single-particle phase advances σ_0 and σ are interpreted in the Larmor frame.

a) Matched Envelope for $\sigma_0 = 80^\circ$ and $\eta = 0.75$



b) Matched Envelope for $\sigma_0 = 80^\circ$ and $\eta = 0.25$

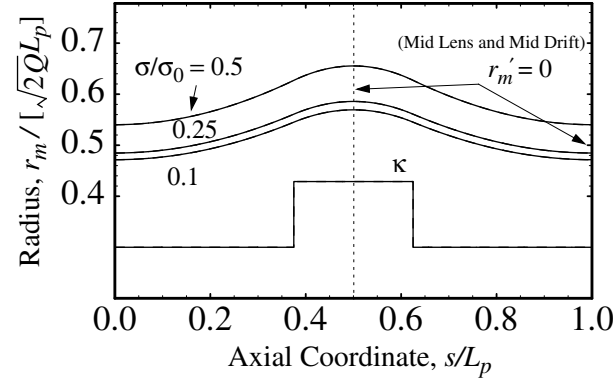


FIG. 11: Scaled matched beam envelope $r_m/(\sqrt{2Q}L_p)$ versus normalized axial coordinate s/L_p for one period of a hard-edge solenoidal focusing channel in Fig. 2(b). Solutions are shown for $\sigma_0 = 80^\circ$ and values of σ/σ_0 indicated for occupancies $\eta = 0.75$ and $\eta = 0.25$ in (a) and (b), respectively.

The analysis in Appendix B shows that the matched, round beam envelope with $r_{xm} = r_{ym} = r_m$ described above can be applied to model beams with finite canonical angular momentum $P_\theta = \langle xy' - yx' \rangle_\perp + [qB_z/(2m\gamma_b\beta_b c)]\langle x^2 + y^2 \rangle_\perp$ in the range $-1 < 2P_\theta/\varepsilon < 1$ if the emittance ε is replaced by the Larmor invariant emittance according to $\varepsilon^2 \rightarrow \varepsilon_x^2 - 4\langle r^2\theta' \rangle_\perp + 4P_\theta^2 = \text{const}$ to include the defocusing effect of $P_\theta \neq 0$. The matched beam parameterization employed with L_p , σ_0 , σ/σ_0 , and η is convenient to understand envelope stability properties in solenoidal focusing and place results in a form directly comparable to those obtained for quadrupole focusing (see Sec. V). However, in calculating perveance (or current) limits, the periodicity of the lattice plays a less direct role for solenoidal focusing than for quadrupole focusing[17, 18]. For a quadrupole lattice alternating focusing and defocusing optics in the period provide net focusing that cannot exist without the regular interchange of focusing and defocusing within the period, whereas in solenoid lattices all optics are focusing and net focusing exists even in the limit of full occupancy ($\eta = 1$) where there is no lattice period.

B. Normal modes

Normal mode solutions for elliptical perturbations ($\delta r_x \neq \delta r_y$) about the round, matched envelope solutions described in Sec. IV A are numerically analyzed using the formulation in Sec. II F. For the special case considered of an axisymmetric matched envelope the reduced eigenvalue formulation with decoupled perturbed envelopes $\delta r_{\pm} = (\delta r_x \pm \delta r_y)/2$ is employed to resolve the perturbations into breathing (+) and quadrupole (−) modes. This reduced problem is equivalent to numerically calculating eigenvalues λ_n of the coupled 4-dimensional matrix equation (47) to characterize the stability properties of the homogeneous equation (38) with $\kappa_x = \kappa_y = \kappa$, $\varepsilon_x = \varepsilon_y = \varepsilon$, and zero driving perturbations ($\delta \mathbf{P} = 0$). Eigenvalues are calculated for specified values of η and ranges of σ_0 and σ/σ_0 to map out mode properties including mode phase advances σ_{\pm} and growth factors γ_{\pm} associated with broad bands of parametric instability. Results we obtained are displayed in Figs. 12–14.

We find that bands of parametric instability with $\gamma_+ > 1$ and $\gamma_- > 1$ for the breathing and quadrupole modes do not overlap. Therefore, in terms of the symmetry classes presented in Fig. 4, eigenvalues can only fall into class (a) [stability] or (c) [lattice resonance instability], and class (d) [double lattice resonance instability] does not occur. As shown in Sec. II F, eigenvalues falling into class (b) [confluent resonance instability] are not possible because the breathing and quadrupole modes are decoupled for solenoidal focusing. Breathing and quadrupole mode phase advances σ_{\pm} and growth factors γ_{\pm} are contoured in Fig. 12 as a function of σ_0 and σ/σ_0 for $\sigma_0 \in (0, 180^\circ)$ and the full range of space-charge depression $\sigma/\sigma_0 \in (0, 1]$. Results are contrasted for occupancies $\eta = 0.75$ and $\eta = 0.25$ in columns (a) and (b). Growth factors of both the breathing ($\gamma_+ > 1$) and quadrupole ($\gamma_- > 1$) modes are superimposed on the same plots because the bands do not overlap, and growth factors of the corresponding damped modes are not plotted because damping factors are given by $1/\gamma_{\pm}$ of the growing mode [see Fig. 4(c) and Table I]. The growth factor contours are restricted to $\sigma_0 \in (90^\circ, 180^\circ)$ because no instability is found for $\sigma_0 < 90^\circ$. These plots help clarify regions of parametric envelope instability observed in previous studies[4, 7, 20]. In the present study, modes are unambiguously identified over the practical range of machine parameters and previous errors in branch calculation are corrected.

To better illustrate the mode structures presented in Figs. 12, in Fig. 13 we plot the mode phase advances and growth factors for fixed σ_0 and η as a function of σ/σ_0 . Curves shown correspond to the vertical dashed lines on the contour plots in Fig. 12. Complex plots of the eigenvalues λ_{\pm} relative to the unit circle are superimposed at several locations to further illustrate the eigenvalue structure of the modes and the symmetry class of the instability bands. Individual mode branches for the breathing and quadrupole modes are identified outside of regions of instability using the formulation described in Sec. II F and branches are continuously connected across bands of parametric instability. As expected for finite space-charge ($\sigma/\sigma_0 < 1$), the in-phase oscillations of the breathing mode with $\delta r_x = \delta r_y$ have higher phase advance σ_+ than the phase advance σ_- of the out-of-phase oscillations of the quadrupole mode with $\delta r_x = -\delta r_y$. Continuous model results superimposed are calculated from Eq. (64) using the single-particle phase advances σ_0 and σ derived from the periodically focused, matched beam. Far from instability bands, the continuous formulas provide accurate estimates of the mode phase advances[7]. Curves for the continuous and periodic focused calculations of σ_{\pm} almost overlay for $\sigma_0 = 80^\circ$ and agreement further improves for lower values of σ_0 . Analysis in Sec. II F [see Eq. (56)] shows that the zero space-charge limit $Q \rightarrow 0$ corresponds to stable breathing and quadrupole mode oscillations with

$$\begin{aligned} \lim_{\sigma \rightarrow \sigma_0} \sigma_{\pm} &= 2\sigma_0, \\ \lim_{\sigma \rightarrow \sigma_0} \gamma_{\pm} &= 1. \end{aligned} \tag{77}$$

These limiting values are indicated on the figure to provide a partial check of results. For another check of results, mode eigenvalues are analytically calculated in Appendix G in the thin-lens limit ($\eta \rightarrow 0$ at fixed σ_0) for a beam with full space-charge depression ($\sigma = 0$). Phase advances and growth rates calculated from this analysis are indicated in Fig. 13(b). The small discrepancies evident are traceable to sensitivities of results on the solenoid occupancy η .

To better understand sensitivities on the solenoid occupancy, variations of the breathing and quadrupole mode phase advances and growth factors with η are illustrated in Fig. 14. From this plot and Fig. 12, note that instability bands get wider and mode growth rates stronger with decreasing η . Limit points indicated on the plots come from analytical calculations of the band structure in the thin-lens limit ($\eta \rightarrow 0$) at full space-charge depression presented in Appendix G and Eq. (77).

The lattice resonance instability bands have been identified as a half-integer parametric resonance between the envelope mode oscillation frequencies and the lattice[7]. This suggests that the location of the envelope bands can be crudely estimated using resonance conditions based on the breathing and quadrupole mode frequencies σ_{\pm} derived from the continuous model with $\sigma_+ = \sqrt{2\sigma_0^2 + 2\sigma^2}$ and $\sigma_- = \sqrt{\sigma_0^2 + 3\sigma^2}$ [see Eq. (64)] as $\sigma_{\pm} = \pi$, or equivalently

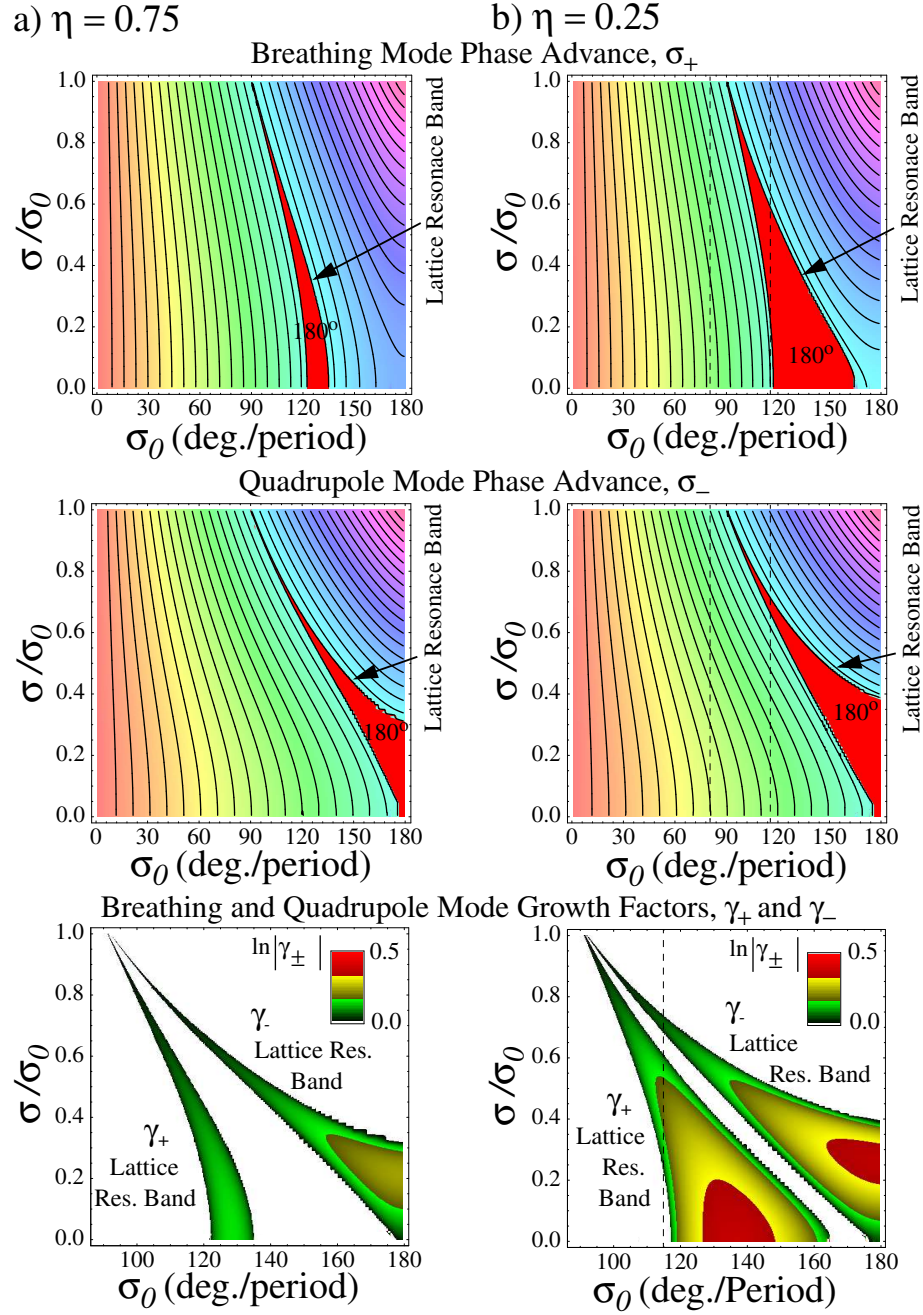


FIG. 12: Contours of (upper row) breathing and (middle row) quadrupole mode phase advances (σ_{\pm}) and (bottom row) growth factors (γ_{\pm}) as a function of σ_0 and σ/σ_0 for a solenoidal focusing channel. Results are shown for occupancies $\eta = 0.75$ and $\eta = 0.25$ in columns (a) and (b). In the upper and middle rows, black contour lines correspond to $\sigma_{\pm} = 10^\circ, 20^\circ, 30^\circ, \dots$ and colors vary continuously with changes in σ_{\pm} (bands of instability with $\sigma_{\pm} = 180^\circ$ are marked in solid red for emphasis). In the lower row, values of $\ln(\gamma_{\pm})$ with $\gamma_{\pm} > 1$ are labeled with continuously varying colors as indicated in the key. Identical color schemes are used in columns (a) and (b) to measure mode phase advances and growth factors. Vertical dashed lines in the plots for $\eta = 0.25$ correspond to the cross-section plots in Fig. 13.

with σ_0 and σ measured in degrees,

$$\sqrt{2\sigma_0^2 + 2\sigma^2} = 180^\circ \quad (78)$$

for the breathing mode, and

$$\sqrt{\sigma_0^2 + 3\sigma^2} = 180^\circ \quad (79)$$

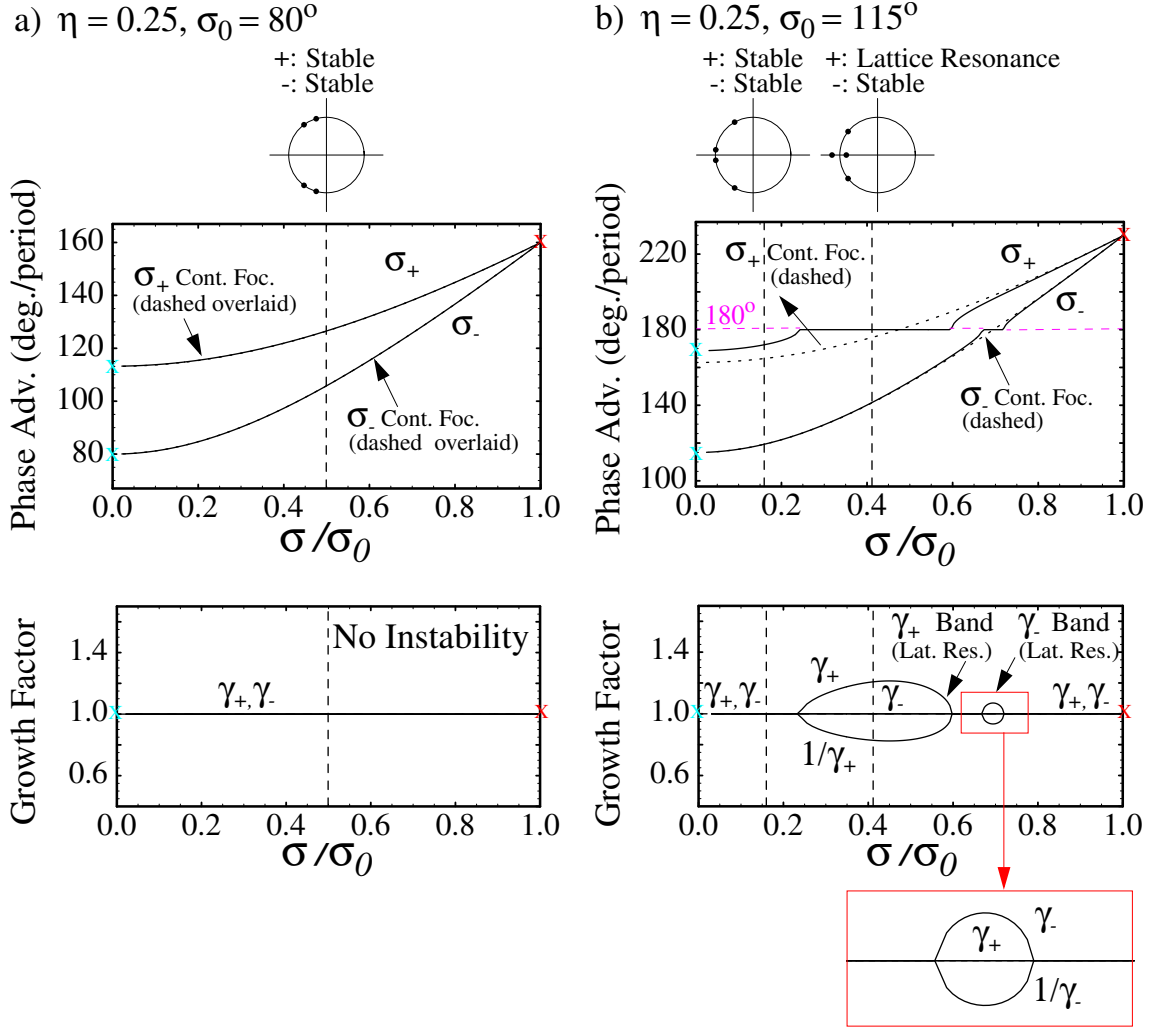


FIG. 13: Phase advance (σ_{\pm}) and growth factors (γ_{\pm}) of the breathing and quadrupole envelope modes versus σ/σ_0 for a solenoidal focusing channel with occupancy $\eta = 0.25$ for $\sigma_0 = 80^\circ$ and $\sigma_0 = 115^\circ$ in columns (a) and (b). Continuous focusing model predictions for σ_{\pm} are superimposed (dashed curves). Red **X**s mark analytical results in the zero space-charge limit and cyan **X**s mark thin-lens limit ($\eta \rightarrow 0$) analytical results with $\sigma/\sigma_0 = 0$. Vertical dashed lines correspond to locations of plots of complex eigenvalues λ_{\pm} placed above. Red boxes denote expanded views.

for the quadrupole mode. Comparing to Fig. 12, these resonance formulas roughly predict band locations, but correspond more closely to the lower thresholds in σ_0 than the maximum growth factor locations as might be anticipated. Moreover, the formulas cannot capture the broad parametric nature of the instability or changes in band structure with solenoid occupancy η . In order to provide better guidance for the band locations in practical applications, parametric data was employed to calculate curve fits for the instability thresholds. We find that instability threshold data can be roughly fit by curves in σ_0 and σ corresponding to: centered elliptical curves with

$$\sigma^2 + f\sigma_0^2 = (90^\circ)^2(1 + f) \quad (80)$$

for the left- and right-boundary curves of the breathing mode band, a curve with form

$$\sigma/\sigma_0 + g\frac{\sigma_0}{90^\circ} = 1 + g \quad (81)$$

for the left-boundary of the quadrupole mode band, and a line with

$$\sigma + g\sigma_0 = 90^\circ(1 + g) \quad (82)$$

for the right-boundary of the quadrupole mode band. In Eqs. (80)–(82), σ_0 and σ are measured in degrees, f and g are undetermined functions of η . Based on the analysis in Sec. IIF, the boundary curves in Eqs. (80)–(82) are

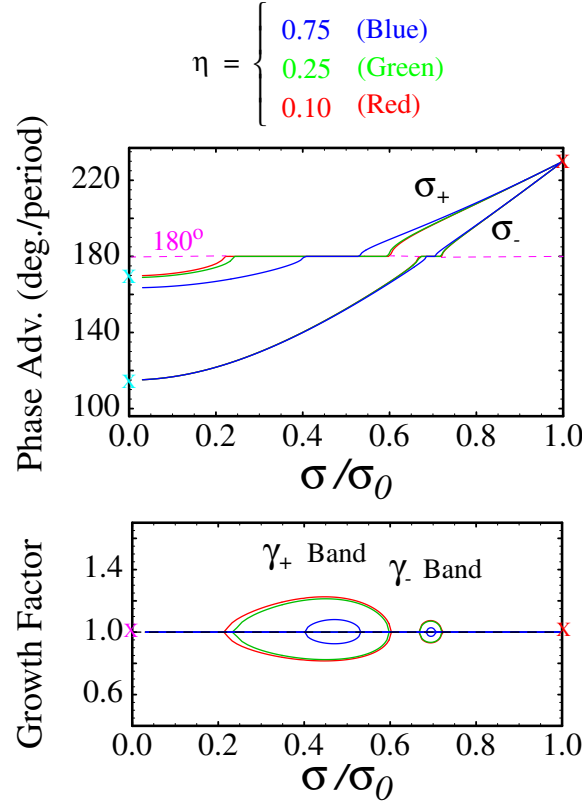


FIG. 14: Variation of mode structure with solenoid occupancy η . Phase advance (σ_{\pm}) and growth factors (γ_{\pm}) of the breathing and quadrupole modes are plotted versus σ/σ_0 for $\sigma_0 = 115^\circ$ and the indicated values of η . Red **X**s mark analytical results in the zero space-charge limit and cyan **X**s mark thin-lens limit ($\eta \rightarrow 0$) analytical results with $\sigma/\sigma_0 = 0$.

constrained to contain the limit point $\sigma = \sigma_0 = 90^\circ$. Consistent with containing this point, Eq. (81) corresponds to the most general centered ellipse in σ_0 and σ , and Eqs. (81) and (82) are the most general lines in σ_0 and σ/σ_0 , and σ_0 and σ , respectively. To account for weak variations from these forms in σ_0 and σ while containing the point $\sigma = \sigma_0 = 90^\circ$, we also take f and g to vary linearly with σ_0 in addition to having dependence on η . Using threshold data with $\sigma_0 \in [96^\circ, 174^\circ]$ and $\eta \in [0.1, 0.7]$, we find that the breathing band threshold are fit by the elliptic formula in Eq. (80) with

$$f(\eta, \sigma_0) = \begin{cases} 1.113 - 0.413\eta + 0.00348\sigma_0, & \text{left-edge,} \\ 1.046 + 0.318\eta + 0.00410\sigma_0, & \text{right-edge,} \end{cases} \quad (83)$$

where average and maximum deviations between the threshold data and the fit formula are $\sim 3^\circ$ and $\sim 6^\circ$ for the left-edge and $\sim 4^\circ$ and $\sim 6^\circ$ for the right-edge. Similarly, using the threshold data over the same range for the quadrupole band with the formulas in Eqs. (81) and (82), we obtain the fits

$$g(\eta) = \begin{cases} 1, & \text{left-edge,} \\ 0.227 + 0.173\eta, & \text{right-edge.} \end{cases} \quad (84)$$

where average and maximum deviations between the threshold data and the fit formulas are $\sim 5^\circ$ and $\sim 8^\circ$ for the left-edge and $\sim 2^\circ$ and $\sim 3^\circ$ for the right-edge. Here, we have neglected weak η and σ_0 variation in the formula for the left-edge of the band and we have neglected variation in σ_0 on the right-edge to produce formulas of similar accuracy to the breathing band. Methods employed by Lee and Briggs[17] to analytically estimate breathing mode band widths for a focusing function $\kappa(s)$ with a constant and sinusoidally varying terms may be generalizable using Fourier expansions of both the piecewise constant lattice focusing function $\kappa(s)$ employed here and the matched envelope to calculate thresholds of the decoupled breathing and quadrupole bands. Future research on this topic is desirable to obtain more reliable band threshold estimates and to better understand the structure of the envelope instabilities.

As discussed in Sec. IIF, the breathing and quadrupole modes are decoupled, and consequently pure modes can be simply launched at axial coordinate $s = s_i$ by taking initial conditions as given in Eqs. (53) and (54). This launching condition is illustrated in Fig. 6 and corresponds to cases (a) and (c) in Table I for stability and instability, respectively. For the case of instability, Table I and Figs. 4 and 5 show that certain subsets of initial conditions with either breathing or quadrupole symmetry can project onto pure exponentially damping or growing modes. Mode phase-space invariant (see Sec. IIF and Appendix E) can be employed analogously to Courant-Snyder invariants in single-particle dynamics to efficiently launch stable breathing or quadrupole modes with specific amplitudes and phases and calculate maximum mismatch excursions at any location in the lattice period.

As a practical matter, note in the parametric plots of the bands of mode instability presented in Fig. 12 that the breathing mode band is encountered before the quadrupole band when approaching from lower values of σ_0 . Therefore the breathing mode instability is generally of greater importance in the selection of machine operating points. Finally, it should be stressed that the breathing mode results presented can be interpreted directly as being laboratory frame, but the quadrupole mode rotates according to the local Larmor frame transformations presented in Appendix B. Breathing mode stability results presented are also valid for beams with finite canonical angular momentum $P_\theta \neq 0$, whereas quadrupole mode results are valid only for $P_\theta = 0$.

V. ENVELOPE MODES IN QUADRUPOLE DOUBLET FOCUSING CHANNELS

In this section, we explore normal mode envelope perturbations ($\delta\mathbf{P} = 0$) in alternating gradient quadrupole focusing channels. Driving perturbations with $\delta\mathbf{P} \neq 0$ are not analyzed. Results are presented in analogous manner to Sec. IV for solenoidal focusing. However, in contrast to Sec. IV, all results are laboratory frame and can be interpreted directly without transformation. The beam considered in this section has zero total canonical angular momentum $P_\theta = \langle xy' - yx' \rangle_\perp = 0$ and the focusing channel has no skew couplings so that the envelope equations (4) apply (see Appendix B). Piecewise constant focusing strength $\kappa_x(s) = -\kappa_y(s) \equiv \kappa_q(s)$ is taken and results can be applied to realistic focusing channels with continuously varying $\kappa_q(s)$ using the equivalency procedures developed in Appendix A.

A. Matched envelope solution

We consider the case of a periodic, matched solution ($r_j = r_{jm}$ for $j = x, y$) to the the envelope equations (4) with equal emittances $\varepsilon_x = \varepsilon_y = \varepsilon$. A hard-edge focusing lattice is assumed with piecewise constant $\kappa_x(s) = -\kappa_y(s) \equiv \kappa_q(s)$ as illustrated in Fig. 2(c) with lattice period L_p , quadrupole strength $\widehat{\kappa_q} = \text{const}$, occupancy η , and syncopation factor α . The matched envelope solutions are parameterized by L_p , σ_0 , σ/σ_0 , η , and α . Numerical solutions are plotted for one lattice period in Fig. 15 in terms of scaled envelope radii $[r_j/(\sqrt{2Q}L_p)]$ versus normalized axial coordinate (s/L_p) for $\alpha = 1/2$ [FODO channel, (a)] and $\alpha = 0.1$ [strong syncopation, (b)]. In these plots, the undepressed single-particle phase advance σ_0 is fixed, and the solution is shown for values of σ/σ_0 . Approximate, analytical solutions can also be constructed using the perturbative formulation of Lee[18]. Symmetry points are indicated on the plot. Contrasting (a) and (b), observe that syncopation with $\alpha \neq 1/2$ reduces the symmetry of the matched envelope but that maximum excursions change little. In contrast to solenoidal transport channels, at fixed σ_0 , little variation in matched envelope structure is observed with changes in quadrupole occupancy η . The value of occupancy employed $\eta = 0.6949$ corresponds to the hard-edge equivalent value of a FODO electric quadrupole lattice in the High Current Transport Experiment (HCX) at the Lawrence Berkeley National Laboratory[24, 25]. This equivalence prescription is derived as an example application in the general discussion of fringe field equivalent models presented in Appendix A. Negligible difference in the structure of the matched beam envelope is observed between the actual focusing function $\kappa_q(s)$ derived from the linear applied field components of the physical lattice and the hard-edge equivalent model with piecewise constant $\kappa_q(s)$.

B. Normal modes

Normal mode solutions are numerically analyzed using the formulation in Sec. IIF. For the matched beam solutions described in Sec. VA, mode perturbations are not simply decoupled by sum (+) and difference (−) coordinates $\delta r_\pm = (r_x \pm r_y)/2$ as in the case of continuous and solenoidal focusing channels analyzed in Secs. III and IV, and we employ the full coupled eigenvalue formulation based on Eq. (38) with $\kappa_x = -\kappa_y = \kappa_q$, $\varepsilon_x = \varepsilon_y = \varepsilon$, and zero driving perturbations ($\delta\mathbf{P} = 0$). Eigenvalues are calculated for specified values of η and α and ranges of σ_0 and σ/σ_0 to map out mode properties. Results we obtained are displayed in Figs. 16–20. Although sum and difference perturbations

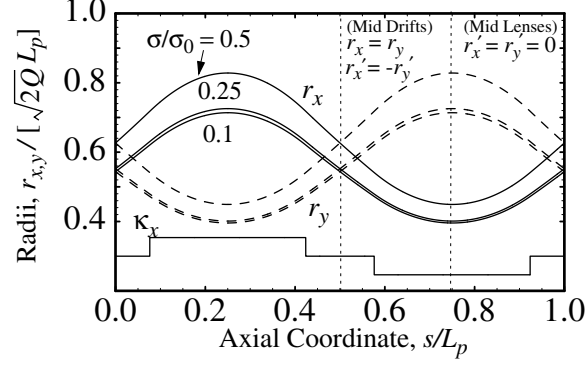
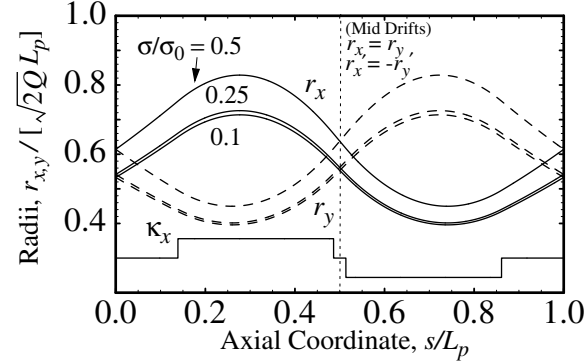
a) Matched Envelope for $\sigma_0 = 80^\circ$, $\eta = 0.6949$, and $\alpha = 1/2$ b) Matched Envelope for $\sigma_0 = 80^\circ$, $\eta = 0.6949$, and $\alpha = 0.1$ 

FIG. 15: Scaled matched beam envelope $r_j/(\sqrt{2Q}L_p)$ versus normalized axial coordinate s/L_p for one period of a hard-edge quadrupole focusing channel in Fig. 2(c). Solutions are shown for $\sigma_0 = 80^\circ$, $\eta = 0.6949$, and values of σ/σ_0 indicated for syncopation factors $\alpha = 1/2$ (FODO) and $\alpha = 0.1$ in (a) and (b), respectively.

are not decoupled in quadrupole transport channels, we find that the pure modes have properties analogous to the sum (i.e., “breathing”) and difference (i.e., “quadrupole”) modes studied in continuous and solenoidal channels. We label envelope modes in the quadrupole focusing channel that in stable regions degenerate into quadrupole- and breathing-like perturbations with B and Q , respectively, (e.g. σ_ℓ with $\ell = B, Q$ for the mode phase advances) to avoid confusion with the purely decoupled sum and difference modes analyzed in Secs. III and IV.

The “breathing” and “quadrupole” mode phase advances σ_B and σ_Q and growth factors γ_B and γ_Q are contoured in Fig. 16 as a function of σ_0 and σ/σ_0 for $\sigma_0 \in (0, 180^\circ)$ and $\sigma/\sigma_0 \in (0, 1]$. Results are shown for quadrupole occupancy $\eta = 0.6949$ and syncopation factors $\alpha = 1/2$ (FODO lattice) and $\alpha = 0.1$ in columns (a) and (b) to contrast a symmetrical FODO lattice with the case of strong syncopation. Growth factors of both the breathing ($\gamma_B > 1$) and quadrupole ($\gamma_Q > 1$) modes are superimposed on the same plots because the bands do not overlap, and growth factors of the corresponding damped modes are not plotted because damping factors are given by $1/\gamma_\ell$ of the growing mode [see Fig. 4 and Table I]. No instability bands are found for $\sigma_0 < 90^\circ$ so the growth contours are restricted to $\sigma_0 \in (90^\circ, 180^\circ)$. In terms of the symmetry classes presented in Fig. 4, eigenvalues fall into class (a) when there is stability and class (b) [confluent resonance] or (c) [lattice resonance] when there is instability. The confluent resonance involves locking of the breathing and quadrupole modes and occurs for both FODO and syncopated ($\alpha \neq 1/2$) lattices, while the lattice resonance is observed only for syncopated lattices (see the thin band to the left of confluent resonance band on the right column of the figure) which have a lesser degree of symmetry. The lattice resonance also only appears for the breathing mode. As for solenoidal transport, the breathing mode instabilities appear to be more dangerous for practical, intense beam transport lines because it is encountered first when increasing σ_0 from small values. These plots help clarify regions of parametric envelope instability observed in previous studies of FODO lattices[4, 21] and a syncopated quadrupole lattice[7]. The thin band associated with the lattice resonance for syncopated quadrupole lattices was previously overlooked. Also, mode branches are unambiguously identified, errors in branch calculations are corrected, and parametric sensitivities and mode properties are thoroughly characterized over the range of practical machine parameters.

To better illustrate the mode structures presented in Fig. 16, in Fig. 17 we plot the mode phase advances and

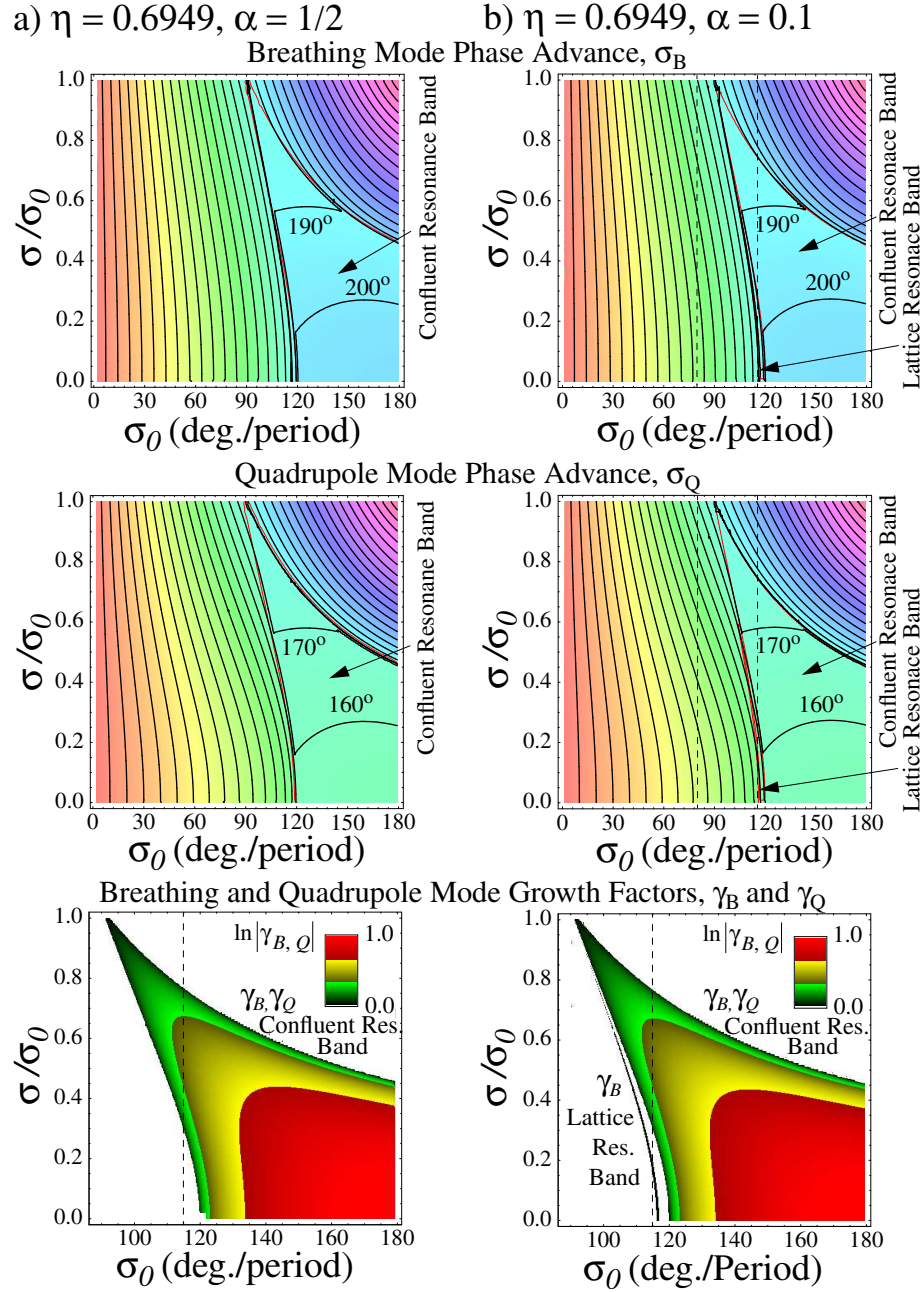


FIG. 16: Contours of (upper row) breathing and (middle row) quadrupole mode phase advances (σ_B, σ_Q) and (bottom row) growth factors (γ_B, γ_Q) as a function of σ_0 and σ/σ_0 for a quadrupole focusing channel with occupancy $\eta = 0.6949$. Results are shown for synchopation factors $\alpha = 1/2$ (FODO) and $\alpha = 0.1$ in columns (a) and (b). In the upper and middle rows, black contour lines correspond to $\sigma_\ell = 10^\circ, 20^\circ, 30^\circ, \dots$ for $\ell = B, Q$, colors vary continuously with changes in σ_ℓ , and thresholds of instability bands are marked with red lines. In the bottom row, values of $\ln(\gamma_\ell)$ with $\gamma_\ell > 1$ are labeled with continuously varying colors as indicated in the key. Identical color schemes are used in columns (a) and (b) to measure mode phase advances and growth factors. Vertical dashed lines in the plots of $\alpha = 0.1$ correspond to cross-section plots in Fig. 17.

growth factors for fixed σ_0 , α , and η as a function of σ/σ_0 . Curves shown correspond to the vertical dashed lines on the contour plots in Fig. 16. Complex plots of the eigenvalues λ_n relative to the unit circle are superimposed at several locations to further illustrate the eigenvalue structure of the modes. Individual mode branches for the breathing and quadrupole modes are identified outside of regions of instability using the formulation described in Sec. II F and branches are continuously connected across bands of parametric instability. The phase advance of the breathing mode σ_B is larger than the quadrupole mode σ_Q for finite space-charge ($\sigma/\sigma_0 < 1$). Continuous focusing model predictions shown for the sum (i.e., breathing) and difference (i.e., quadrupole) mode phase advances σ_+ and σ_-

are derived from Eq. (64) using the single-particle phase advances σ_0 and σ calculated from the periodically focused, matched beam. Far from bands of instability, σ_+ and σ_- provide accurate estimates for the numerically calculated breathing and quadrupole mode phase advances σ_B and σ_Q [7]. This correspondence helps justify the identification of the mode branches being breathing- and quadrupole-like. The continuous focusing and alternating gradient model phase advances are in better agreement for lower values of σ_0 and weaker syncopation ($\alpha \rightarrow 1/2$). Analysis in Sec. II F [see Eq. (56)] shows that the zero space-charge limit $Q \rightarrow 0$ corresponds to stable breathing and quadrupole mode oscillations with

$$\begin{aligned} \lim_{\sigma \rightarrow \sigma_0} \sigma_\ell &= 2\sigma_0, \\ \lim_{\sigma \rightarrow \sigma_0} \gamma_\ell &= 1. \end{aligned} \quad (85)$$

These limiting values are indicated on the figure to provide a partial check.

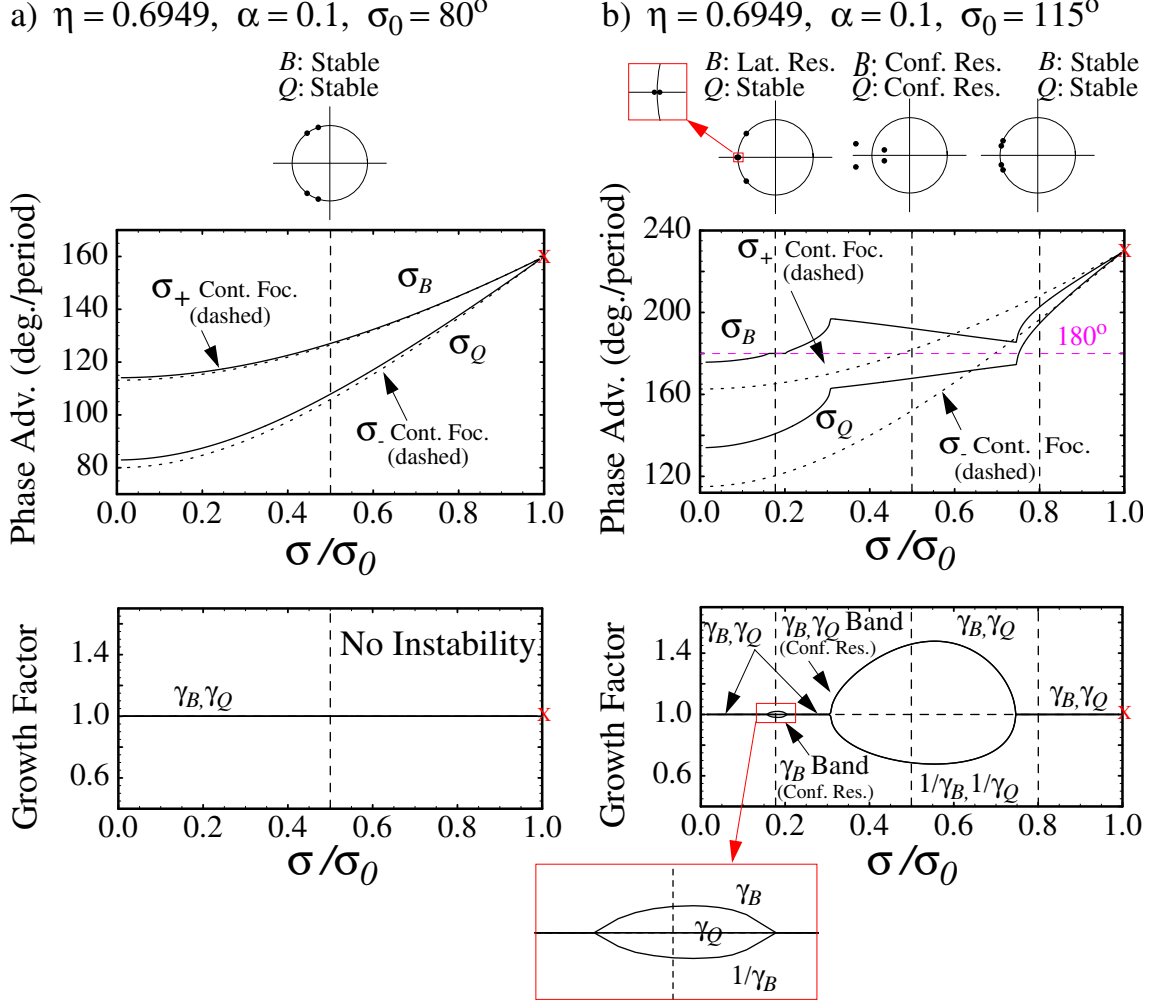


FIG. 17: Phase advance (σ_B and σ_Q) and growth factors (γ_B and γ_Q) of the breathing and quadrupole envelope modes versus σ/σ_0 for a quadrupole focusing channel with occupancy $\eta = 0.6949$, syncopation factor $\alpha = 0.1$, and $\sigma_0 = 80^\circ$ and $\sigma_0 = 115^\circ$ in columns (a) and (b). Continuous focusing model predictions for σ_\pm are superimposed on the phase advance plots (dashed curves). Red Xs mark analytical results in the zero space-charge limit. Vertical dashed lines correspond to locations of plots of complex eigenvalues λ_n placed above. Red boxes denote expanded views.

For FODO lattices with the same values of the particle phase advances σ_0 and σ , little variation is observed in envelope mode structure with changes in quadrupole occupancy η . On the other hand, significant variations can occur in lattices with strong syncopation (α far from $1/2$). To illustrate this point, the mode phase advances σ_B and σ_Q and growth factors γ_B and γ_Q are plotted in Fig. 18 for several values of η . Results are contrasted in columns (a) and (b) for a FODO lattice ($\alpha = 1/2$) and a strongly syncopated lattice with $\alpha = 0.1$. The small variations presented in Fig. 18(a)

illustrate the insensitivity of the mode structure to changes in η for a FODO lattice. The location and strength of the confluent resonance instability band changes only weakly with η . Even smaller variations are observed in FODO lattices when making comparisons for σ_0 farther from the first instability band or when comparing results for the hard-edge lattice taken here with full fringe field models calculated from physical lattices (see Appendix A). Results from eigenvalues analytically calculated in Appendix G for the thin-lens limit ($\eta \rightarrow 0$ at fixed σ_0) of a FODO lattice with a fully space-charge depressed beam ($\sigma = 0$) are indicated in Fig. 18(a). The good agreement with the thin-lens results is traceable to mode structure in a FODO lattice being relatively insensitive to the solenoid occupancy η . For FODO lattices, σ_0 and σ are the most important parameters, whereas shape parameters characterizing the occupancy and fringe components of the focusing field are of much lesser importance. In contrast, for strong syncopation, it is evident from Fig. 18(b) that the mode structure can vary significantly with occupancy η . This strong variation is correlated to the existence of the second band of parametric instability (lattice resonance) for the breathing mode, which was shown in Sec. IV to vary strongly with η in a solenoidal focusing lattice. Observe from the $\alpha = 0.1$ plots in Fig. 18(b) that the instability band of the lattice resonance is weakly expressed compared to the confluent resonance band for higher lattice occupancies η , whereas it is strongly expressed for η small. High resolution numerical studies suggest that the lattice resonance instability band disappears (becoming both thinner and weaker) as $\alpha \rightarrow 1/2$.

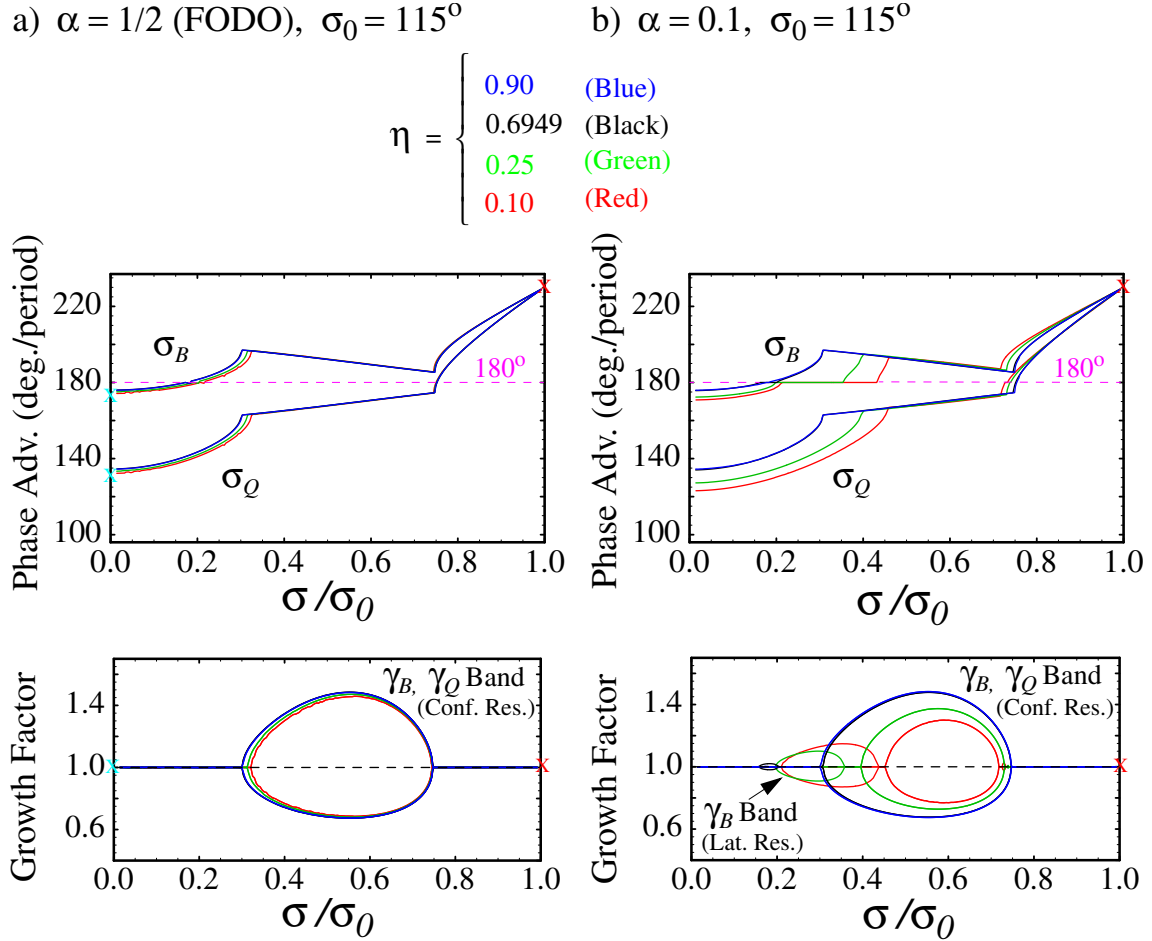


FIG. 18: Variation of mode structure with quadrupole occupancy η and syncopation factor α . Phase advance (σ_B and σ_Q) and growth factors (γ_B and γ_Q) of the breathing and quadrupole modes are plotted versus σ/σ_0 for $\sigma_0 = 115^\circ$ and the indicated values of η . Results are contrasted in columns (a) and (b) for $\alpha = 1/2$ (FODO) and $\alpha = 0.1$ (strong syncopation). Red **X**s mark analytical results in the zero space-charge limit, and **X**s mark thin-lens limit ($\eta \rightarrow 0$) analytical results for a FODO focusing with $\sigma/\sigma_0 = 0$.

The confluent resonance instability band has been identified as a half-integer parametric resonance between both envelope mode oscillation frequencies and the lattice, and the lattice resonance instability band has been identified as a half-integer parametric resonance between one envelope mode and the lattice[7]. This suggests that the location of the envelope bands can be crudely estimated using resonance conditions based on the breathing and quadrupole mode frequencies σ_\pm derived from the continuous model with $\sigma_+ = \sqrt{2\sigma_0^2 + 2\sigma^2}$ and $\sigma_- = \sqrt{\sigma_0^2 + 3\sigma^2}$ [see Eq. (64)]

as $(\sigma_+ + \sigma_-)/2 = \pi$ for the confluent resonance band and $\sigma_+ = \pi$ for the lattice resonance band, or equivalently with σ_0 and σ measured in degrees,

$$\sqrt{2\sigma_0^2 + 2\sigma^2} + \sqrt{\sigma_0^2 + 3\sigma^2} = 360^\circ \quad (86)$$

for the confluent resonance band (both breathing and quadrupole modes), and

$$\sqrt{2\sigma_0^2 + 2\sigma^2} = 180^\circ \quad (87)$$

for the lattice resonance band (breathing mode). Comparing to Fig. 16, Eq. (86) roughly predicts the maximum growth factor in the confluent resonance band for the breathing and quadrupole modes, and Eq. (87) roughly predicts the location of the thin lattice resonance band associated with the breathing mode in syncopated lattices. However, the formulas cannot capture broad parametric nature of the instability or changes in band structure with solenoid occupancy η or syncopation factor α . Moreover, Eq. (87) fails to suggest the non-existence of the band for FODO lattices with $\alpha = 1/2$. In order to provide some guidance for band locations in practical applications, parametric data was employed to calculate curve fits for the instability thresholds for a FODO lattice. A least-squares fit was carried out using a large amount of threshold data for the confluent resonance band. Elliptic and linear boundary constraint equations in σ_0 and σ measured in degrees were applied with forms:

$$\sigma^2 + f(\eta)\sigma_0^2 = (90^\circ)^2[1 + f(\eta)], \quad (88)$$

for the left-edge of the FODO confluent resonance band, and

$$\sigma + g(\eta)\sigma_0 = 90^\circ[1 + g(\eta)], \quad (89)$$

for the right-edge of the FODO confluent resonance band. Here, $f(\eta)$ and $g(\eta)$ are functions to be determined by fitting the data, and the forms taken correspond to the most general centered ellipse and line containing the limit point $\sigma = \sigma_0 = 90^\circ$. We find very little variation in η when fitting to these forms (almost to the accuracy of the numerical data) and errors are minimized by taking

$$\begin{aligned} f(\eta) &= \frac{4}{3}, \\ g(\eta) &= \frac{1}{9}. \end{aligned} \quad (90)$$

Maximum errors (all η values) in threshold prediction from Eqs. (88)–(90) are $\sim 5^\circ$ and $\sim 2^\circ$ for the left- and right-edge of the band, respectively. No two-dimensional curve fits were attempted to understand and characterize the more intricate band changes observed in a syncopated quadrupole lattice with $\alpha \neq 1/2$. Generalizations of methods employed by Lee and Briggs[17] using Fourier expansions of the lattice focusing function $\kappa_q(s)$ might be employed to derive analytical formulas to better understand the instability thresholds. This topic is left for future research.

To further illustrate the mode structure, pure mode launching conditions in $\delta\mathbf{R} = (\delta r_x, \delta r'_x, \delta r_y, \delta r'_y)$ are plotted in Fig. 19 for both the breathing and quadrupole modes. Launching conditions are plotted at axial locations corresponding to matched beam symmetry points in a FODO lattice: the axial mid-drift with focusing- and defocusing-in- x quadrupoles at smaller and larger s values, and mid-quadrupole within a focusing-in- x quadrupole. Launching conditions at the other axial mid-drift and mid-defocusing-quadrupole locations are simply derivable by symmetry from the plots shown. The launching conditions employed are described in Table I and coordinates and angles are scaled as $\delta r_j/(\sqrt{2Q}L_p)$ and $\delta r'_j/\sqrt{2Q}$. Mode amplitudes A_ℓ with $\ell = B, Q$ are selected so that the maximum excursions in $|\delta r_j|$ for the pure mode are 10% of the average matched beam radius {i.e., $\text{Max}[\delta r_j(\psi_\ell)] = 0.1(1/L_p) \int_0^{L_p} ds \sqrt{r_{xm}r_{ym}}$ } and launching conditions are plotted versus mode phase ψ_ℓ for $-\pi \leq \psi_\ell \leq \pi$ (the absolute value of the phases are arbitrary). Parameters chosen for Fig. 19 correspond to stable modes with eigenvalues and launching conditions falling into class (a) in Fig. 4 and Table I. To launch a stable mode with a prescribed maximal excursion in $\delta r_j(s)$, it suffices to select a particular axial location $s = s_i$ of interest, calculate needed eigenvectors for the full lattice period as a function of s , calculate the maximum value of $|\delta r_j(s_i)|$ with respect to both s and the mode phase ψ_ℓ , and then scale the mode amplitude A_ℓ such that this maximum value equals the prescribed excursion. Outside of exceptional cases where the mode phase advance σ_ℓ is a rational fraction of 2π (i.e., the lattice phase advance), this maximal excursion will be approached arbitrarily close as the beam propagates through the periodic lattice.

Comparing the launching conditions in Fig. 19, we observe that initial conditions in δr_j and $\delta r'_j$ for pure quadrupole or breathing mode launches vary significantly in form with the axial location within the lattice period. This contrasts the situation for the decoupled sum and difference modes analyzed in Secs. III and IV for continuous and solenoidal

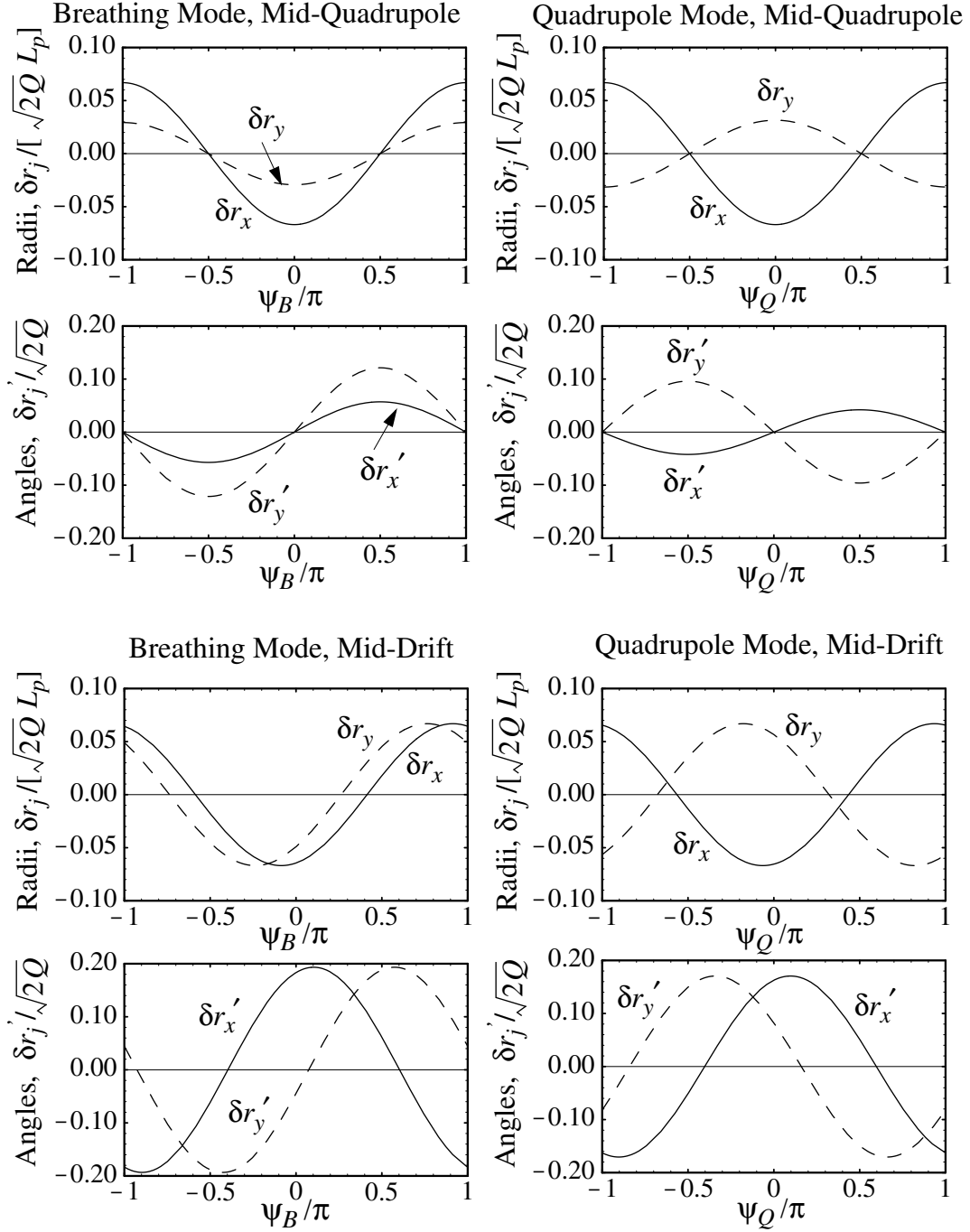


FIG. 19: Scaled pure mode launching conditions in $\delta r_j/(\sqrt{2Q}L_p)$ and $\delta r'_j/\sqrt{2Q}$ ($j = x, y$) plotted versus mode phase ψ_ℓ ($\ell = B, Q$) for stable breathing and quadrupole modes at the axial mid-drift (upper-half) and mid-quadrupole (lower-half) locations in a FODO lattice. Parameters chosen are $\eta = 0.6949$, $\alpha = 1/2$ (FODO), $\sigma_0 = 80^\circ$, and $\sigma/\sigma_0 = 0.2$.

focusing channels. In these decoupled cases the launching conditions are the same form independent of axial location [see Eqs. 53 and (54)] and, to launch a given mode amplitude, only the relative projections on the normal mode coordinates and angles vary with axial location in the lattice period. The decoupled mode launch conditions in Eqs. (53) and (54) are a poor approximation to the pure breathing and quadrupole modes launching conditions for an alternating gradient channel even though the modes have rough breathing and quadrupole symmetry for specific launch phases and axial coordinate locations. Thus the use of the continuous model as a guide for pure mode launchings in alternating gradient focusing lattices (common in simulations studies etc.) can result in significant launching errors with unwanted projections on the mode desired to be suppressed. A useful reduced prescription for stable pure mode

launching ($\sigma_0 < 90^\circ$) at the mid axial location of a focusing-in- x quadrupole in a FODO lattice (where the x excursion of r_{xm} is maximum and the y excursion in r_{ym} is minimum) is to take δr_x to be a specified fraction of δr_y and zero perturbed angles ($\delta r'_j = 0$). By symmetry, analogous launching conditions with the same fractions apply at the mid axial location of a focusing-in- y quadrupole. The numerically calculated excursion ratio $\delta r_x/\delta r_y$ needed for this pure mode launch is illustrated in Fig. 20. The excursion ratio is plotted separately for pure breathing and quadrupole mode launches as a function of σ_0 for several values of quadrupole occupancy η and σ/σ_0 . Observe that the excursion ratio varies weakly in both occupancy η and space-charge depression σ/σ_0 relative to variations in σ_0 . For approximate launches these variations in η and σ/σ_0 can sometimes be neglected and the curves shown can then be applied for values of these parameters not shown. Observe that for decreasing values of σ_0 the excursion ratio approaches unity. This is expected because alternating gradient focusing is better approximated by continuous focusing for lower values of σ_0 [3]. The launching conditions illustrated in Fig. 20 hold only for a lattice with FODO symmetry ($\alpha = 1/2$) and are violated if the lattice is synchrotroned with $\alpha \neq 1/2$.

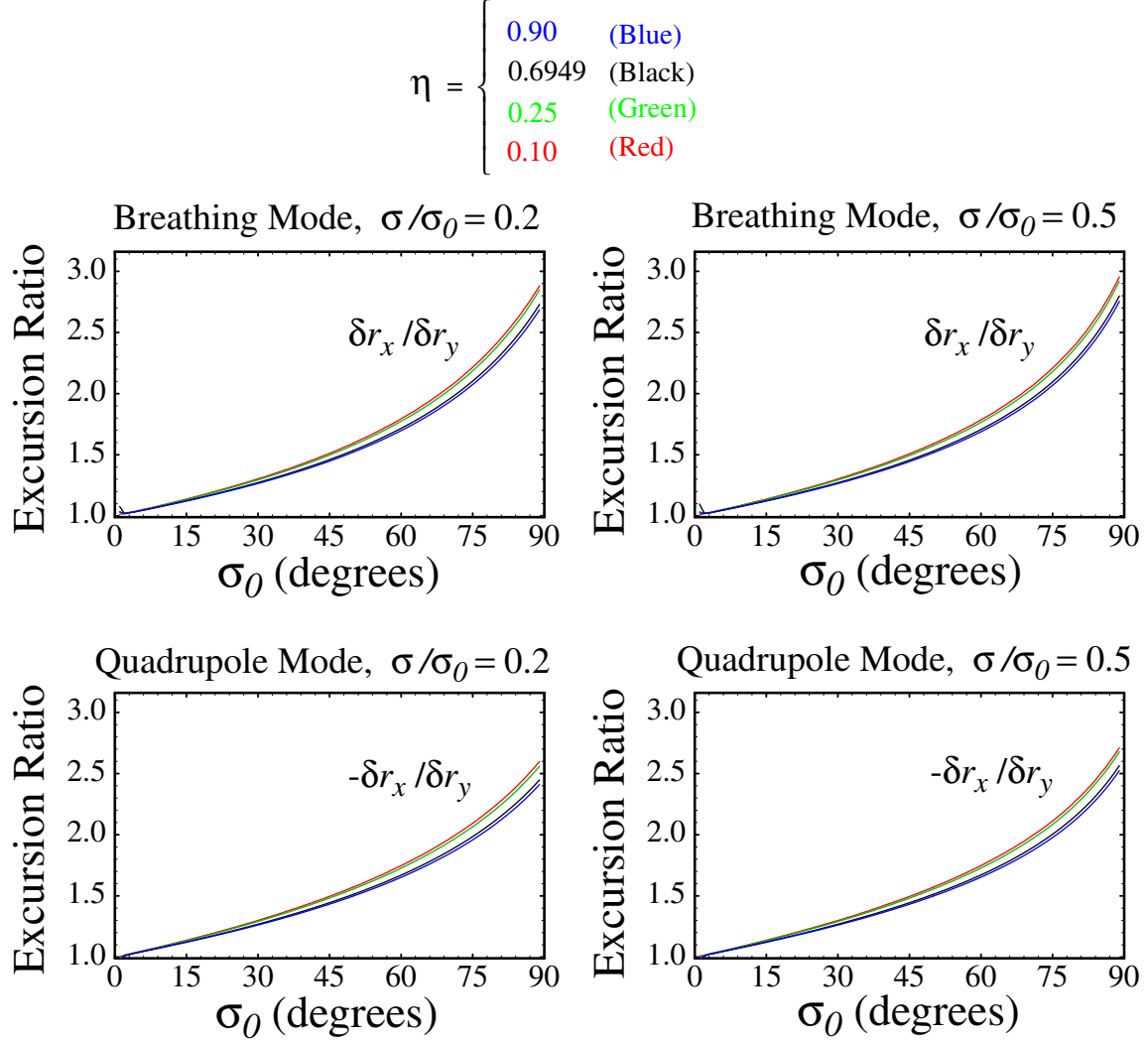


FIG. 20: Ratio of $\delta r_x/\delta r_y$ as a function of σ_0 for breathing (upper row) and quadrupole (lower row) mode launches at the axial midpoint of a focusing-in- x quadrupole in a FODO ($\alpha = 1/2$) lattice. Both launch conditions have $\delta r'_x = 0 = \delta r'_y$ and are shown for $\sigma/\sigma_0 = 0.2$ (left column) and $\sigma/\sigma_0 = 0.5$ (right column) and the indicated values of η .

VI. CONCLUSIONS

This study extends the present understanding of the stability properties of mismatch modes supported by the KV envelope equations describing the transverse evolution of a coasting, unbunched beam envelope. New, generalized

linear perturbation equations were derived that describe mismatch evolution resulting from both the usual mismatch source of errors in envelope coordinates from the periodic matched-beam condition as well as driving errors in focusing, perveance, and emittance. Important general properties of undriven envelope modes were analyzed including symmetry classes, zero space-charge limits, and phase-space invariants. The linear perturbation equations were solved in general for continuous focusing channels, and example solutions presented illustrate important differences in the action of adiabatic and sudden driving errors as well as the scaling of contributions to the breathing and quadrupole mismatch modes from the driving errors. The normal modes in the absence of driving errors were also parametrically analyzed in hard-edge, periodic solenoidal and syncopated, alternating gradient quadrupole focusing channels. This analysis extended earlier work by Struckmeier and Reiser[7] by systematically identifying possible envelope instabilities over a wide range of system parameters, thereby providing valuable data for practical applications. For solenoidal focusing, a systematic derivation of the consistent KV distribution identified invariant emittances and the appropriate Larmor frame transformation to interpret the analysis under — both of which are necessary for elliptical beam perturbations and were overlooked in earlier studies. It was shown that the solenoid occupancy strongly influences stability properties and that “quadrupole” symmetry envelope perturbations are generally less critical than “breathing” symmetry envelope perturbations for intense beam transport, thereby simplifying design considerations. For a quadrupole focusing, a previously overlooked mode was found associated with syncopated doublet lattices where one drift between quadrupoles is shorter than the other. For both solenoidal and quadrupole focusing channels, pure mismatch mode launching conditions were constructed. Exact launching conditions were specified for pure breathing or quadrupole envelope mode evolutions in solenoidal channels and approximate launch conditions were formulated for quadrupole focusing channels at lattice symmetry points. These new results provide insight on beam envelope control and have important applications in envelope matching including possible halo mitigation through breathing mode suppression, and in simulation studies.

The present study is limited in that only specific (though representative) cases of linear solenoidal and quadrupole focusing lattices have been analyzed. Also, analysis of properties of mode evolutions due to driving term errors in focusing, perveance, and emittance in periodic focusing channels is left for future study.

APPENDIX A: FRINGE FIELD EQUIVALENT MODELS FOR APPLIED FOCUSING ELEMENTS

Physical electric or magnetic focusing elements in the laboratory have material structures that produce applied fields consistent with the three-dimensional Maxwell equations. The resulting fields will, in general, contain both linear components that contribute to the applied focusing functions $\kappa_j(s)$ (see Sec. II B) as well as nonlinear error terms outside the scope of this paper. Typically, the material extent of a focusing element is axially long relative to the transverse extent of its clear-bore aperture. Near the axial mid-plane, the elements in this case can often be regarded as two-dimensional axially extruded structures, and the fields within this region can then be well-approximated by lower-dimensional models. Near the ends, this lower-dimensional approximation breaks down, and there are significant field variations as well as unwanted nonlinear field terms. In many cases the ends have approximate left-right symmetries about the axial mid-plane of the element. Consistent with these field variations in the element, the linear focusing functions $\kappa_j(s)$ of the lattice will generally vary in s : typically with near constant value in the neighborhood of the axial mid-plane till the end regions are approached, then smoothly dropping to exponentially small values outside of the ends. This s -variation near the ends is called the fringe field and is associated with all physical focusing elements — leading to the obvious question on how well so-called hard-edge lattice models with piecewise constant $\kappa_j(s)$ such as introduced in Sec. II B apply to physical lattices.

Differences between physical and hard-edge focusing functions $\kappa_j(s)$ can be regarded as driving perturbations [i.e., the $\delta\kappa_j(s)$ in Sec. II F] about a hard-edge lattice. Alternatively, the physical and hard-edge focusing functions can be thought of as producing different matched beam envelopes for the same beam parameters with deviations between these matched envelopes leading to possible variations in envelope mode structure about the matched beam. In either case, prescriptions must be given for best possible choices of “equivalent” hard-edge focusing parameters. In this Appendix we take the latter interpretation of the physical and model (hard-edge or otherwise) focusing functions giving different matched envelopes and develop procedures for fixing “equivalent” model focusing functions to the physical lattice that minimize deviations between physical and model matched beam envelopes. No fully general optimal procedure can be given, because deviations depend on the specific lattice considered and the structure of the matched envelope. With regards to low-order beam evolutions modeled by the KV envelope equations (4), we generally find that hard-edge models produce results that are close to physical models for a *periodic* lattice if appropriate, “equivalent” hard-edge equivalent parameters (e.g., for solenoids the occupancy η and focusing strength $\hat{\kappa}$) are employed. The level of agreement improves for simpler lattices with higher degrees of symmetry [e.g., the solenoidal and quadrupole hard-edge lattices introduced in Sec. II B]. This agreement is likely a consequence of compensating errors and that periodic focusing “kicks” in a repeating solution can be well modeled by kicks of varying shape that impart the same total

impulse. On the other hand for more general lattices and evolutions (e.g., a matching section where beam envelope parameters are transformed and there is no periodicity), uncompensated accumulated phase errors in the envelope excursions can result in significant errors if accurate fringe-field models are not employed.

No unique prescription exists on how to best fix parameters employed to model $\kappa_j(s)$ for either hard-edge models or for more detailed fringe-field models. In both cases we refer best fit model parameters as “equivalent fringe” parameters. Here we outline several reasonable procedures that can be used to fix equivalent fringe parameters.

One way to fix equivalent fringe parameters is through the dynamics of the particles. Equating matrix elements of the 2×2 transfer maps $\mathbf{M}_j(s|s_i)$ [see Eq. (19)] connecting one side of the optic before the fringe entering the focusing element to the end of the fringe leaving the focusing element will result in equivalent evolutions in drift regions. It is usually sufficient to carry out such procedures only for the undepressed orbits ($Q = 0$ maps) which provide a direct measure of the applied focusing functions. This will result in three, rather than four, independent constraints in each of the x - and y -planes (the x - and y -planes can yield identical or related constraints for some optics) because $\mathbf{M}_j(s|s_i)$ is symplectic and has a unit determinant. Unfortunately, these kinematic methods of fixing equivalent fringe parameters prove less than satisfactory in practical applications because they do not result in scale invariant models and must be repeated with changes in particle energy. Moreover, if there are more equivalent fringe parameters than kinematic constraints employed, the method is ambiguous and must be supplemented by additional constraints.

Because of these limitations, we employ an alternative, non-kinematic method of fixing equivalent fringe field parameters defined as follows. Denote the physical and equivalent fringe model focusing functions by $\kappa_j(s)$ and $\kappa_{fj}(s)$. Then we specify $\kappa_{fj}(s)$ by requiring:

- (1) Equal focusing strength at the mid-planes of the elements, i.e.,

$$\kappa_{fj}(s_m) = \kappa_j(s_m),$$

where $s = \{s_m\}$ are the axial coordinates of the mid-planes of the physical focusing elements.

- (2) Correct integrated focusing strength in each focusing element, i.e.,

$$\int_{\text{element}} ds \kappa_j(s) = \int_{\text{element}} ds \kappa_{fj}(s),$$

where the integration range contains the full fringe field of the physical and equivalent elements.

- (3) Minimum least square error between the physical and fringe equivalent lattices. Here, we take the error measure to be given by

$$\text{error} = \int_{s_i}^{s_i + L_p} ds [\kappa_j(s) - \kappa_{fj}(s)]^2.$$

The constraint (1) allows easy understanding of the overall “excitation” needed for the focusing element. The physical element focusing strength $\kappa_j(s_m)$ can also be replaced in (1) by lower-dimensional optical models (e.g. a 2D analytical quadrupole model) to allow analytical estimates of needed excitations. The constraint (2) maintains a good low-order equivalency of focusing strength. To obtain higher-precision equivalences, (2) can be replaced by a constraint for equal values of the single particle phase advance σ_{0j} in the physical and equivalent lattices to obtain partial kinematic equivalency. Finally, (3) constrains any additional parameters after (1) and (2) establish low-order equivalency. Note that $\kappa_{fj}(s) = \kappa_j(s)$ corresponds to zero error and an identical kinematic transfer matrix $\mathbf{M}_j(s|s_i)$ between all points in the lattice with or without space-charge. Constraints (2) and (3) both recover the correct thin-lens limit. Additional criteria can also be added to the error function in (3) to further constrain the equivalent fringe model for minimum envelope excursions and other criteria[26]. For the special case of solenoidal and FODO quadrupole lattices with piecewise constant $\kappa_j(s)$ as defined in Sec. II B, only two equivalent lattice parameters need be set (e.g., $\hat{\kappa}$ and η for the solenoidal lattice) for which the first two constraints are sufficient and the third error constraint is not needed.

We illustrate the results of this equivalent fringe procedure with the FODO electric quadrupole lattice of the High Current Transport Experiment (HCX) at the Lawrence Berkeley National Laboratory[24, 25]. As shown in cross-section in Fig. 21(a), the quadrupoles are formed from left and right conducting end-plates held at equal magnitude positive and negative biases and conducting rods attached to each end-plate along the principal x - and y -axes as indicated. The structure is mechanically supported at the axial mid-plane by a plate connected to the end-plates by insulators, end-plates are 12.7mm thick with clear-bore aperture holes of radii $r_p = 23.0\text{mm}$, rods are of radii $\sim (8/7)r_p = 26.3\text{mm}$ (ratio chosen to minimize nonlinear fields in 2D axial extruded geometry of the mid-plane) and axial length 154.5mm, and gaps between rods and end-plates are 17.7mm. The quadrupoles are arranged with an overall lattice period of $L_p = 435.2\text{mm}$ and adjacent end-plates are biased to the same potential. This detailed lattice

equivalency procedure is applied to set geometric parameters of the equivalent lattice. These results illustrate the general feature that simple equivalent fringe models result in little change in matched envelope structure for lattices with a high degree of symmetry.

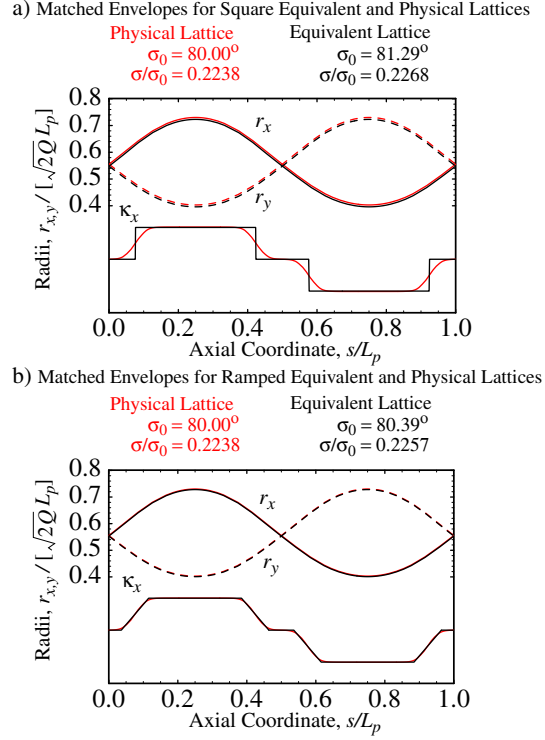


FIG. 22: Comparison of matched beam envelopes calculated from a full fringe field model (red) and an equivalent fringe models (black) for (a) the a square-edge and (b) the ramped-edge models shown in Fig. 21. The presentation format of the matched solutions is the same as in Fig. 15. Both the physical and equivalent fringe model lattices have the same quadrupole excitation, beam parameters are $Q = 8. \times 10^{-4}$ and $\varepsilon_x = \varepsilon_y = 60$. mm-mrad, and the undepressed and depressed single particle phase advances σ_0 and σ are listed above the plots.

APPENDIX B: LARMOR-FRAME TRANSFORMATIONS FOR ANALYSIS OF SOLENOIDAL FOCUSING SYSTEMS AND SELF-CONSISTENT KV DISTRIBUTION FUNCTIONS

In situations where there is an s -varying solenoidal magnetic field $\mathbf{B}(s) = -[B'_z(s)/2](x\hat{\mathbf{x}} + y\hat{\mathbf{y}}) + B_z(s)\hat{\mathbf{z}}$ in addition to (or in place of) other physical laboratory-frame focusing forces described by $\kappa_x(s)$ and $\kappa_y(s)$ (e.g., electric or magnetic quadrupoles or a uniform, partially neutralizing background), the transverse equations of motion of a beam particle can be expressed as[3, 28]

$$\begin{aligned} x'' + \kappa_x x - k'_L y - 2k_L y' + \frac{q}{m\gamma_b^3\beta_b^2c^2} \frac{\partial\phi}{\partial x} &= 0, \\ y'' + \kappa_y y + k'_L x + 2k_L x' + \frac{q}{m\gamma_b^3\beta_b^2c^2} \frac{\partial\phi}{\partial y} &= 0. \end{aligned} \quad (\text{B1})$$

Here,

$$k_L(s) = \frac{qB_z(s)}{2m\gamma_b\beta_b c} = \frac{\omega_c}{2\gamma_b\beta_b c} \quad (\text{B2})$$

is the Larmor wavenumber, $\omega_c = qB_z/m$ is the cyclotron frequency, and $-\partial\phi/\partial x$ and $-\partial\phi/\partial y$ are the x - and y -components of the self-electric field of the beam in the electrostatic approximation. For solenoidal focusing $\kappa_x = \kappa_y = 0$ and $\int_0^{L_p} ds k_L(s)^2 \neq 0$. Note that Eq. (B1) reduces to Eq. (1) for $k_L = 0$ and $(q/m\gamma_b^3\beta_b^2c^2)\partial\phi/\partial x = -Qx/[(r_x + r_y)r_x]$

and $(q/m\gamma_b^3\beta_b^2c^2)\partial\phi/\partial y = -Qy/[(r_x + r_y)r_y]$, corresponding to the interior fields of a uniform density elliptical beam in free-space with principal axis radii r_x and r_y oriented along the x and y coordinate axes.

For solenoidal focusing, the cross-coupled form of Eq. (B1) results in a macroscopic rotation of the beam about the longitudinal axis. Because of this, we analyze the particle equations in a $\tilde{x} - \tilde{y}$ coordinate system rotated by an angle $\tilde{\psi}(s)$ relative to the $x - y$ laboratory-frame as indicated in Fig. 23 with

$$\begin{aligned}\tilde{x} &= x \cos \tilde{\psi} + y \sin \tilde{\psi}, \\ \tilde{y} &= -x \sin \tilde{\psi} + y \cos \tilde{\psi}.\end{aligned}\tag{B3}$$

Henceforth, we use tildes ($\tilde{}$) to denote quantities measured in the rotating-frame. For a uniform density elliptical beam with (possibly evolving) principal axes $\tilde{r}_{\tilde{x}} = 2\langle\tilde{x}^2\rangle_{\perp}$ and $\tilde{r}_{\tilde{y}} = 2\langle\tilde{y}^2\rangle_{\perp}$ along the rotating \tilde{x} and \tilde{y} coordinate axes (see Fig. 23), the self-field forces within the beam are given by

$$\begin{aligned}-\frac{q}{m\gamma_b^3\beta_b^2c^2}\frac{\partial\phi}{\partial x} &= \frac{2Q}{\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}}}\left(\frac{\tilde{x}}{\tilde{r}_{\tilde{x}}}\cos\tilde{\psi} - \frac{\tilde{y}}{\tilde{r}_{\tilde{y}}}\sin\tilde{\psi}\right), \\ -\frac{q}{m\gamma_b^3\beta_b^2c^2}\frac{\partial\phi}{\partial y} &= \frac{2Q}{\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}}}\left(\frac{\tilde{x}}{\tilde{r}_{\tilde{x}}}\sin\tilde{\psi} + \frac{\tilde{y}}{\tilde{r}_{\tilde{y}}}\cos\tilde{\psi}\right).\end{aligned}\tag{B4}$$

Paralleling the analysis of Wiedemann[28], we find that $\tilde{\psi}$ can be selected such that the principal axes of the uniform density elliptical beam remain aligned with the \tilde{x} - and \tilde{y} -axes as the elliptical beam evolves. This occurs when $\tilde{\psi}$ satisfies the ‘‘Larmor-frame’’ condition $\tilde{\psi}' = -k_L$ with the initial condition $\tilde{\psi}(s = s_i) = 0$, or equivalently that

$$\tilde{\psi} = -\int_{s_i}^s d\bar{s} k_L(\bar{s}).\tag{B5}$$

For this choice of $\tilde{\psi}$, the particle equations of motion (B1) can be simply expressed in the rotating ‘‘Larmor-frame’’ as

$$\begin{aligned}\tilde{x}'' + k_L^2\tilde{x} - \frac{2Q}{(\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}})\tilde{r}_{\tilde{x}}}\tilde{x} &= 0, \\ \tilde{y}'' + k_L^2\tilde{y} - \frac{2Q}{(\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}})\tilde{r}_{\tilde{y}}}\tilde{y} &= 0.\end{aligned}\tag{B6}$$

Consistent with this Larmor transform, the particle angles x' and y' transform as

$$\begin{aligned}\tilde{x}' &= x' \cos \tilde{\psi} + y' \sin \tilde{\psi} + k_L(x \sin \tilde{\psi} - y \cos \tilde{\psi}), \\ \tilde{y}' &= -x' \sin \tilde{\psi} + y' \cos \tilde{\psi} + k_L(x \cos \tilde{\psi} + y \sin \tilde{\psi}).\end{aligned}\tag{B7}$$

The particle equations of motion (B6) in the rotating Larmor-frame variables are the same form as the laboratory-frame equations of motion (1) with $\kappa_x = \kappa_y \rightarrow k_L^2$. Therefore, the usual KV analysis[29] involving transformations to phase-space invariants that are quadratic forms in conjugate phase-space variables can be employed in the rotating-frame to construct a self-consistent, KV equilibrium solution to the Vlasov equation. In the Larmor-frame, the Vlasov equation for the single-particle distribution function $\tilde{f}(\tilde{x}, \tilde{x}', \tilde{y}, \tilde{y}')$ consistent with the particle equations of motion (B6) can be expressed as

$$\frac{d}{ds}\tilde{f} = \frac{\partial}{\partial s}\tilde{f} + \tilde{x}'\frac{\partial}{\partial\tilde{x}}\tilde{f} + \tilde{y}'\frac{\partial}{\partial\tilde{y}}\tilde{f} + \left(-k_L^2\tilde{x} + \frac{2Q\tilde{x}}{(\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}})\tilde{r}_{\tilde{x}}}\right)\frac{\partial}{\partial\tilde{x}'}\tilde{f} + \left[-k_L^2\tilde{y} + \frac{2Q\tilde{y}}{(\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}})\tilde{r}_{\tilde{y}}}\right]\frac{\partial}{\partial\tilde{y}'}\tilde{f} = 0.\tag{B8}$$

The KV equilibrium distribution \tilde{f} satisfying the Vlasov equation can be written as

$$\tilde{f}(\tilde{x}, \tilde{x}', \tilde{y}, \tilde{y}') = \frac{\lambda}{q\pi^2\tilde{\varepsilon}_{\tilde{x}}\tilde{\varepsilon}_{\tilde{y}}}\delta\left[\left(\frac{\tilde{x}}{\tilde{r}_{\tilde{x}}}\right)^2 + \frac{(\tilde{r}_{\tilde{x}}\tilde{x}' - \tilde{r}_{\tilde{x}}'\tilde{x})^2}{\tilde{\varepsilon}_{\tilde{x}}^2} + \left(\frac{\tilde{y}}{\tilde{r}_{\tilde{y}}}\right)^2 + \frac{(\tilde{r}_{\tilde{y}}\tilde{y}' - \tilde{r}_{\tilde{y}}'\tilde{y})^2}{\tilde{\varepsilon}_{\tilde{y}}^2} - 1\right],\tag{B9}$$

where $\delta(x)$ is the Dirac delta-function, $\tilde{\varepsilon}_{\tilde{x}}$ and $\tilde{\varepsilon}_{\tilde{y}}$ are conserved rms emittances of the uniform density beam in the rotating-frame defined by

$$\begin{aligned}\tilde{\varepsilon}_{\tilde{x}} &\equiv 4[\langle\tilde{x}^2\rangle_{\perp}\langle\tilde{x}'^2\rangle_{\perp} - \langle\tilde{x}\tilde{x}'\rangle_{\perp}^2]^{1/2} = \text{const}, \\ \tilde{\varepsilon}_{\tilde{y}} &\equiv 4[\langle\tilde{y}^2\rangle_{\perp}\langle\tilde{y}'^2\rangle_{\perp} - \langle\tilde{y}\tilde{y}'\rangle_{\perp}^2]^{1/2} = \text{const},\end{aligned}\tag{B10}$$

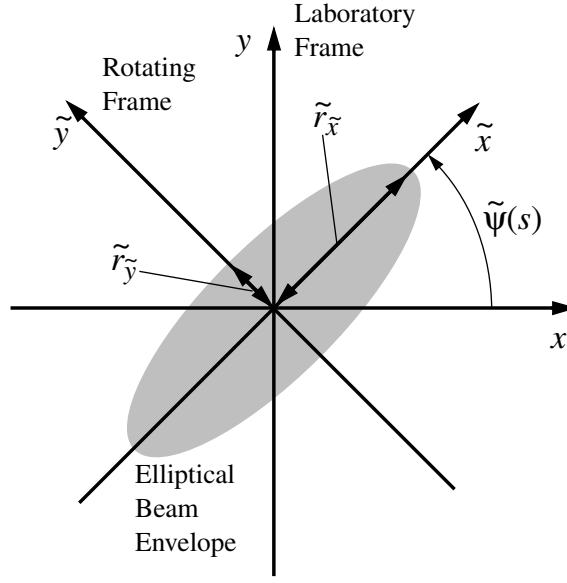


FIG. 23: Solenoidally focused elliptical envelop beam with principal axis radii $\tilde{r}_{\tilde{x}}$ and $\tilde{r}_{\tilde{y}}$ aligned along \tilde{x} and \tilde{y} coordinate axes that are rotated by an angle $\tilde{\psi}(s)$ relative to the laboratory-frame.

and the envelope radii $\tilde{r}_{\tilde{x}} = 2\sqrt{\langle \tilde{x}^2 \rangle_{\perp}}$ and $\tilde{r}_{\tilde{y}} = 2\sqrt{\langle \tilde{y}^2 \rangle_{\perp}}$ obey the envelope equations

$$\begin{aligned} \tilde{r}_{\tilde{x}}'' + k_L^2 \tilde{r}_{\tilde{x}} - \frac{2Q}{\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}}} - \frac{\tilde{\varepsilon}_{\tilde{x}}^2}{\tilde{r}_{\tilde{x}}^3} &= 0, \\ \tilde{r}_{\tilde{y}}'' + k_L^2 \tilde{r}_{\tilde{y}} - \frac{2Q}{\tilde{r}_{\tilde{x}} + \tilde{r}_{\tilde{y}}} - \frac{\tilde{\varepsilon}_{\tilde{y}}^2}{\tilde{r}_{\tilde{y}}^3} &= 0. \end{aligned} \quad (\text{B11})$$

If the $\tilde{}$ s are dropped, Eq. (B9) can also be applied to describe the laboratory-frame KV distribution appropriate for quadrupole or continuous focusing channels that is consistent with $\varepsilon_x = \text{const}$, $\varepsilon_y = \text{const}$, and the envelope equation (4)[1, 3] for the evolution of $r_x = 2\sqrt{\langle x^2 \rangle_{\perp}}$ and $r_y = 2\sqrt{\langle y^2 \rangle_{\perp}}$.

The laboratory-frame envelope equations (4) are identical to the Larmor-frame envelope equations (B11) under the substitutions

$$\begin{aligned} \kappa_x = \kappa_y &\rightarrow k_L^2 = \left(\frac{\omega_c}{2\gamma_b \beta_b c} \right)^2, \\ r_x &\rightarrow \tilde{r}_{\tilde{x}}, \\ r_y &\rightarrow \tilde{r}_{\tilde{y}}, \\ \varepsilon_x &\rightarrow \tilde{\varepsilon}_{\tilde{x}}, \\ \varepsilon_y &\rightarrow \tilde{\varepsilon}_{\tilde{y}}. \end{aligned} \quad (\text{B12})$$

Therefore, we can apply the laboratory-frame envelope equations (4) to analyze the evolution of an elliptical beam envelope in a solenoidally focused transport channel provided we take $\kappa_x = \kappa_y = k_L^2$ and interpret the results as applying in the rotating Larmor-frame defined by Eqs. (B3) and (B5). This correspondence *also* requires that the stationary laboratory-frame x - y coordinate system be chosen to lie along the principal axes of the initial ($s = s_i$) elliptical perturbations with initial values $r_x(s_i) = 2\sqrt{\langle x^2(s_i) \rangle_{\perp}} = \tilde{r}_{\tilde{x}}(s_i)$ and $r_y(s_i) = 2\sqrt{\langle y^2(s_i) \rangle_{\perp}} = \tilde{r}_{\tilde{y}}(s_i)$ and the particle phase advances (i.e., σ_0 , σ_x and σ_y) must also be interpreted as being defined in the rotating Larmor-frame.

Moment calculations verify that the KV distribution (B9) is self-consistent and help elucidate the structure of the rotating equilibrium. The Larmor-frame transformation defined by Eqs. (B3) and (B7) is canonical and phase-space area preserving, with $dx dy = d\tilde{x} d\tilde{y}$ and $dx' dy' = d\tilde{x}' d\tilde{y}'$ and hence the distribution transforms to the lab-frame as

$$\tilde{f}(\tilde{x}, \tilde{x}', \tilde{y}, \tilde{y}') = f(x, x', y, y'). \quad (\text{B13})$$

The rotating-frame density $\tilde{n} = \int d^2 \tilde{x}' \tilde{f}$ is equal to the lab frame density, i.e.,

$$\tilde{n}(\tilde{x}, \tilde{y}) = n(x, y) = \int d^2 x' f \quad (\text{B14})$$

TABLE II: Moments of the KV distributions for an elliptical beam with $P_\theta = 0$ [Eq. (B9)] and an axisymmetric beam with $P_\theta \neq 0$ and $-1 < 2P_\theta/\tilde{\varepsilon} < 1$ [Eq. (B21)]. All second-order moments not listed vanish (i.e., $\int d^2\tilde{x}' \tilde{x}\tilde{y}'\tilde{f} = 0$, $\langle \tilde{x}\tilde{y} \rangle_\perp = 0$) for both distributions.

Moment	KV Distribution	
	Elliptical with $P_\theta = 0$ [Eq. (B9)]	Axisymmetric with $P_\theta \neq 0$ [Eq. (B21)]
$\int d^2\tilde{x}' \tilde{x}'\tilde{f}$	$\tilde{r}'_{\tilde{x}} \frac{\tilde{x}}{\tilde{r}_{\tilde{x}}} \tilde{n}$	$\left(\frac{\tilde{r}'_b}{\tilde{r}_b} \tilde{x} - 2 \frac{P_\theta}{\tilde{r}_b^2} \tilde{y} \right) \tilde{n}$
$\int d^2\tilde{x}' \tilde{y}'\tilde{f}$	$\tilde{r}'_{\tilde{y}} \frac{\tilde{y}}{\tilde{r}_{\tilde{y}}} \tilde{n}$	$\left(\frac{\tilde{r}'_b}{\tilde{r}_b} \tilde{y} + 2 \frac{P_\theta}{\tilde{r}_b^2} \tilde{x} \right) \tilde{n}$
$\int d^2\tilde{x}' \tilde{x}'^2\tilde{f}$	$\left[\frac{\tilde{\varepsilon}_{\tilde{x}}^2}{2\tilde{r}_{\tilde{x}}^2} \left(1 - \frac{\tilde{x}^2}{\tilde{r}_{\tilde{x}}^2} - \frac{\tilde{y}^2}{\tilde{r}_{\tilde{y}}^2} \right) + \tilde{r}'_{\tilde{x}}{}^2 \frac{\tilde{x}^2}{\tilde{r}_{\tilde{x}}^2} \right] \tilde{n}$	$\left[\frac{\tilde{r}'_b{}^2}{\tilde{r}_b^2} \tilde{x}^2 + \frac{4P_\theta}{\tilde{r}_b^3} \left(\frac{P_\theta}{\tilde{r}_b} \tilde{y} - \tilde{r}'_b \right) \tilde{y} + \frac{\tilde{\varepsilon}^2}{2\tilde{r}_b^2} \left(1 - \frac{4P_\theta^2}{\tilde{\varepsilon}^2} \right) \left(1 - \frac{\tilde{x}^2}{\tilde{r}_b^2} - \frac{\tilde{y}^2}{\tilde{r}_b^2} \right) \right] \tilde{n}$
$\int d^2\tilde{x}' \tilde{y}'^2\tilde{f}$	$\left[\frac{\tilde{\varepsilon}_{\tilde{y}}^2}{2\tilde{r}_{\tilde{y}}^2} \left(1 - \frac{\tilde{x}^2}{\tilde{r}_{\tilde{x}}^2} - \frac{\tilde{y}^2}{\tilde{r}_{\tilde{y}}^2} \right) + \tilde{r}'_{\tilde{y}}{}^2 \frac{\tilde{y}^2}{\tilde{r}_{\tilde{y}}^2} \right] \tilde{n}$	$\left[\frac{\tilde{r}'_b{}^2}{\tilde{r}_b^2} \tilde{y}^2 + \frac{4P_\theta}{\tilde{r}_b^3} \left(\frac{P_\theta}{\tilde{r}_b} \tilde{x} + \tilde{r}'_b \right) \tilde{x} + \frac{\tilde{\varepsilon}^2}{2\tilde{r}_b^2} \left(1 - \frac{4P_\theta^2}{\tilde{\varepsilon}^2} \right) \left(1 - \frac{\tilde{x}^2}{\tilde{r}_b^2} - \frac{\tilde{y}^2}{\tilde{r}_b^2} \right) \right] \tilde{n}$
$\int d^2\tilde{x}' \tilde{x}\tilde{x}'\tilde{f}$	$\frac{\tilde{r}'_{\tilde{x}}}{\tilde{r}_{\tilde{x}}} \tilde{x}^2 \tilde{n}$	$\left(\frac{\tilde{r}'_b}{\tilde{r}_b} \tilde{x} - \frac{2P_\theta}{\tilde{r}_b^2} \tilde{y} \right) \tilde{x} \tilde{n}$
$\int d^2\tilde{x}' \tilde{y}\tilde{y}'\tilde{f}$	$\frac{\tilde{r}'_{\tilde{y}}}{\tilde{r}_{\tilde{y}}} \tilde{y}^2 \tilde{n}$	$\left(\frac{\tilde{r}'_b}{\tilde{r}_b} \tilde{y} + \frac{2P_\theta}{\tilde{r}_b^2} \tilde{x} \right) \tilde{y} \tilde{n}$
$\int d^2\tilde{x}' (\tilde{x}\tilde{y}' - \tilde{y}\tilde{x}')\tilde{f}$	0	$\frac{2P_\theta}{\tilde{r}_b^2} (\tilde{x}^2 + \tilde{y}^2) \tilde{n}$
$\langle \tilde{x}^2 \rangle_\perp$	$\frac{\tilde{r}_{\tilde{x}}^2}{4}$	$\frac{\tilde{r}_b^2}{4}$
$\langle \tilde{y}^2 \rangle_\perp$	$\frac{\tilde{r}_{\tilde{y}}^2}{4}$	$\frac{\tilde{r}_b^2}{4}$
$\langle \tilde{x}'^2 \rangle_\perp$	$\frac{\tilde{r}_{\tilde{x}}^2}{4} + \frac{\tilde{\varepsilon}_{\tilde{x}}^2}{4\tilde{r}_{\tilde{x}}^2}$	$\frac{\tilde{r}_b'^2}{4} + \frac{\tilde{\varepsilon}^2}{4\tilde{r}_b^2}$
$\langle \tilde{y}'^2 \rangle_\perp$	$\frac{\tilde{r}_{\tilde{y}}^2}{4} + \frac{\tilde{\varepsilon}_{\tilde{y}}^2}{4\tilde{r}_{\tilde{y}}^2}$	$\frac{\tilde{r}_b'^2}{4} + \frac{\tilde{\varepsilon}^2}{4\tilde{r}_b^2}$
$\langle \tilde{x}\tilde{x}' \rangle_\perp$	$\frac{\tilde{r}_{\tilde{x}} \tilde{r}'_{\tilde{x}}}{4}$	$\frac{\tilde{r}_b \tilde{r}'_b}{4}$
$\langle \tilde{y}\tilde{y}' \rangle_\perp$	$\frac{\tilde{r}_{\tilde{y}} \tilde{r}'_{\tilde{y}}}{4}$	$\frac{\tilde{r}_b \tilde{r}'_b}{4}$
$\langle \tilde{x}\tilde{y}' - \tilde{y}\tilde{x}' \rangle_\perp$	0	P_θ
$16[\langle \tilde{x}^2 \rangle_\perp \langle \tilde{x}'^2 \rangle_\perp - \langle \tilde{x}\tilde{x}' \rangle_\perp^2]$	$\tilde{\varepsilon}_{\tilde{x}}^2$	$\tilde{\varepsilon}^2$
$16[\langle \tilde{y}^2 \rangle_\perp \langle \tilde{y}'^2 \rangle_\perp - \langle \tilde{y}\tilde{y}' \rangle_\perp^2]$	$\tilde{\varepsilon}_{\tilde{y}}^2$	$\tilde{\varepsilon}^2$

and can be calculated as

$$\tilde{n} = \int d^2\tilde{x}' \tilde{f} = \begin{cases} \frac{\lambda}{\pi \tilde{r}_{\tilde{x}} \tilde{r}_{\tilde{y}}}, & \text{if } (\tilde{x}/\tilde{r}_{\tilde{x}})^2 + (\tilde{y}/\tilde{r}_{\tilde{y}})^2 < 1, \\ 0, & \text{otherwise.} \end{cases} \quad (\text{B15})$$

verifying consistency. Laboratory-frame statistical averages are simply expressed in terms of rotating-frame distribution as

$$\langle \cdots \rangle_\perp = \frac{\int d^2\tilde{x} \int d^2\tilde{x}' \cdots \tilde{f}}{\int d^2\tilde{x} \int d^2\tilde{x}' \tilde{f}}. \quad (\text{B16})$$

Various moments of the Larmor-frame KV distribution (B9) are summarized in Table II. The moments in Table II can also be applied to the laboratory-frame KV distribution for quadrupole and continuous focusing channels by simply dropping all \tilde{s} . It should be stressed that the rotating-frame emittances $\tilde{\varepsilon}_{\tilde{x}}$ and $\tilde{\varepsilon}_{\tilde{y}}$ are *not*, in general, equal to the laboratory-frame emittances ε_x and ε_y , which evolve in s for an elliptical KV beam in a solenoidal focusing channel. Laboratory-frame projections of the moments are straightforward to calculate from the transformations (B3) and (B7).

The angular momentum of the KV distribution (B9) is important in understanding the structure of the equilibrium. The vector potential of the axial magnetic field can be expressed as $\mathbf{A} = (B_z/2)(y\hat{\mathbf{x}} - x\hat{\mathbf{y}})$, and canonical momenta conjugate to the coordinates $Q_x = x$ and $Q_y = y$ are $P_x = x' - k_L y$ and $P_y = y' + k_L x$. Therefore, the single-particle canonical angular momentum $p_\theta \equiv \mathbf{Q} \times \mathbf{P} \cdot \hat{\mathbf{z}}$ can be expressed as

$$\begin{aligned} p_\theta &= xy' - yx' + k_L(x^2 + y^2) \\ &= \tilde{x}\tilde{y}' - \tilde{y}\tilde{x}'. \end{aligned} \quad (\text{B17})$$

For any distribution of particles, it follows from the equations of motion (B1) that the system canonical angular

momentum

$$P_\theta \equiv \langle p_\theta \rangle_\perp = \langle xy' - yx' \rangle_\perp + k_L \langle x^2 + y^2 \rangle_\perp \quad (\text{B18})$$

satisfies

$$\frac{d}{ds} P_\theta = (\kappa_x - \kappa_y) \langle xy \rangle_\perp - \frac{q}{m\gamma_b^3 \beta_b^2 c^2} \left\langle x \frac{\partial \phi}{\partial y} - y \frac{\partial \phi}{\partial x} \right\rangle_\perp. \quad (\text{B19})$$

For a solenoidal focused beam, $\kappa_x = \kappa_y = 0$ and the first moment term in Eq. (B19) vanishes. Using Green's functions for the Poisson equation $\nabla^2 \phi_\perp = -qn/\epsilon_0$, it can be shown that the second moment term in Eq. (B19) also vanishes provided any conducting boundaries are azimuthally invariant ($\partial/\partial\theta = 0$). Thus, in a solenoidal channel, $P_\theta = \text{const}$ for any distribution function focused within an axisymmetric beam pipe. For the specific KV distribution in Eq. (B9), we calculate

$$P_\theta \equiv \langle p_\theta \rangle_\perp = \langle \tilde{x}\tilde{y}' - \tilde{y}\tilde{x}' \rangle_\perp = 0. \quad (\text{B20})$$

This zero value of P_θ is appropriate for a beam launched from a field-free source (i.e., $B_z = 0$ at the source location), and results in maximum focusability for given Larmor-frame emittances $\tilde{\epsilon}_{\tilde{x}}$ and $\tilde{\epsilon}_{\tilde{y}}$. Beams injected from a source immersed in a finite axial magnetic field B_z have nonzero P_θ and higher effective emittances[30, 31]. Also, for a KV equilibrium evolving in an alternating gradient focusing channel, Eq. (B9) can be applied in the laboratory frame (drop all $\tilde{}$ s) to show that $P_\theta = \langle xy' - yx' \rangle_\perp = 0$ in this case too. Elliptical KV distributions analogous to Eq. (B9) can also be constructed for nonzero values of $P_\theta = \text{const}$ for both solenoidally focused beams in the Larmor-frame and quadrupole focused (possibly with skew-couplings) beams in the laboratory-frame. However, these distributions will result in envelope equations that differ in form from Eq. (4) and have more complicated invariant emittances explored by Dragt, Neri, and Rangarajan[32] and Barnard (see Ref. [33]) because the elliptical beam axes rotate within the Larmor-frame. Coupled moment formulations have been employed to analyze the special case of elliptical envelope perturbations about a round-beam equilibrium for a continuously focused beam with $P_\theta \neq 0$ [34]. In the present paper, we explore only cases of envelope evolution that we can readily map to Eq. (4) while concretely connecting the model to physically relevant focusing systems and quantities. Elliptical beams with $P_\theta \neq 0$ in solenoidal or alternating gradient quadrupole focusing channels[35] are beyond the scope of the present analysis. For the special case of a *round* beam envelope (i.e., $\tilde{r}_{\tilde{x}} = \tilde{r}_{\tilde{y}} \equiv \tilde{r}_b$) with $P_\theta \neq 0$ in a solenoidal focusing channel, the envelope equations can also be mapped to the form of Eq. (B11) with a KV distribution previously analyzed by Chen, Pakter, and Davidson[36]. (In Ref. [36] the authors do not refer to the distribution analyzed as being KV, but it is appropriate to label any distribution as being of KV form if it is a delta-function of a Courant-Snyder invariant that is expressible as a quadratic form in canonically transformed phase-space variables and has a uniform density projection. An infinity of KV distributions can be constructed through linear canonical transformations of the quadratic standard form of the KV distribution[29].) For this special axisymmetric case the self-consistent KV distribution satisfying the Vlasov equation can be expressed as

$$\begin{aligned} \tilde{f}(\tilde{x}, \tilde{x}', \tilde{y}, \tilde{y}') = \frac{\lambda}{q\pi^2 \tilde{\epsilon}^2} \delta \left[\left(\frac{\tilde{x}}{\tilde{r}_b} \right)^2 + \left(\frac{\tilde{r}_b \tilde{x}' - \tilde{r}_b' \tilde{x}}{\tilde{\epsilon}} \right)^2 + \left(\frac{\tilde{y}}{\tilde{r}_b} \right)^2 \right. \\ \left. + \left(\frac{\tilde{r}_b \tilde{y}' - \tilde{r}_b' \tilde{y}}{\tilde{\epsilon}} \right)^2 - \frac{4P_\theta}{\tilde{\epsilon}^2} (\tilde{x}\tilde{y}' - \tilde{y}\tilde{x}') - \left(1 - \frac{4P_\theta^2}{\tilde{\epsilon}^2} \right) \right] \end{aligned} \quad (\text{B21})$$

and the corresponding emittances and envelope equation are given by Eqs. (B10) and (B11) with $\tilde{\epsilon}_{\tilde{x}} = \tilde{\epsilon}_{\tilde{y}} \equiv \tilde{\epsilon}$ and $\tilde{r}_{\tilde{x}} = \tilde{r}_{\tilde{y}} = \tilde{r}_b$. The self-consistent density can be calculated from Eq. (B21) for $-1 < 2P_\theta/\tilde{\epsilon} < 1$ (corresponding to sufficiently small angular momentum to be focusable) as

$$\tilde{n} = \int d^2 \tilde{x}' \tilde{f} = \begin{cases} \frac{\lambda}{\pi \tilde{r}_b^2}, & \text{if } (\tilde{x}/\tilde{r}_b)^2 + (\tilde{y}/\tilde{r}_b)^2 < 1, \\ 0, & \text{otherwise,} \end{cases} \quad (\text{B22})$$

and additional moments are summarized in Table II for $-1 < 2P_\theta/\tilde{\epsilon} < 1$. Note that the nonzero P_θ term results in directed azimuthal flow contributions to various moments. For an axisymmetric beam, it is instructive to employ Eqs. (B3) and (B7) to express the constant Larmor-frame emittance $\tilde{\epsilon}$ in terms of laboratory-frame moments. This gives

$$\tilde{\epsilon}^2 = \epsilon_x^2 - 4\langle r^2 \theta' \rangle_\perp + 4P_\theta^2 = \text{const}, \quad (\text{B23})$$

where $\varepsilon_x = \varepsilon_y$ is the ordinary laboratory-frame emittance given by Eq. (5) and $r = \sqrt{x^2 + y^2}$ and $\theta = \tan^{-1}(y, x)$ are the usual cylindrical particle coordinates in the laboratory-frame. Because $P_\theta = \text{const}$, it follows from Eq. (B23) that

$$\varepsilon_r \equiv \sqrt{\varepsilon_x^2 - 4\langle r^2 \theta' \rangle_\perp} \quad (\text{B24})$$

can be interpreted as a conserved radial emittance for an axisymmetric beam. In summary, round beam envelopes with $r_x = r_y$ and $P_\theta \neq 0$ can also be analyzed with the envelope equations (4) provided we interpret the results in the rotating Larmor-frame and substitute

$$\begin{aligned} \kappa_x &= \kappa_y \rightarrow k_L^2, \\ r_x &= r_y \rightarrow \tilde{r}_b, \\ \varepsilon_x &= \varepsilon_y \rightarrow \tilde{\varepsilon} = \end{aligned} \quad (\text{B25})$$

in Eq. (4). In this axisymmetric case, the initial phase of orientation of the stationary laboratory-frame is arbitrary. Various authors have derived equivalent axisymmetric beam envelope equations valid for finite P_θ including: Lee and Cooper[31], Miller[30], and Chen, Pakter and Davidson[36].

APPENDIX C: DERIVATION OF EQUATION (18)

The free-drift differential equation $r_+'' = Q/r_+$ [Eq. (17)] can be integrated to give

$$C_1 = \frac{r_+'^2}{2} - Q \ln r_+, \quad (\text{C1})$$

where $C_1 = \text{const}$ is the scaled envelope Hamiltonian. We temporarily assume that $r_+' \geq 0$. Then $r_+' = \sqrt{2Q \ln r_+ + 2C_1}$, and integrating once again we have

$$s = e^{-C_1} \sqrt{\pi} \operatorname{erfi} \left[\sqrt{\ln \left(\frac{r_+}{\sqrt{2Q}} \right) + C_1} \right] - C_2, \quad (\text{C2})$$

where $C_2 = \text{const}$ and $\operatorname{erfi}(z) = \operatorname{erf}(iz)/i = (2/\sqrt{\pi}) \int_0^z dt \exp(t^2)$ is the imaginary error function. Eliminating C_1 and C_2 in terms of the initial conditions $r_+ = r_+(s_i)$ and $R_+' = R_+'(s_i)$ at $s = s_i$ yields

$$\ln \left[\frac{r_+(s)}{r_+(s_i)} \right] = -\frac{r_+'^2(s_i)}{2Q} + \left[\operatorname{erfi}^{-1} \left\{ \operatorname{erfi} \left[\frac{r_+'(s_i)}{\sqrt{2Q}} \right] + \sqrt{\frac{2Q}{\pi}} e^{\frac{r_+'^2(s_i)}{2Q}} \frac{(s - s_i)}{r_+(s_i)} \right\} \right]^2. \quad (\text{C3})$$

Because $r_+'' = Q/r_+$, r_+ is an analytic function. Therefore, even though Eq. (C3) was derived under assumption that $r_+' \geq 0$, Eq. (C3) is also valid for $r_+' < 0$. Solving Eq. (C3) for $r_+(s)$ yields the free-drift solution given in Eq. (18).

APPENDIX D: PHASE ADVANCE OF ENVELOPE MODES IN THE ZERO SPACE-CHARGE LIMIT

In the limit of zero space-charge ($Q = 0$), the equations of motion [see Eq. (1)] for the particle x - and y -orbits are decoupled and of the same form. Likewise, the resulting x - and y -envelope equations [see Eq. (4)] are decoupled and of the same form. Therefore, we analyze only the x -equation here. The x equation of motion of the particle is given by

$$x'' + \kappa_x x = 0. \quad (\text{D1})$$

Here, $\kappa_x(s + L_p) = \kappa_x(s)$ describes the linear applied focusing function of a lattice with periodicity L_p that is of otherwise unspecified form. To define the phase advance of the x -orbit, without loss in generality, we express the orbit in phase-amplitude form as[12, 13]

$$x(s) = A_x w_x(s) \cos[\psi_x(s)]. \quad (\text{D2})$$

Here, $A_x = \text{const}$, $\psi_x'(s) = 1/w_x^2(s)$, and $w_x(s)$ is the positive solution to the equation

$$w_x'' + \kappa_x w_x - \frac{1}{w_x^3} = 0 \quad (\text{D3})$$

satisfying the periodicity requirement $w_x(s+L_p) = w_x(s)$. This equation is recognized as the scaled envelope equation with zero space-charge [see Eq. (4)] and therefore the matched beam envelope r_{xm} is related to the amplitude function w_x as

$$r_{xm} = \sqrt{\epsilon_x} w_x. \quad (\text{D4})$$

Consistent with Eqs. (24) and (26), the single-particle phase advance σ_{0x} of oscillations in x over one lattice period is

$$\sigma_{0x} = \psi_x(s_i + L_p) - \psi_x(s_i) = \int_{s_i}^{s_i + L_p} \frac{ds}{w_x^2}, \quad (\text{D5})$$

independent of the initial axial coordinate s_i .

Consistent with the x -particle equation of motion (D1), the beam envelope equation for $r_x = 2\sqrt{\langle x^2 \rangle_\perp}$ is

$$r_x'' + \kappa_x r_x - \frac{\epsilon_x^2}{r_x^3} = 0. \quad (\text{D6})$$

We expand r_x as $r_x = r_{xm} + \delta r_x$ where $r_{xm} = \sqrt{\epsilon_x} w_x$ is the matched beam radius, and δr_x is a small-amplitude perturbation about the matched beam. Then δr_x satisfies the linearized envelope equation [see also Eq. (37)]

$$\delta r_x'' + \kappa_x \delta r_x + 3 \frac{\epsilon_x^2}{r_{xm}^4} \delta r_x = 0. \quad (\text{D7})$$

Paralleling the analysis above for the particle orbits, the solution to the linearized envelope equation can be expressed in phase-amplitude form as

$$\delta r_x(s) = A_e w_e(s) \cos[\psi_e(s)]. \quad (\text{D8})$$

Here, $A_e = \text{const}$, $\psi_e'(s) = 1/w_e^2(s)$, and $w_e(s)$ the positive solution to

$$w_e'' + \kappa_x w_e + \frac{3}{w_x^4} w_e - \frac{1}{w_e^3} = 0 \quad (\text{D9})$$

satisfying the periodicity requirement $w_e(s+L_p) = w_e(s)$. The phase advance σ_{ex} of oscillations in δr_x over one lattice period is given by

$$\sigma_{ex} = \psi_e(s_i + L_p) - \psi_e(s_i) = \int_{s_i}^{s_i + L_p} \frac{ds}{w_e^2}. \quad (\text{D10})$$

Comparison of Eqs. (D3) and (D9) shows that the solution for w_e is connected to w_x as

$$w_e = \frac{w_x}{\sqrt{2}}. \quad (\text{D11})$$

Thus, from Eqs. (D5) and (D10), the phase advances of the single-particle x -orbit and the envelope δr_x are related as

$$\sigma_{ex} = 2\sigma_{0x}. \quad (\text{D12})$$

Equation (D12) proves that in the limit of zero space-charge that the phase advance of oscillations in δr_x are two times the phase advance of undepressed particle oscillations in x . An analogous result to Eq. (D12) holds in the y -plane. Equation (D12) is straightforward to generalize to show that for zero space-charge and arbitrary, non-periodic lattices with general $\kappa_x(s)$ that the rate of phase accumulation of a small-amplitude envelope perturbation about a non-periodic reference envelope evolution is twice the rate of phase accumulation of the single-particle orbit.

APPENDIX E: ENVELOPE MODE COURANT-SNYDER INVARIANTS

For continuous focusing or solenoidal transport channels with $\kappa_x = \kappa_y \equiv \kappa$, undriven envelope perturbations $\delta r_\pm = (r_x \pm r_y)/2$ satisfy the uncoupled equations [see Eq. (45)]

$$\begin{aligned} \delta r_+'' + \kappa \delta r_+ + \frac{2Q}{r_m^2} \delta r_+ + \frac{3\epsilon^2}{r_m^4} \delta r_+ &= 0, \\ \delta r_-'' + \kappa \delta r_- + \frac{3\epsilon^2}{r_m^4} \delta r_- &= 0. \end{aligned} \quad (\text{E1})$$

Here, $\kappa(s + L_p) = \kappa(s)$ describes the linear applied focusing forces of the lattice with periodicity L_p and is otherwise unspecified ($\kappa = k_{\beta 0}^2 = \text{const}$ for continuous focusing). As in standard treatments of single-particle orbits[12, 13], without loss in generality, we express the envelope perturbations in phase-amplitude form as

$$\delta r_{\pm} = A_{\pm} w_{\pm}(s) \cos[\psi_{\pm}(s)]. \quad (\text{E2})$$

Here, $A_{\pm} = \text{const}$, $\psi'_{\pm} = 1/w_{\pm}^2$, and w_{\pm} are positive solutions to the equations

$$\begin{aligned} w_+'' + \kappa w_+ + \frac{2Q}{r_m^2} w_+ + \frac{3\varepsilon^2}{r_m^4} w_+ - \frac{1}{w_+^3} &= 0, \\ w_-'' + \kappa w_- + \frac{3\varepsilon^2}{r_m^4} w_- - \frac{1}{w_-^3} &= 0 \end{aligned} \quad (\text{E3})$$

satisfying the periodicity requirements $w_{\pm}(s + L_p) = w_{\pm}(s)$. Employing scaling procedures analogous to those presented in Sec. II E, it can be shown that the envelope amplitude functions w_{\pm} can be regarded as being parameterized by L_p , σ_0 , σ/σ_0 , and parameters that describe the shape of the lattice focusing function $\kappa(s)$. In contrast to the usual single-particle amplitude functions of undepressed particle orbits[12, 13], w_{\pm} will depend on matched beam space-charge depression parameter σ/σ_0 in addition to the lattice parameters σ_0 , L_p , etc. The phase advance σ_{\pm} of oscillations in δr_{\pm} over one lattice period is given by

$$\sigma_{\pm} = \psi_{\pm}(s_i + L_p) - \psi_{\pm}(s_i) = \int_{s_i}^{s_i + L_p} \frac{ds}{w_{\pm}^2}, \quad (\text{E4})$$

independent of the initial coordinate axial s_i . Differentiating Eq. (E2) and employing $\psi'_{\pm} = 1/w_{\pm}^2$ to simplify the result gives

$$\begin{aligned} \frac{\delta r_{\pm}}{w_{\pm}} &= A_{\pm} \cos \psi_{\pm}, \\ w'_{\pm} \delta r_{\pm} - w_{\pm} \delta r'_{\pm} &= A_{\pm} \sin \psi_{\pm}. \end{aligned} \quad (\text{E5})$$

Squaring and adding these equations, we obtain quadratic Courant-Snyder invariants in δr_{\pm} - $\delta r'_{\pm}$ given by

$$\left(\frac{\delta r_{\pm}}{w_{\pm}} \right)^2 + (w'_{\pm} \delta r_{\pm} - w_{\pm} \delta r'_{\pm})^2 = A_{\pm}^2 = \text{const}. \quad (\text{E6})$$

These invariants of the envelope perturbations are equations of ellipses in δr_{\pm} - $\delta r'_{\pm}$ phase-space where the axes of the ellipses do not, in general, align with the δr_{\pm} and $\delta r'_{\pm}$ axes. They can be interpreted as area measures because as the perturbations evolve the set of all initial conditions satisfying Eq. (E6) (corresponding to all pure modes with the same oscillation amplitude) will trace out an ellipse in δr_{\pm} - $\delta r'_{\pm}$ phase-space with area $\pi A_{\pm} = \text{const}$. Analysis of the evolution of this constant area ellipse (in terms of elongation and rotation) can be facilitated by introducing Twiss parameters as in standard treatments of uncoupled single-particle dynamics[13]. It is straightforward to show that Courant-Snyder invariants directly analogous to those in Eq. (E6) apply to non-periodic lattices with general $\kappa(s)$ for any small-amplitude envelope perturbations about a reference envelope evolution that need not be matched. In this non-periodic case, w_{\pm} satisfies Eq. (E3) for a general reference envelope solution r_m and w_{\pm} need not be periodic.

Unfortunately, the analysis of Courant-Snyder invariants for the more general case of undriven coupled envelope modes evolving according to [see Eq. (37)]

$$\delta r_j'' + \kappa_j \delta r_j + \frac{2Q}{(r_{xm} + r_{ym})^2} (\delta r_x + \delta r_y) + \frac{3\varepsilon_j^2}{r_{jm}^4} \delta r_j = 0 \quad (\text{E7})$$

with $j = x, y$, and $\kappa_x \neq \kappa_y$ is considerably more complicated than in the continuous or solenoidal focusing case above. This complication arises because when $\kappa_x \neq \kappa_y$ the normal coordinates of the coupled modes are not simply expressible. In the previous case, the decoupled sum and difference coordinates $\delta r_{\pm} = (r_x \pm r_y)/2$ provided simple expressions of the normal coordinates. For $\kappa_x \neq \kappa_y$, the normal coordinates are expressible in terms of the s -varying eigenvectors of the transfer map in Eq. (47). Fortunately, Edwards and Teng[37] have presented a general formulation for analysis of two-dimensional coupled linear motion that can be directly applied to coupled envelope modes. To make a connection to this work, the equations of motion (E7) of the envelope perturbations can be expressed in

Hamiltonian form as

$$\begin{aligned}\frac{d}{ds}\delta r_j &= \frac{\partial H}{\partial \delta r'_j}, \\ \frac{d}{ds}\delta r'_j &= -\frac{\partial H}{\partial \delta r_j},\end{aligned}\tag{E8}$$

where

$$H = \frac{1}{2}(\delta r_x'^2 + \delta r_y'^2) + \frac{1}{2}\kappa_x\delta r_x^2 + \frac{1}{2}\kappa_y\delta r_y^2 + \frac{Q}{(r_{xm} + r_{ym})^2}(\delta r_x + \delta r_y)^2 + \frac{3}{2}\frac{\varepsilon_x^2}{r_{xm}^4}\delta r_x^2 + \frac{3}{2}\frac{\varepsilon_y^2}{r_{ym}^4}\delta r_y^2\tag{E9}$$

is the envelope Hamiltonian. From this Hamiltonian formulation, the correspondence of variables and coefficients employed by Edwards and Teng to those used here are readily identified. The conjugate variables x , p_x and y , p_y of Edwards and Teng are replaced by

$$\begin{aligned}x &\rightarrow \delta r_x, \\ p_x &\rightarrow \delta r'_x, \\ y &\rightarrow \delta r_y, \\ p_y &\rightarrow \delta r'_y,\end{aligned}\tag{E10}$$

and the coefficients L , F , G , and K are identified as

$$\begin{aligned}L &= 0, \\ F &= \kappa_x + \frac{2Q}{(r_{xm} + r_{ym})^2}, \\ G &= \kappa_y + \frac{2Q}{(r_{xm} + r_{ym})^2}, \\ K &= \frac{2Q}{(r_{xm} + r_{ym})^2}.\end{aligned}\tag{E11}$$

The quadratic invariants calculated by Edwards and Teng can then be directly applied and are generalized Courant-Snyder invariants of the coupled envelope modes. Application and interpretation of these coupled motion invariants are considerably more complicated than in the case presented above for solenoidal and continuous focusing. However, the structure and consequences of the generalized invariants are loosely analogous to the uncoupled motion Courant-Snyder invariants.

APPENDIX F: MATRIX ANALYSIS OF CONTINUOUS FOCUSING NORMAL ENVELOPE MODES

For continuous focusing, the matrix form of the equation of motion of undriven envelope perturbations $\delta\mathbf{R} = (\delta r_x, \delta r'_x, \delta r_y, \delta r'_y)$ is given by $d\delta\mathbf{R}/ds + \mathbf{K} \cdot \delta\mathbf{R} = 0$ [Eq. (38) with $\delta\mathbf{P} = 0$] with a constant coupling matrix \mathbf{K} given by Eq. (40). The equilibrium constraint equation (61) can be used to evaluate \mathbf{K} as

$$\mathbf{K} = \begin{bmatrix} 0 & -1 & 0 & 0 \\ \frac{\sigma_+^2 + \sigma_-^2}{2L_p^2} & 0 & \frac{\sigma_+^2 - \sigma_-^2}{2L_p^2} & 0 \\ 0 & 0 & 0 & -1 \\ \frac{\sigma_+^2 - \sigma_-^2}{2L_p^2} & 0 & \frac{\sigma_+^2 + \sigma_-^2}{2L_p^2} & 0 \end{bmatrix}.\tag{F1}$$

Here we have expressed the elements of \mathbf{K} in terms of the phase advances of the breathing and quadrupole modes $\sigma_+ = \sqrt{2\sigma_0^2 + 2\sigma^2}$ and $\sigma_- = \sqrt{\sigma_0^2 + 3\sigma^2}$ as defined in Eq. (64). The equation of motion for $\delta\mathbf{R}$ is trivially integrated from an initial condition $\delta\mathbf{R}(s_i)$ at axial coordinate $s = s_i$ as

$$\delta\mathbf{R}(s) = \mathbf{M}_e(s|s_i)\delta\mathbf{R}(s_i),\tag{F2}$$

where

$$\mathbf{M}_e(s|s_i) = e^{-\mathbf{K}(s-s_i)}\tag{F3}$$

is the transfer matrix of the envelope perturbations. This solution is equivalent to the one presented in Eq. (65).

Any linear transform of the envelope coordinates $\delta\mathbf{R}$ can be expressed as

$$\delta\tilde{\mathbf{R}} = \mathbf{T} \cdot \delta\mathbf{R}, \quad (\text{F4})$$

where $\mathbf{T} = \text{const}$ is some invertible 4×4 matrix and $\delta\tilde{\mathbf{R}}$ is the transformed (tilde variables) envelope coordinate vector. The equation of motion in transformed coordinates becomes

$$\frac{d}{ds}\delta\tilde{\mathbf{R}} + \tilde{\mathbf{K}} \cdot \delta\tilde{\mathbf{R}} = 0, \quad (\text{F5})$$

where

$$\tilde{\mathbf{K}} = \mathbf{T} \cdot \mathbf{K} \cdot \mathbf{T}^{-1}. \quad (\text{F6})$$

The solution to Eq. (F5) is given by

$$\delta\tilde{\mathbf{R}}(s) = \tilde{\mathbf{M}}_e(s|s_i)\delta\tilde{\mathbf{R}}(s_i) \quad (\text{F7})$$

where the transformed transfer map

$$\tilde{\mathbf{M}}_e(s|s_i) = e^{-\tilde{\mathbf{K}}(s-s_i)} \quad (\text{F8})$$

is related to the untransformed map $\mathbf{M}_e(s|s_i)$ by

$$\tilde{\mathbf{M}}_e(s|s_i) = \mathbf{T} \cdot \mathbf{M}_e(s|s_i) \cdot \mathbf{T}^{-1}. \quad (\text{F9})$$

The matrix $\mathbf{M}_e(s_i + L_p|s_i)$ has four eigenvalues λ_n with $n = 1, 2, 3$, and 4 defined by $\mathbf{M}_e(s_i + L_p|s_i) \cdot \mathbf{E}_n = \lambda_n \mathbf{E}_n$ [see Eq. (47)]. Transforming this equation gives $\tilde{\mathbf{M}}_e(s_i + L_p|s_i) \cdot \tilde{\mathbf{E}}_n = \lambda_n \tilde{\mathbf{E}}_n$, where $\tilde{\mathbf{E}}_n = \mathbf{T} \cdot \mathbf{E}_n$, thereby showing that the eigenvalues of \mathbf{M}_e are invariant under the transform \mathbf{T} . Similarly, the four eigenvalues of the matrix \mathbf{K} are equal to the eigenvalues of the transformed matrix $\tilde{\mathbf{K}} = \mathbf{T} \cdot \mathbf{K} \cdot \mathbf{T}^{-1}$. Consider a transform \mathbf{T} to fully decoupled coordinates $\delta\tilde{\mathbf{R}}$ where $\tilde{\mathbf{M}}_e(s|s_i)$ is diagonal. Then from Eq. (F8) $\tilde{\mathbf{K}}$ is also diagonal. In this representation, the diagonal elements of both $\tilde{\mathbf{M}}_e(s_i + L_p|s_i)$ and $\tilde{\mathbf{K}}$ are their respective eigenvalues. The eigenvalues of \mathbf{K} can be calculated using Eq. (F1) as $\pm i\sigma_+/L_p$ and $\pm i\sigma_-/L_p$. Therefore,

$$\tilde{\mathbf{K}} = \mathbf{T} \cdot \mathbf{K} \cdot \mathbf{T}^{-1} = \begin{bmatrix} -i\sigma_+ & 0 & 0 & 0 \\ 0 & i\sigma_+ & 0 & 0 \\ 0 & 0 & -i\sigma_- & 0 \\ 0 & 0 & 0 & i\sigma_- \end{bmatrix},$$

and Eq. (F8) gives

$$\tilde{\mathbf{M}}_e(s|s_i) = \begin{bmatrix} \exp(i\sigma_+ \frac{s-s_i}{L_p}) & 0 & 0 & 0 \\ 0 & \exp(-i\sigma_+ \frac{s-s_i}{L_p}) & 0 & 0 \\ 0 & 0 & \exp(i\sigma_- \frac{s-s_i}{L_p}) & 0 \\ 0 & 0 & 0 & \exp(-i\sigma_- \frac{s-s_i}{L_p}) \end{bmatrix}. \quad (\text{F10})$$

Form Eq. (F10) the eigenvalues of $\mathbf{M}_e(s_i + L_p|s_i)$ are identified as $\lambda_n = e^{\pm i\sigma_+}$, $e^{\pm i\sigma_-}$. To complete the analysis, the fully decoupled solution for $\delta\tilde{\mathbf{R}}(s)$ given by Eqs. (F7) and Eq. (F10) is connected to the untransformed coordinates $\delta\mathbf{R} = (\delta r_x, \delta r'_x, \delta r_y, \delta r'_y)$ by $\delta\tilde{\mathbf{R}} = \mathbf{T} \cdot \delta\mathbf{R}$ through the transformation

$$\mathbf{T} = \frac{1}{2} \begin{bmatrix} -i\frac{\sigma_+}{L_p} & -1 & -i\frac{\sigma_+}{L_p} & -1 \\ -i\frac{\sigma_+}{L_p} & 1 & -i\frac{\sigma_+}{L_p} & 1 \\ -i\frac{\sigma_-}{L_p} & -1 & i\frac{\sigma_-}{L_p} & 1 \\ -i\frac{\sigma_-}{L_p} & 1 & i\frac{\sigma_-}{L_p} & -1 \end{bmatrix}, \quad (\text{F11})$$

$$\mathbf{T}^{-1} = \frac{1}{2} \begin{bmatrix} i\frac{L_p}{\sigma_+} & i\frac{L_p}{\sigma_+} & i\frac{L_p}{\sigma_-} & i\frac{L_p}{\sigma_-} \\ -1 & 1 & -1 & 1 \\ i\frac{L_p}{\sigma_+} & i\frac{L_p}{\sigma_+} & -i\frac{L_p}{\sigma_-} & -i\frac{L_p}{\sigma_-} \\ -1 & 1 & 1 & -1 \end{bmatrix}.$$

It is instructive to examine the connection of this matrix transformation approach to the decoupled sum and difference coordinates $\delta r_{\pm} = (\delta r_x \pm \delta r_y)/2$ employed in Sec. III. Taking $\delta \mathbf{R} = (\delta r_+, \delta r'_+, \delta r_-, \delta r'_-) = \mathbf{T} \cdot \delta \mathbf{R}$ corresponds to the linear transformation

$$\mathbf{T} = \frac{1}{2} \mathbf{T}^{-1} = \frac{1}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 1 & 0 & 1 \\ 1 & 0 & -1 & 0 \\ 0 & 1 & 0 & -1 \end{bmatrix}. \quad (\text{F12})$$

Under this transformation, $\tilde{\mathbf{K}}$ is block diagonal with

$$\tilde{\mathbf{K}} = \mathbf{T} \cdot \mathbf{K} \cdot \mathbf{T}^{-1} = \begin{bmatrix} 0 & -1 & 0 & 0 \\ \frac{\sigma_+^2}{L_p^2} & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 1 & \frac{\sigma_-^2}{L_p^2} & 0 \end{bmatrix}.$$

The corresponding transfer map $\tilde{\mathbf{M}}_e(s|s_i) = \exp[-\tilde{\mathbf{K}}(s - s_i)]$ can be directly calculated using the series definitions of the matrix exponential, recognizing the recursion among terms, and summing resulting series to give

$$\tilde{\mathbf{M}}_e(s|s_i) = \begin{bmatrix} \cos(\sigma_+ \frac{s-s_i}{L_p}) & \frac{L_p}{\sigma_+} \sin(\sigma_+ \frac{s-s_i}{L_p}) & 0 & 0 \\ -\frac{\sigma_+}{L_p} \sin(\sigma_+ \frac{s-s_i}{L_p}) & \cos(\sigma_+ \frac{s-s_i}{L_p}) & 0 & 0 \\ 0 & 0 & \cos(\sigma_- \frac{s-s_i}{L_p}) & \frac{L_p}{\sigma_-} \sin(\sigma_- \frac{s-s_i}{L_p}) \\ 0 & 0 & -\frac{\sigma_-}{L_p} \sin(\sigma_- \frac{s-s_i}{L_p}) & \cos(\sigma_- \frac{s-s_i}{L_p}) \end{bmatrix}. \quad (\text{F13})$$

The block diagonal form of Eq. (F13) corresponds to rotations in the decoupled $r_+ - r'_+$ and $r_- - r'_-$ phase-spaces. This solution also follows immediately from Eq. (65). Finally, it is instructive to point out that the transformation to fully decoupled coordinates presented in Eq. (F11) can be derived in terms of two successive linear transformations, first a transformation to decoupled δr_{\pm} coordinates as given by Eq. (F12) and then a transformation from trigonometric forms [i.e., $\cos[\sigma_{\pm}(s - s_i)/L_p]$] to exponential forms [i.e., $e^{i\sigma_{\pm}(s-s_i)/L_p}$].

APPENDIX G: THIN-LENS ANALYSIS OF NORMAL ENVELOPE MODES IN PERIODIC SOLENOIDAL AND FODO QUADRUPOLE FOCUSING CHANNELS AT ZERO AND FULL SPACE-CHARGE DEPRESSION

Normal envelope modes of thin-lens ($\eta \rightarrow 0$ with σ_0 fixed) solenoidal and FODO ($\alpha = 1/2$) quadrupole focusing channels can be analyzed analytically in the limit of zero ($\sigma \rightarrow \sigma_0$) and full ($\sigma \rightarrow 0$) space-charge depression[38]. In the zero space-charge limit, the x - and y -envelope coordinates decouple and the general analysis in II F applies to show that all envelope modes have phase advance $2\sigma_0$. As a consequence of this phase advance limit and the decoupling, instabilities are possible only for $\sigma_0 = 90^\circ$ and 180° . A straightforward transfer matrix analysis of single-particle orbits can then be used to show that there is no envelope instability for $\sigma_0 = 90^\circ$, and there is linear growth in oscillation amplitude with lattice periods traversed for $\sigma_0 = 180^\circ$.

To analyze the opposite limit of full space-charge depression, we proceed as follows. Let L be the length of the free-drift interval between the two subsequent thin-lenses, solenoids or quadrupoles ($L_p = L$ for solenoids and $L_p = 2L$ for quadrupoles) as illustrated in Fig. 24. By symmetry we only need to consider the envelope evolution of the beam between two lenses only. We take the first lens to be at axial location $s = -L/2$ and the second one to be at $s = L/2$.

The envelope equations (4) for the case of a fully depressed beam (with $\sigma = 0$), which corresponds to zero beam emittance ($\varepsilon_x = \varepsilon_y = 0$), can be written in terms of scaled sum and difference coordinates $R_{\pm} = (r_x \pm r_y)/(2\sqrt{2Q})$ as:

$$\begin{aligned} 2R_+''(s) + 2\kappa_x(s)R_+(s) - \frac{1}{R_+(s)} &= 0, \\ 2R_-''(s) + 2\kappa_x(s)R_-(s) &= 0 \end{aligned} \quad (\text{G1a})$$

for solenoidal focusing, and

$$\begin{aligned} 2R_+''(s) + 2\kappa_x(s)R_-(s) - \frac{1}{R_+(s)} &= 0, \\ 2R_-''(s) + 2\kappa_x(s)R_+(s) &= 0 \end{aligned} \quad (\text{G1b})$$

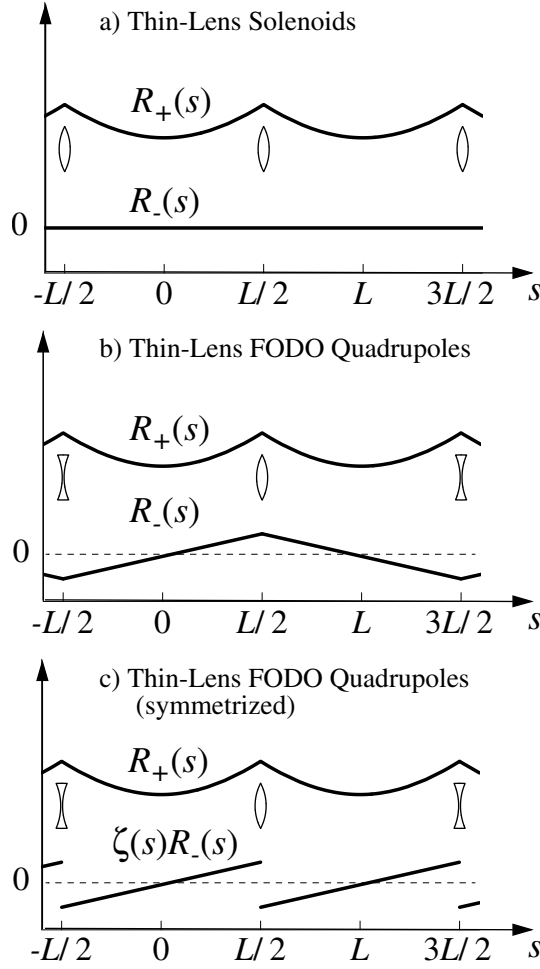


FIG. 24: Matched beam envelopes $R_{\pm}(s)$ and transport lattice for (a) solenoid and (b) FODO quadrupole thin-lens transport channels. In (c), $\zeta(s)R_-(s)$ is plotted for the quadrupole channel.

for quadrupole focusing. Here, we have employed $\kappa_x = \kappa_y$ for solenoidal focusing and $\kappa_x = -\kappa_y$ for quadrupole focusing. For the solenoidal channel all thin-lens focusing kicks are focusing in x . Without loss of generality, we assume that in the alternating gradient channel that the lens at $s = L/2$ is focusing in x . Then for both thin-lens solenoids and quadrupoles we take near $s = L/2$ [see Eq. (13)]

$$\kappa_x(s) = \frac{1}{f} \delta\left(s - \frac{L}{2}\right), \quad (\text{G2})$$

where $f = \text{const}$ is the thin-lens focal length and $\delta(s)$ is the Dirac delta-function. The focal length f can be related to the undepressed particle phase advance over one lattice period σ_0 as [see Eq. (30)]

$$\frac{L}{f} = \begin{cases} 2 - 2 \cos \sigma_0, & \text{solenoidal focusing,} \\ \sqrt{2 - 2 \cos \sigma_0}, & \text{quadrupole focusing.} \end{cases} \quad (\text{G3})$$

To analyze the envelope stability of the fully space-charge depressed beam in solenoidal and quadrupole focusing channels we examine the change in the envelope coordinate vector $\mathbf{R}(s) = (R_+(s), R'_+(s), \zeta(s)R_-(s), \zeta(s)R'_-(s))$ from the mid-drift at $s = 0$ to the next mid-drift at $s = L$. Here, $\zeta(s) = 1$ when the next lens to be traversed is focusing, and $\zeta(s) = -1$ when the next lens is defocusing. For solenoidal focusing $\zeta(s) = 1$, and for alternating gradient quadrupole focusing $\zeta(s) = -1$ for $0 \leq s \leq L/2$ and $\zeta(s) = 1$ for $L/2 < s \leq L$. The effect of $\zeta(s)$ is to map the matched beam envelope R_- in the second drift region of the quadrupole ($L/2 < s \leq L$) into the first drift region ($0 \leq s < L/2$) [see Fig. 24(c)]. This mapping expedites the use of symmetry in the matched envelope to simplify calculations for the FODO lattice.

To analyze the first-order perturbations in the coordinate vector $\mathbf{R}(s)$ we compute the Jacobian matrix $\mathbf{M}(0, L)$ where $\mathbf{M}(s_1|s_2) = \partial \mathbf{R}(s_2) / \partial \mathbf{R}(s_1)$ and derivatives are evaluated for a matched beam envelope. The Jacobian matrix

$\mathbf{M}(0|L)$ is identical to the symplectic transfer map in Eq. (46). Analogously to the treatment in Sec. IIF, the stability of the envelope to linear perturbations about the matched envelope solution corresponds to $\mathbf{M}(0|L)$ having all eigenvalues on the complex unit circle. To characterize mode properties, eigenvalues will be calculated in terms of σ_0 .

In calculating $\mathbf{M}(0|L)$, we henceforth denote $\mathcal{F}(s \pm 0) \equiv \lim_{\delta \rightarrow \pm 0} \mathcal{F}(s + \delta)$ to represent the discontinuous action of the thin-lenses on the beam envelope functions. To exploit lattice symmetries, we split the interval $(0, L)$ into three parts $(0, \frac{L}{2} - 0)$, $(\frac{L}{2} - 0, \frac{L}{2} + 0)$ and $(\frac{L}{2} + 0, L)$, and calculate $\mathbf{M}(0, L)$ as

$$\mathbf{M}(0|L) = \mathbf{M}(\frac{L}{2} + 0|L) \mathbf{M}(\frac{L}{2} - 0|\frac{L}{2} + 0) \mathbf{M}(0|\frac{L}{2} - 0).$$

By symmetry, $\mathbf{M}(\frac{L}{2} + 0|L) = \mathbf{M}(0|\frac{L}{2} + 0)^{-1}$ and so this can be expressed as

$$\mathbf{M}(0|L) = \mathbf{M}_f(-\frac{L}{2} + 0)^{-1} \mathbf{M}_s \mathbf{M}_f(\frac{L}{2} - 0), \quad (\text{G4})$$

where $\mathbf{M}_s = \mathbf{M}(\frac{L}{2} - 0|\frac{L}{2} + 0)$ is the “singular Jacobian” associated with the thin-lens focusing kick, and $\mathbf{M}_f(s) = \mathbf{M}(0|s)$ for $|s| < L/2$ is the “free-drift Jacobian” associated with the half-drift.

To evaluate \mathbf{M}_s , we consider the action of the thin-lens according to Eq. (14). We obtain for the solenoidal channel

$$\mathbf{M}_s = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\frac{1}{f} & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & -\frac{1}{f} & 1 \end{bmatrix}, \quad (\text{G5a})$$

and for the quadrupole channel keeping in mind that the $\zeta(s)R_-$ changes sign from one free-drift region to the next,

$$\mathbf{M}_s = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & -\frac{1}{f} & 0 \\ 0 & 0 & -1 & 0 \\ \frac{1}{f} & 0 & 0 & -1 \end{bmatrix}. \quad (\text{G5b})$$

Using Eq. (G3), the elements of \mathbf{M}_s can be expressed in terms of σ_0 and L .

To evaluate elements of $\mathbf{M}_f(s)$, the space-charge dominated free-expansion solutions in Eqs. (18) and the Hamiltonian constraint in Eq. (C1) are employed. These equations, valid within the drift regions, can be expressed in the scaled R_{\pm} coordinates as

$$\ln \frac{R_+(s)}{R_+(0)} = -R_+^{\prime 2}(0) + \left\{ \text{erfi}^{(-1)} \left[\text{erfi } R_+'(0) + e^{R_+^{\prime 2}(0)} \frac{s}{\sqrt{\pi} R_+(0)} \right] \right\}^2, \quad (\text{G6a})$$

$$R_-(s) = R_-(0) + R_-'(0)s, \quad (\text{G6b})$$

$$R_+^{\prime 2}(s) - \ln R_+(s) = \text{const.} \quad (\text{G6c})$$

Here, $R_{\pm}(0)$ and $R'_{\pm}(0)$ are the values of $R_{\pm}(s)$ and $R'_{\pm}(s)$ at $s = 0$. Eqs. (G6a) and (G6b) for $R_{\pm}(s)$ satisfy Eqs. (G1a) and (G1b) in the free-drift region $|s| < L/2$ where $\kappa_x(s) = 0$. Employing Eq. (G6a) and $R_+'(0) = 0$, which follows from the matched beam symmetry $R_+(s) = R_+(-s)$, yields

$$\mathbf{M}_f(s) = \begin{bmatrix} \frac{R_+(s) - s R_+'(s)}{R_+(0)} & 2R_+(0) R_+'(s) & 0 & 0 \\ -\frac{s}{2R_+(0) R_+(s)} & \frac{R_+(0)}{R_+(s)} & 0 & 0 \\ 0 & 0 & 1 & s \\ 0 & 0 & 0 & 1 \end{bmatrix}. \quad (\text{G7})$$

To complete the evaluation of $\mathbf{M}_f(L/2 - 0)$, we find relations of the elements to σ_0 and L by deriving equations connecting $R_+(L/2 - 0) \equiv R_+(L/2)$, $R_+'(L/2 - 0)$, and $R_+(0)$ to these quantities for the matched beam envelope. By symmetry, for a periodic matched envelope

$$\begin{aligned} R_+'(\frac{L}{2} - 0) &= -R_+'(\frac{L}{2} + 0), \\ R_-'(\frac{L}{2} - 0) &= -R_-'(\frac{L}{2} + 0). \end{aligned} \quad (\text{G8})$$

For solenoids, Eqs. (G1a) and (G2) can be integrated once about $s = L/2$ to show that

$$\begin{aligned} R'_+(\frac{L}{2} + 0) &= R'_+(\frac{L}{2} - 0) - \frac{1}{f} R_+(\frac{L}{2}), \\ R'_-(\frac{L}{2} + 0) &= R'_-(\frac{L}{2} - 0) - \frac{1}{f} R_-(\frac{L}{2}). \end{aligned}$$

Combining these constraints with the matching conditions (G8), we get

$$\begin{aligned} R'_+(\frac{L}{2} - 0) &= \frac{1}{2f} R_+(\frac{L}{2}), \\ R'_-(\frac{L}{2} - 0) &= \frac{1}{2f} R_-(\frac{L}{2}). \end{aligned} \tag{G9a}$$

Similarly, using Eqs. (G1b) and (G2) for alternating gradient focusing and matched beam symmetries (G8), we obtain

$$\begin{aligned} R'_+(\frac{L}{2} - 0) &= \frac{1}{2f} R_-(\frac{L}{2}), \\ R'_-(\frac{L}{2} - 0) &= \frac{1}{2f} R_+(\frac{L}{2}). \end{aligned} \tag{G9b}$$

For quadrupole focusing, Eqs. (G9b) and (14) can be combined to yield an additional constraint

$$R'_+(\frac{L}{2} - 0) = \frac{L}{8f^2} R_+(\frac{L}{2}). \tag{G9c}$$

Both the solenoidal and quadrupole matching conditions in Eqs. (G9) for R_+ can be expressed as

$$R'_+(\frac{L}{2} - 0) = \frac{\hat{k}}{L} R_+(\frac{L}{2}), \tag{G10}$$

where

$$\hat{k} = \begin{cases} \frac{L}{2f} = 1 - \cos \sigma_0, & \text{solenoidal focusing,} \\ \frac{L^2}{8f^2} = \frac{1}{4}(1 - \cos \sigma_0), & \text{quadrupole focusing.} \end{cases}$$

Applying the constant, drift region envelope Hamiltonian in Eq. (G6c) between $s = 0$ and $s = L/2 - 0$ and taking $R'_+(0) = 0$ consistent with a matched beam equilibrium in the resulting expression leads to the constraint

$$R_+(\frac{L}{2}) = R_+(0) e^{R'_+(\frac{L}{2}-0)}. \tag{G11}$$

Then evaluating the free-drift expansion formula (G6a) at $s = L/2$ with $R'_+(0) = 0$ and using Eq. (G11) to simplify the result yields

$$\frac{L}{R_+(0)} = 2\sqrt{\pi} \operatorname{erfi} R'_+(\frac{L}{2} - 0). \tag{G12}$$

Equations (G10)–(G12) produce a relation between σ_0 and $R'_+(\frac{L}{2} - 0)$:

$$\hat{k} = 2\sqrt{\pi} e^{-R'_+(\frac{L}{2}-0)} R'_+(\frac{L}{2} - 0) \operatorname{erfi} R'_+(\frac{L}{2} - 0). \tag{G13}$$

Equations (G10)–(G13) provide the needed constraints to relate the elements of $\mathbf{M}_f(L/2 - 0)$ to σ_0 and L . Needed elements of $\mathbf{M}_f(-L/2 + 0)$ can be calculated from these constraints using the matched beam symmetry requirements

$$\begin{aligned} R_+(-\frac{L}{2}) &= R_+(\frac{L}{2}), \\ R'_+(-\frac{L}{2} + 0) &= -R'_+(\frac{L}{2} - 0). \end{aligned} \tag{G14}$$

Henceforth, to abbreviate formulas, we denote $R'_+(L/2 - 0) \equiv R'_+(L/2)$ and $R'_+(-L/2 + 0) \equiv R'_+(-L/2)$.

For solenoidal focusing R_{\pm} are uncoupled, and $\mathbf{M}(0|L)$ is of block diagonal form with [see Eq. (50)]

$$\mathbf{M}(0|L) = \begin{bmatrix} \mathbf{M}_+(0|L) & 0 \\ 0 & \mathbf{M}_-(0|L) \end{bmatrix},$$

where $\mathbf{M}_{\pm}(0|L)$ are 2×2 symplectic matrices that can be independently analyzed for the stability of perturbations in R_+ (breathing mode) and R_- (quadrupole mode). Mode phase advances (σ_{\pm}) and growth factors (γ_{\pm}) can be

calculated from the eigenvalues λ_{\pm} of $\mathbf{M}_{\pm}(0|L)$. Stable modes with λ_{\pm} on the complex unit circle correspond to $(1/2) |\text{Tr } \mathbf{M}_{\pm}(0|L)| < 1$ [see Eq. (52)]. The matrices $\mathbf{M}_{\pm}(0|L)$ can be evaluated from Eqs. (G4) using Eqs. (G5a) and (G7). Resulting expressions are simplified with the constraints in Eqs. (G10)–(G12) to show that

$$\begin{aligned} \mathbf{M}_+(0|L) &= \begin{bmatrix} \frac{R_+(-\frac{L}{2}) + \frac{L}{2} R'_+(-\frac{L}{2})}{R_+(0)} & 2R_+(0)R'_+(-\frac{L}{2}) \\ \frac{\frac{L}{2}}{2R_+(0)R_+(-\frac{L}{2})} & \frac{R_+(0)}{R_+(-\frac{L}{2})} \end{bmatrix}^{-1} \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} \begin{bmatrix} \frac{R_+(\frac{L}{2}) - \frac{L}{2} R'_+(\frac{L}{2})}{R_+(0)} & 2R_+(0)R'_+(\frac{L}{2}) \\ -\frac{\frac{L}{2}}{2R_+(0)R_+(\frac{L}{2})} & \frac{R_+(0)}{R_+(\frac{L}{2})} \end{bmatrix} \\ &= \begin{bmatrix} \cos \sigma_0 - 4R_+'^2(\frac{L}{2}) \cos^2(\frac{\sigma_0}{2}) & 2\frac{R_+^{(0)}}{f} [1 - 2R_+'^2(\frac{L}{2})] \\ \frac{-f}{R_+^2(0)} \cos^2(\frac{\sigma_0}{2}) [1 - \cos \sigma_0 + 4R_+'^2(\frac{L}{2}) \cos^2(\frac{\sigma_0}{2})] & \cos \sigma_0 - 4 \cos^2(\frac{\sigma_0}{2}) R_+'^2(\frac{L}{2}) \end{bmatrix}, \\ \mathbf{M}_-(0|L) &= \begin{bmatrix} 1 & -\frac{L}{2} \\ 0 & 1 \end{bmatrix}^{-1} \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} \begin{bmatrix} 1 & \frac{L}{2} \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos \sigma_0 & \frac{L}{2}(1 + \cos \sigma_0) \\ -\frac{2}{L}(1 - \cos \sigma_0) & \cos \sigma_0 \end{bmatrix}. \end{aligned} \quad (\text{G15})$$

Eigenvalues λ_{\pm} of the matrices $\mathbf{M}_{\pm}(0|L)$ are calculated from Eq. (G15) as

$$\begin{aligned} \lambda_+ &= \cos \sigma_0 - 4R_+'^2(\frac{L}{2}) \cos^2(\frac{\sigma_0}{2}) \pm 2i \cos(\frac{\sigma_0}{2}) \sqrt{[1 - 2R_+'^2(\frac{L}{2})] [\sin^2(\frac{\sigma_0}{2}) + 2R_+'^2(\frac{L}{2}) \cos^2(\frac{\sigma_0}{2})]}, \\ \lambda_- &= \cos \sigma_0 \pm i \sin \sigma_0. \end{aligned} \quad (\text{G16})$$

From these eigenvalues, we calculate mode phase advances

$$\begin{aligned} \sigma_+ &= \arg \lambda_+ \text{ with } + \text{ sign in Eq. (G16),} \\ \sigma_- &= \sigma_0, \end{aligned} \quad (\text{G17})$$

and growth factors

$$\begin{aligned} \gamma_+ &= \begin{cases} 1, & \text{in stable regions,} \\ \sqrt{2 [\cos \sigma_0 - 4R_+'^2(\frac{L}{2}) \cos^2(\frac{\sigma_0}{2})]^2 - 1}, & \text{in unstable region,} \end{cases} \\ \gamma_- &= 1. \end{aligned} \quad (\text{G18})$$

These solutions for σ_{\pm} and γ_{\pm} are plotted in Fig. 25 as a function of σ_0 using the constraint equation (G13) to numerically eliminate $R_+^2(L/2)$ in terms of σ_0 . Continuous focusing results $\sigma_+ = \sqrt{2}\sigma_0$ and $\sigma_- = \sigma_0$ [see Eq. (64) with $\sigma = 0$] are superimposed on the phase advance plot for branch comparison. The extent of the band of instability ($\gamma_+ \neq 1$) in σ_0 can be calculated from γ_+ directly or by examining where the stability condition [see Eq. (52)]

$$\frac{1}{2} |\text{Tr } \mathbf{M}_+(0|L)| = \cos \sigma_0 - 4R_+'^2(\frac{L}{2}) \cos^2(\frac{\sigma_0}{2}) < 1$$

is violated. This occurs where $R_+^2(L/2) > 1/2$ and $\sigma_0 < \pi$. Using Eqs. (G10)–(G13) we conclude that the instability band for solenoidal focusing is located on the interval

$$\sigma_0 \in \left[\arccos \left(1 - \sqrt{\frac{2\pi}{e}} \text{erfi} \frac{1}{\sqrt{2}} \right), \pi \right] \approx [116.715^\circ, 180^\circ]. \quad (\text{G19})$$

Here, we have denoted the boundary points of the interval to be unstable based on an analysis of the matrices $\mathbf{M}_{\pm}(0|L)$ which shows that there is linear growth in R_+ when $R_+^2(L/2) = 1/2$, and linear growth in R_- when $\sigma_0 = \pi$.

The stability of quadrupole focusing can be investigated analogously to the case of solenoidal focusing except that we must work with the full 4×4 Jacobian matrix $\mathbf{M}(0|L)$ because R_{\pm} are coupled in this case. After multiplying out the matrices in Eq. (G4) and employing Eqs. (G9c) and (G14), we obtain

$$\mathbf{M}(0|L) = \begin{bmatrix} 1 - \frac{L^2}{8f^2} & \frac{L}{2f^2} R_+^2(0) & -\frac{L}{4f^3} R_+(0) R_+(\frac{L}{2}) & -\frac{L^2}{8f^2} R_+(0) R_+(\frac{L}{2}) \\ \frac{L(L^2/f^2 - 16)}{32fR_+(0)} & 1 - \frac{L^2}{8f^2} & \frac{(L^2/f^2 - 16)R_+(\frac{L}{2})}{16fR_+(0)} & \frac{L(L^2/f^2 - 16)R_+(\frac{L}{2})}{32fR_+(0)} \\ -\frac{L(L^2/f^2 - 16)R_+(\frac{L}{2})}{32fR_+(0)} & \frac{L^2}{8f^3} R_+(0) R_+(\frac{L}{2}) & -1 & -L \\ -\frac{L(L^2/f^2 - 16)R_+(\frac{L}{2})}{16fR_+(0)} & \frac{L}{4f^3} R_+(0) R_+(\frac{L}{2}) & 0 & -1 \end{bmatrix}. \quad (\text{G20})$$

The four eigenvalues λ of $\mathbf{M}(0|L)$ are calculated from Eq. (G20) and then simplified using the constraints in Eqs. (G10)–(G13). We obtain:

$$\lambda = w - \frac{1}{4} \sin^2(\frac{\sigma_0}{2}) \pm i \sqrt{\frac{1}{2} w \sin^2(\frac{\sigma_0}{2}) + \frac{1}{2} [1 - \frac{1}{4} \sin^2(\frac{\sigma_0}{2})] [\sin^2(\frac{\sigma_0}{2}) + 16R_+'^2(\frac{L}{2})]}, \quad (\text{G21})$$

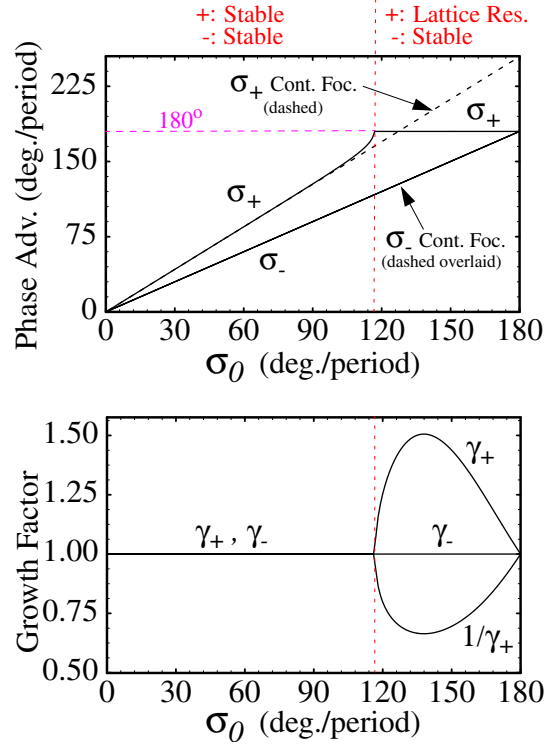


FIG. 25: Phase advance (σ_{\pm}) and growth factors (γ_{\pm}) for the breathing and quadrupole modes versus σ_0 for a thin-lens solenoidal focusing channel and a fully depressed beam with $\sigma = 0$. Continuous focusing model predictions for σ_{\pm} are indicated with dashed lines.

where

$$w = \pm \sqrt{\left[1 - \frac{1}{4} \sin^2\left(\frac{\sigma_0}{2}\right)\right] \left[1 - \frac{1}{4} \sin^2\left(\frac{\sigma_0}{2}\right) - 8R_+^2 \left(\frac{L}{2}\right)\right]}.$$

These eigenvalues can be employed to calculate phase advances (σ_B and σ_Q) and growth factors (γ_B and γ_Q) of the breathing and quadrupole modes as $\sigma_{B,Q} = 2 \arg \lambda$ and $\gamma_{B,Q} = |\lambda^2|$. Here, the factors of two stem from $\mathbf{M}(0|L)$ being a half-period advance in a symmetric FODO lattice with period $2L$. The physical branches of λ selected according to the prescriptions given in Sec. II F correspond to Taylor series $\sigma_B = \sqrt{2}\sigma_0(1 + \frac{1}{768}\sigma_0^4 + \frac{211}{967680}\sigma_0^6 + \dots)$ and $\sigma_Q = \sigma_0(1 + \frac{1}{96}\sigma_0^2 + \frac{203}{92160}\sigma_0^4 + \dots)$. These solutions are plotted in Fig. 26 as a function of σ_0 using the constraint equation (G13) to numerically eliminate $R'_+(L/2)$ in terms of σ_0 . Using Eqs. (G13) and Eq. (G21) we find numerically that the instability band is located on the interval

$$\sigma_0 \in (121.055^\circ, 180^\circ). \quad (\text{G22})$$

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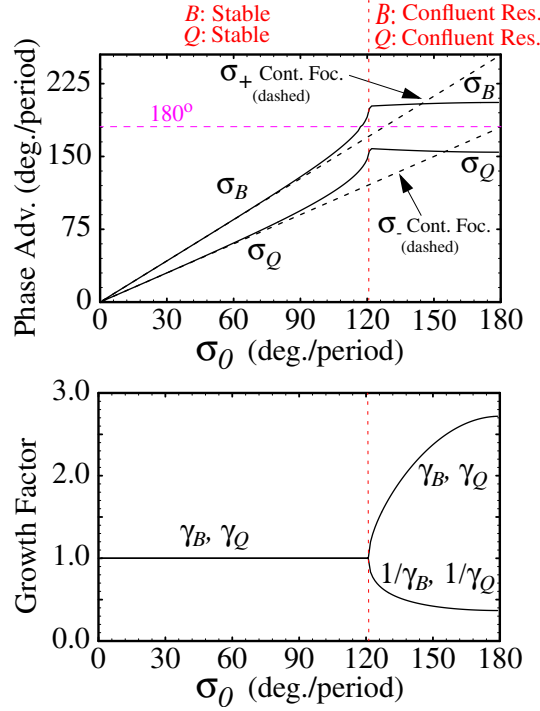


FIG. 26: Phase advance (σ_Q and σ_B) and growth factors (γ_Q and γ_B) for the breathing and quadrupole modes versus σ_0 for a thin-lens FODO quadrupole focusing channel and a fully depressed beam with $\sigma = 0$. Continuous focusing model predictions for σ_{\pm} are indicated with dashed lines.

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- [1] I. Kapchinskij and V. Vladimirskij, in *Proceedings of the International Conference on High Energy Accelerators and Instrumentation* (CERN Scientific Information Service, Geneva, 1959), p. 274.
 - [2] M. Reiser, *Theory and Design of Charged Particle Beams* (John Wiley & Sons, Inc., New York, 1994).
 - [3] R. C. Davidson and H. Qin, *Physics of Intense Charged Particle Beams in High Energy Accelerators* (World Scientific, 2001).
 - [4] I. Hofmann, L. J. Laslett, L. Smith, and I. Haber, *Particle Accelerators* **13**, 145 (1983).
 - [5] P. M. Lapostolle, *IEEE Trans. Nucl. Sci.* **18**, 1101 (1971).
 - [6] F. J. Sacherer, *IEEE Trans. Nucl. Sci.* **18**, 1105 (1971).
 - [7] J. Struckmeier and M. Reiser, *Part. Accel.* **14**, 227 (1984).
 - [8] R. L. Gluckstern, *Phys. Rev. Lett.* **73**, 1247 (1994).
 - [9] S. M. Lund and R. C. Davidson, *Physics of Plasmas* **5**, 3028 (1998).
 - [10] This result can be proved for small-amplitude mismatch excursions about a matched beam using results developed later. No fully nonlinear proof is known for large-amplitude mismatches, although numerical results support the conjecture.
 - [11] S. Humphries, *Charged Particle Beams* (John Wiley & Sons, Inc., New York, 1990).
 - [12] E. D. Courant and H. S. Snyder, *Annals of Physics* **3**, 1 (1958).
 - [13] H. Wiedemann, *Particle Accelerators Physics: Basic Principles and Linear Beam Dynamics* (Springer-Verlag, New York, 1993).
 - [14] R. Pakter and F. B. Rizzato, *Phys. Rev. Lett.* **87**, 044801 (2001).
 - [15] R. Pakter and F. B. Rizzato, *Phys. Rev. E* **65**, 056503 (2002).
 - [16] Caution must be used when interpreting Refs. [14] and [15] because the authors employ σ_0 as a focusing parameter which does not correspond the undeepressed particle phase-advance.
 - [17] E. Lee and R. J. Briggs, *Tech. Rep. LBNL-40774, UC-419*, Lawrence Berkeley National Laboratory (1997).
 - [18] E. P. Lee, *Physics of Plasmas* **9**, 4301 (2002).
 - [19] E. P. Lee, T. J. Fessenden, and L. J. Laslett, *IEEE Trans. Nuc. Sci.* **NS-26**, 2489 (1985).
 - [20] C. Chen and R. C. Davidson, *Phys. Rev. Lett.* **72**, 2195 (1994).
 - [21] Q. Qian and R. C. Davidson, *Phys. Rev. E* **53**, 5349 (1996).
 - [22] A. Dragt, in *Physics of High Energy Particle Accelerators*, edited by R. A. Carrigan, F. R. Hudson, and M. Month

- (American Institute of Physics, New York, 1982), vol. AIP Conf. Proc. No. 87, p. 147.
- [23] J. J. Barnard, S. M. Lund, and M. de Hoon, Tech. Rep. Lawrence Berkeley National Laboratory, LBNL-49286, United States Particle Accelerator School, Course Notes, Boulder, CO, June 4–8 (2001).
 - [24] V. P. Karpenko, P. A. Seidl, R. M. Franks, and S. M. Lund, in *Proceedings of the 2001 Particle Accelerator Conference* (IEEE #01CH37268C. Piscataway, NJ 08855, 2001), p. 1447.
 - [25] P. A. Seidl, D. Baca, F. M. Bieniosek, A. Faltens, S. M. Lund, A. W. Molvik, L. R. Prost, D. B. Shuman, and W. L. Waldron, *Laser and Particle Beams* **20**, 435 (2002).
 - [26] C. K. Allen and M. Reiser, *Nuc. Instr. Meth. A* **384**, 322 (1997).
 - [27] D. P. Grote, A. Friedman, I. Haber, W. Fawley, and J.-L. Vay, *Nuc. Instr. Meth. A* **415**, 428 (1998).
 - [28] H. Wiedemann, *Particle Accelerators Physics II: Nonlinear and Higher-Order Beam Dynamics* (Springer-Verlag, New York, 1995).
 - [29] F. J. Sacherer, Ph.D. thesis, University of California (1968).
 - [30] R. B. Miller, *An Introduction to the Physics of Intense Charged Particle Beams* (Plenum Press, New York, 1982).
 - [31] E. P. Lee and R. K. Cooper, *Part. Accel.* **7**, 83 (1976).
 - [32] A. J. Dragt, F. Neri, and G. Rangarajan, *Phys. Rev. A* **45**, 2572 (1992).
 - [33] R. A. Kishek, J. J. Barnard, and D. P. Grote, in *Proceedings of the 1999 Particle Accelerator Conference* (New York City, 1999), p. 1761.
 - [34] J. J. Barnard and B. Losic, in *Proceedings of the XX International Linac Conference* (Monterey, CA, 2001), p. 293 and MOE12.
 - [35] The alternating gradient case with $P_\theta \neq 0$ can occur in lattices with skew quadrupoles or where the principal axes of the elliptical beam are not initially aligned with the quadrupole axes.
 - [36] C. Chen, R. Pakter, and R. C. Davidson, *Phys. Rev. Lett.* **79**, 225 (1997).
 - [37] D. A. Edwards and L. C. Teng, *IEEE Trans. Nuc. Sci.* **20**, 885 (1973).
 - [38] B. Bukh and S. M. Lund, in *Proceedings of the 2003 Particle Accelerator Conference* (Portland, OR, 2003), p. WPPG019.